

AFML-TR-79-4037 Vol II



Evaluation of the Crac for Monitoring Aircraft Flaw Growth Potential Volume II – Test Results of the Potential **Evaluation of the Crack Gage Concept** for Monitoring Aircraft

Volume II - Test Results

A Division of The Boeing Company 3801 South Oliver Wichita, Kansas 67210

June 1979

Technical Report AFML-TR-79-4037, Vol. II.

611018

Final Report for Period July 1977 - December 1978

Distribution Statement

Approved for public release: distribution unlimited

Prepared for

United States Air Force Air Force Systems Command Aeronautical Systems Division/PPMRR Wright-Patterson AFB, Ohio 45433

79 11 05 119

NOTICE

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor any obligation whatsover; and the fact that the government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

This report has been reviewed by the Information Office (01) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

ALTEN F. GRANDT, Jr.

Project Engineer

Metals Behavior Branch

Metals and Ceramics Division

MG Tupper NATHAN G. TUPPER, Chief

Metals Behavior Branch

Metals and Ceramics Division

"If your address has changed, if you wish to be removed from our mailing list, or if the addressee is no longer employed by your organization please notify AFML/LLN, W-PAFB, OH 45433 to help us maintain a current mailing list".

Copies of this report should not be returned unless return is required by security considerations, contractual obligations, or notice on a specific document.

AIR FORCE/56780/1 October 1979 - 270

DISCLAIMER NOTICE

THIS DOCUMENT IS BEST QUALITY PRACTICABLE. THE COPY FURNISHED TO DDC CONTAINED A SIGNIFICANT NUMBER OF PAGES WHICH DO NOT REPRODUCE LEGIBLY.

(19) REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
AFML-TR-79-4037 - Vol	ION NO. 3. RECIPIENT'S CATALOG NUMBER
TITLE (and Subtitle)	5. TYPE OF REPORT A REPION COVERED
EVALUATION OF THE CRACK GAGE CONCEPT FOR MONITORING AIRCRAFT FLAW GROWTH POTENTIAL	Final Report 1July 277 — December 1978.
. AUTHOR(s)	8. CONTRACT OR GRANT NUMBER(s)
Gary G. Cassatt	15 F33615-77-C-5Ø73
PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Test Engineering Unit Boeing Wichita Company Wichita, Kansas 67210	ILIR - 0092 1700
United States Air Force Wright-Patterson Air Force Systems Command Ohio Aeronautical Systems Division/PPMRR	AFB 72 Jun 79 12 2
14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling	Office) 15. SECURITY CLASS. (of this report)
Air Force Materials Laboratory (AFML/LLN)	Unclassified
Air Force Wright Aeronautical Laboratories	15a. DECLASSIFICATION/DOWNGRADING
Wright-Patterson Air Force Base, Ohio 4543	3 SCHEDULE
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if diff	erent from Report)
18. SUPPLEMENTARY NOTES	
9. KEY WORDS (Continue on reverse side if necessary and identify by block Crack Gage	number)
Stepped Design	
Flaw Growth	
Fleet Tracking	
0. ABSTRACT (Continue on reverse side If necessary and identify by block	
The results of a test program to evaluate the ded coupon to monitor the growth of flaws in All testing utilized 7075-T651 aluminum from thickness and stepped crack gages were evaluated.	the basic structure are included. a a single plate. Both constant

SECURITY CLASSIFICATION OF THIS PAGE(When Date Entered) flaw were evaluated. The cyclic test loading included constant amplitude of two R ratios and three representative aircraft usage flight profiles. Strain gage instrumentation was used to measu a structure stresses and load transferred into the crack gages.

FOREWORD

The experimental research program reported herein was the responsibility of the Test Engineering Unit of the Boeing Wichita Company. The work was conducted in the time period from 1 July 1977 to 1 December 1978. The work was performed to fulfill the requirements of the Air Force Materials Laboratory Contract F33615-77-C-5073.

A. F. Grandt was the AFML technical monitor. Dr. Grandt's guidance and interest were of great benefit to the program. Gary G. Cassatt of the Test Engineering Unit was the principal investigator for Boeing Wichita and all aspects of this program were conducted under his direction.

Specimen fabrication and preparation were performed by personnel of the Structures Laboratory of the Boeing Wichita Company.

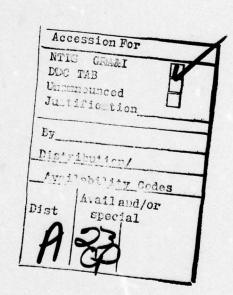
Analytical contributions were the product of Ramesh Shah of BMAD, Boeing Aerospace Company of Seattle, Washington. Dr. Shah's contributions added much to the success of the program.

Program Management was the responsibility of Jack L. Bickhard of the Boeing Wichita Company.

Significant effort was supplied by Bill Evans and Betty Dunegan for data processing and report preparation. The publication of the final report was accomplished by the Industrial Graphics Department.

TABLE OF CONTENTS

Section		Page
I	INTRODUCTION	1
11	STRESS SURVEY EVALUATION	3
III	INSTRUMENTATION DETAILS & STRAIN MEASUREMENTS	9
IV	CRACK PROPAGATION DATA	115
V	KMAX Vs da/dn CALCULATIONS AND PLOTS	167
VI	CRACK GAGE MATERIAL da/dn TESTS	225



LIST OF FIGURES

Figure		Page
. 1 1	Stress Survey Specimen Details	4
2	Stress Survey Specimen Installed in Test Machine	5
3	Instrumentation Details - Specimen AFCG-1	11
4	Instrumentation Details - Specimen AFCG-2	13
5	Instrumentation Details - Specimen AFCG-3	15
6	Instrumentation Details - Specimen AFCG-4	17
ap. 7	Instrumentation Details - Specimen AFCG-5	19
8	Instrumentation Details - Specimen AFCG-6	21
1819	Photograph of Specimen AFCG-1 Side 1	23
10	Photograph of Specimen AFCG-1 Side 2	24
11	Photograph of Specimen AFCG-2 Side 1	25
12	Photograph of Specimen AFCG-2 Side 1 Detail	26
13	Photograph of Specimen AFCG-2 Side 1 Detail	27
14	Photograph of Specimen AFCG-2 Side 2	28
15	Photograph of Specimen AFCG-2 Side 2 Detail	29
16	Photograph of Specimen AFCG-2 Side 2 Detail	30
17	Photograph of Specimen AFCG-3 Side 1	31
18	Photograph of Specimen AFCG-3 Side 1 Detail	32
19	Photograph of Specimen AFCG-3 Side 1 Detail	33
20	Photograph of Specimen AFCG-3 Side 2	34
21	Photograph of Specimen AFCG-3 Side 2 Detail	35
22	Photograph of Specimen AFCG-3 Side 2 Detail	36
23	Photograph of Specimen AFCG-4 Side 1	37
24	Photograph of Specimen AFCG-4 Side 1 Detail	38
25	Photograph of Specimen AFCG-4 Side 1 Detail	39
26	Photograph of Specimen AFCG-4 Side 2	40
27	Photograph of Specimen AFCG-4 Side 2 Detail	41
28	Photograph of Specimen AFCG-4 Side 2 Detail	42

LIST OF FIGURES (CONTINUED)

Figure		Page
29	Photograph of Specimen AFCG-5 Side 1	43
30	Photograph of Specimen AFCG-5 Side 2	44
31	Photograph of Specimen AFCG-6 Side 1	45
32	Photograph of Specimen AFCG-6 Side 2	46
33	Crack Propagation Plot of Crack Length Vs Cycles - AFCG-1 Side 1	155
34	Crack Propagation Plot of Crack Length Vs Cycles - AFCG-1 Side 2	156
35	Crack Propagation Plot of Crack Length Vs Cycles - AFCG-2 Side 1	157
36	Crack Propagation Plot of Crack Length Vs Cycles - AFCG-2 Side 2	158
37	Crack Propagation Plot of Crack Length Vs Flights - AFCG-3 Side 1	159
38	Crack Propagation Plot of Crack Length Vs Flights - AFCG-3 Side 2	160
39	Crack Propagation Plot of Crack Length Vs Flights - AFCG-4 Side 1	161
40	Crack Propagation Plot of Crack Length Vs Flights - AFCG-4 Side 2	162
41	Crack Propagation Plot of Crack Length Vs Cycles - AFCG-5 Side 1	163
42	Crack Propagation Plot of Crack Length Vs Cycles - AFCG-5 Side 2	164
43	Crack Propagation Plot of Crack Length Vs Flights - AFCG-6 Side 1	165
44	Crack Propagation Plot of Crack Length Vs Flights - AFCG-6 Side 2	166
45	K _{MAX} Vs dc/dn Plot - AFCG-1 Flaw 2	197
46	K _{MAX} Vs dc/dn Plot - AFCG-1 Flaw 3	198
47	K _{MAX} Vs dc/dn Plot - AFCG-1 Flaw 4	199

LIST OF FIGURES (CONTINUED)

Figure		Page
48	K _{MAX} Vs d2c/dn Plot - AFCG-1 Flaw 5	200
49	K _{MAX} Vs dc/dn Plot - AFCG-2 Flaw 3	201
50	K _{MAX} Vs dc/dn Plot - AFCG-2 Flaw 4	202
51	K _{MAX} Vs d2c/dn Plot - AFCG-2 Flaw 5	203
52	K _{MAX} Vs dc/dn Plot - AFCG-3 Flaw 1	204
53	K _{MAX} Vs dc/dn Plot - AFCG-3 Flaw 2	205
54	K _{MAX} Vs dc/dn Plot - AFCG-3 Flaw 3	206
55	K _{MAX} Vs dc/dn Plot - AFCG-3 Flaw 4	207
56	K _{MAX} Vs d2c/dn Plot - AFCG-3 Flaw 5	208
57	K _{MAX} Vs dc/dn Plot - AFCG-4 Flaw 1	209
58	K _{MAX} Vs dc/dn Plot - AFCG-4 Flaw 2	210
59	K _{MAX} Vs dc/dn Plot - AFCG-4 Flaw 3	211
60	K _{MAX} Vs dc/dn Plot - AFCG-4 Flaw 4	212
61	K _{MAX} Vs d2c/dn Plot - AFCG-4 Flaw 5	213
62	K _{MAX} Vs dc/dn Plot - AFCG-5 Flaw 1	214
63	K _{MAX} Vs dc/dn Plot - AFCG-5 Flaw 2	215
64	K _{MAX} Vs dc/dn Plot - AFCG-5 Flaw 3	216
65	K _{MAX} Vs dc/dn Plot - AFCG-5 Flaw 4	217
66	K _{MAX} Vs d2c/dn Plot - AFCG-5 Flaw 5	218
67	K _{MAX} Vs dc/dn Plot - AFCG-6 Flaw 1	219
68	K _{MAX} Vs dc/dn Plot - AFCG-6 Flaw 2	220
69	K _{MAX} Vs dc/dn Plot - AFCG-6 Flaw 3	221
70	K _{MAX} Vs dc/dn Plot - AFCG-6 Flaw 4	222
71	K _{MAX} Vs d2c/dn Plot - AFCG-6 Flaw 5	223
72	Thin Section Specimen Detail & da/dn Plot	226
73	K _{MAX} Vs d2c/dn Plot - Specimen DADN-1	241
74	K _{MAX} Vs d2c/dn Plot - Specimen DADN-2	242

LIST OF FIGURES (CONCLUDED)

Figure		Page
75	K _{MAX} Vs d2c/dn Plot - Specimen DADN-3	243
76	K _{MAX} Vs d2c/dn Plot - Specimen DADN-4	244
77	K _{MAX} Vs d2c/dn Plot - Specimen DADN-5	245
78	K _{MAX} Vs d2c/dn Plot - Specimen DADN-6	246
79	K _{MAX} Vs d2c/dn Composite Plot DADN-1 Thru DADN-6	247

LIST OF TABLES

Table		Page
1	Stress Survey Results with Crack Gages Installed	6
2	Stress Survey Results with Crack Gages Removed	7
3	Structure Flaw Details - AFCG-1	12
4	Crack Gage Details - AFCG-1	12
aa 5	Structure Flaw Details - AFCG-2	14
6	Crack Gage Details - AFCG-2	14
7	Structure Flaw Details - AFCG-3	16
8	Crack Gage Details - AFCG-3	16
9	Structure Flaw Details - AFCG-4	18
10	Crack Gage Details - AFCG-4	18
11	Structure Flaw Details - AFCG-5	20
12	Crack Gage Details - AFCG-5	20
13	Structure Flaw Details - AFCG-6	22
14	Crack Gage Details - AFCG-6	22
15	Strain Gage Results at Start of Test - AFCG-1	47
16	Strain Gage Results at Start of Test - Crack Gages on AFCG-2	48
17	Strain Gage Results at 8000 Cycles - Crack Gages on AFCG-2	50
18	Strain Gage Results at 17800 Cycles - Crack Gages on AFCG-2	52
19	Strain Gage Results at 26800 Cycles - Crack Gages on AFCG-2	54
20	Strain Gage Results at 32200 Cycles - Crack Gages on AFCG-2	56
21	Strain Gage Results at 37600 Cycles - Crack Gages on AFCG-2	58
22	Strain Gage Results at 55000 Cycles - Crack Gages on AFCG-2	60
23	Strain Gage Results at 161200 Cycles - Crack Gages	62

LIST OF TABLES (CONTINUED)

Table		Page
24	Strain Gage Results for Basic emel at Start of Test - AFCG-2	64
25	Strain Gage Results for Basic Femel at 161200 Cycles - AFCG-2	65
26	Strain Gage Results for Tension Loading at Start of Test- AFCG-3	66
27	Strain Gage Results for Compression Loading at Start of Test - AFCG-3	68
28	Strain Gage Results for Tension Loading at 410 Flights - AFCG-3	70
29	Strain Gage Results for Compression Loading at 410 Flights - AFCG-3	72
30	Strain Gage Results for Tension Loading at 565 Flights - AFCG-3	74
31	Strain Gage Results for Compression Loading at 565 Flights - AFCG-3	76
32	Strain Gage Results for Tension Loading at 721 Flights - AFCG-3	78
33	Strain Gage Results for Compression Loading at 721 Flights - AFCG-3	80
34	Strain Gage Results for Tension Loading at 1000 Flights - AFCG-3	82
35	Strain Gage Results for Compression Loading at 1000 Flights - AFCG-3	84
36	Strain Gage Results for Tension wading at 1405 Flights - AFCG-3	86
37	Strain Gage Results for Compress om Loading at 1405 Flights - AFCG-3	88
38	Strain Gage Results for Tension Loading at 2520 Flights - AFCG-3	90
39	Strain Gage Results for Compress on Loading at 2520 Flights - AFCG-3	92
40	Strain Gage Results for Tension Loading at 3640 Flights -	94

LIST OF TABLES (CONTINUED)

Table		Page
41	Strain Gage Results for Compression Loading at 3640 Flights - AFCG-3	96
42	Strain Gage Results at Start of Test - AFCG-4	98
43	Strain Gage Results at 2 Flights - AFCG-4	100
44	Strain Gage Results at 499 Flights - AFCG-4	102
45	Strain Gage Results at 631 Flights - AFCG-4	104
46	Strain Gage Results at 670 Flights - AFCG-4	106
47	Strain Gage Results at 802 Flights - AFCG-4	108
48	Strain Gage Results at 876 Flights - AFCG-4	110
49	Strain Gage Results at Start of Test - AFCG-5	112
50	Strain Gage Results at Start of Test - AFCG-6	113
51	Crack Propagation Data from Side 1 - AFCG-1	116
52	Crack Propagation Data from Side 2 - AFCG-1	119
53	Crack Propagation Data from Side 1 - AFCG-2	122
54	Crack Propagation Data from Side 2 - AFCG-2	125
55	Crack Propagation Data from Side 1 - AFCG-3	128
56	Crack Propagation Data from Side 2 - AFCG-3	131
57	Crack Propagation Data from Side 1 - AFCG-4	134
58	Crack Propagation Data from Side 2 - AFCG-4	136
59	Crack Propagation Data from Side 1 - AFCG-5	138
60	Crack Propagation Data from Side 2 - AFCG-5	142
61	Crack Propagation Data from Side 1 - AFCG-6	145
62	Crack Propagation Data from Side 2 - AFCG-6	150
63	K _{MAX} Vs dc/dn Calculations - AFCG-1 Flaw 2	168
64	K _{MAX} Vs dc/dn Calculations - AFCG-1 Flaw 3	169
65	K _{MAX} Vs dc/dn Calculations - AFCG-1 Flaw 4	170
66	K _{MAX} Vs d2c/dn Calculations - AFCG-1 Flaw 5	171
67	K _{MAX} Vs dc/dn Calculations - AFCG-2 Flaw 3	172

LIST OF TABLES (CONTINUED)

Table		Page
68	K _{MAX} Vs dc/dn Calculations - AFCG-2 Flaw 4	173
69		174
	K _{MAX} Vs d2c/dn Calculations - AFCG-2 Flaw 5	
70	K _{MAX} Vs dc/dn Calculations - AFCG-3 Flaw 1	175
71	K _{MAX} Vs dc/dn Calculations - AFCG-3 Flaw 2	176
72	K _{MAX} Vs dc/dn Calculations - AFCG-3 Flaw 3	177
73	K _{MAX} Vs dc/dn Calculations - AFCG-3 Flaw 4	178
74	K _{MAX} Vs d2c/dn Calculations - AFCG-3 Flaw 5	179
75	K _{MAX} Vs dc/dn Calculations - AFCG-4 Flaw 1	180
76	K _{MAX} Vs dc/dn Calculations - AFCG-4 Flaw 2	181
77	K _{MAX} Vs dc/dn Calculations - AFCG-4 Flaw 3	182
78	K _{MAX} Vs dc/dn Calculations - AFCG-4 Flaw 4	183
79	K _{MAX} Vs d2c/dn Calculations - AFCG-4 Flaw 5	184
80	K _{MAX} Vs dc/dn Calculations - AFCG-5 Flaw 1	185
81	K _{MAX} Vs dc/dn Calculations - AFCG-5 Flaw 2	186
82	K _{MAX} Vs dc/dn Calculations - AFCG-5 Flaw 3	187
83	K _{MAX} Vs dc/dn Calculations - AFCG-5 Flaw 4	188
84		189
85		190
86		192
87	K _{MAX} Vs dc/dn Calculations - AFCG-6 Flaw 2	194
	K _{MAX} Vs dc/dn Calculations - AFCG-6 Flaw 3	
88	K _{MAX} Vs dc/dn Calculations - AFCG-6 Flaw 4	195
89	K _{MAX} Vs d2c/dn Calculations - AFCG-6 Flaw 5	196
90	Crack Propagation Data - Specimen DADN-1	227
91	Crack Propagation Data - Specimen DADN-2	228
92	Crack Propagation Data - Specimen DADN-3	229
93	Crack Propagation Data - Specimen DADN-4	230
94	Crack Propagation Data - Specimen DADN-5	231

LIST OF TABLES (CONCLUDED)

Table		Page
95	Crack Propagation Data - Specimen DADN-6	232
96	K _{MAX} Vs d2c/dn Specimen DADN-1	233
97	K _{MAX} Vs d2c/dn Specimen DADN-2	234
98	K _{MAX} Vs d2c/dn Specimen DADN-3	235
99	K _{MAX} Vs d2c/dn Specimen DADN-4	237
100	K _{MAX} Vs d2c/dn Specimen DADN-5	238
101	K _{MΔX} Vs d2c/dn Specimen DADN-6	240

NOMENCLATURE

Symbol Symbol	Discription	<u>Units</u>
a	Crack Length Down Hole Wall	MM (Inches)
ASIP	Aircraft Structural Integrity Program	
b	One Half of Width W	MM (Inches)
В	Thickness	MM (Inches)
BAC, BMS	Boeing Company Specifications	2000
BMAD	Boeing Military Airplane Group	in
BWC	Boeing Wichita Company	
C	Crack Length on Surface Out of Hole	MM (Inches)
CNS	Center Notch Stepped	
СРМ	Cycles Per Minute	Hz
da/dn	Crack Growth Rate	mm/cy(in/cy)
DFHS	Double Flawed Hole Stepped	a <u>aninyadu</u> Z
E	Elastic Modulus in Tension	M Pa (PSI)
EDM	Electrical Discharge Machining	··· 9
F	Front (Side 1) Location	aa . <u></u> . 22
FPL	Forest Products Laboratories	wA 0
Н	Unbond Length	MM (Inches)
IN	Inches	elt n
k	Structure Spring Constant	cn/mm (Pounds/Inch)
KI, SIF	Stress Intensity Factor	M Pavin (PSIVIN)
Ктн	Threshold Stress Intensity Value	
L	Length	MM (Inches)
MM	Millimeters	
MTS	MTS System Corporation, Minneapolis, Minn.	
P	Load	kN (Lbs.)
PABST	Primary Adhesive Bonded Structure	
PSI	Stress	M Pa (Lbs/In ²)
R	Ratio of Minimum Load to Maximum Load	

NOMENCLATURE (Continued)

Symbol Symbol	Description	Units
R.H.	Relative Humidity	6
SENCT	Single Edge Notch Constant Thickness	AS121
SENS	Single Edge Notch Constant Stepped	d
t (remain) M	Thickness	MM (Inches)
UFRS	Unflawed Reference Stepped	\$M07_748
V	Displacement Sucret Sharper A Visit First Sharper	MM (Inches)
w	Sceling Wichita Company htbiW	MM (Inches)
·σ (sedoni) M	Stress 910% to 180 aparad no dignal don't	M Pa (PSI)
Δ	Deflection baggers noton resmall	Inches

Subscripts

S	Structure	
G	Gross Area	
g	Crack Gage	
0	Average	
T (sadow)	Total	
N	Net Section	

SECTION I

Six specimens were tested in this program. Each specimen consisted of a large aluminum plate containing five flaws and having ten crack gages bonded on. Strain gages were used to evaluate stress fields, load distribution and load transferred through the crack gages. Three of the specimens were tested under constant amplitude loading and three were tested under variable amplitude (flight spectrum) loading. Test data consisted of crack lengths and applied cycles or flights. Flaws and cracks in the large aluminum plates will be hereinafter referred to as structure flaws, and flaws and cracks in the crack gages will be addressed as gage flaws.

In addition to the six primary tests, support testing to evaluate the influence of the crack gage installation on the basic panel stress field and to determine baseline crack propagation da/dn data for the crack gage material was conducted.

This volume contains detail sketches of the instrumentation and crack gages used on each specimen as well as raw data of strain and crack length measurements.

Also included are the computer tabulations of $K_{\mbox{MAX}}$ versus da/dn calculations.

The purpose of Volume II is to provide a complete assemblage of test results in the uncorrected and uninterpreted form to allow future researchers to conduct their own analyses and interpretations of the results. By putting the details, raw test data and data processing calculations in Volume II, Volume I becomes a more useful technical presentation uncluttered by details.

SECTION II STRESS SURVEY EVALUATION

This test utilized an aluminum plate identical in geometry to the test specimens. The purpose of this test was to verify that crack gage placement did not significantly influence the stress field at the structure flaw locations.

The test procedure consisted of the following items: 1.) Instrumenting the test panel with crack gages and strain gages. Strain gages were placed at the flaw locations, on the panel cross section and on the crack gages. 2.) Measuring strains at applied load increments to 75 KIPS tension and 3.) Removing the crack gages and again obtaining strain measurement to 75 KIPS. Tabulated results of those measurements are presented in Tables 1 and 2. Comparison of the "with" and "without" crack gage readings showed that the effect of the crack gages on the structure flaw stress field was minimal.

A drawing of the specimen, complete with instrumentation arrangement, is presented as Figure 1. A photograph of the test panel installed in the 200 KIP MTS test machine for testing is presented in Figure 2.

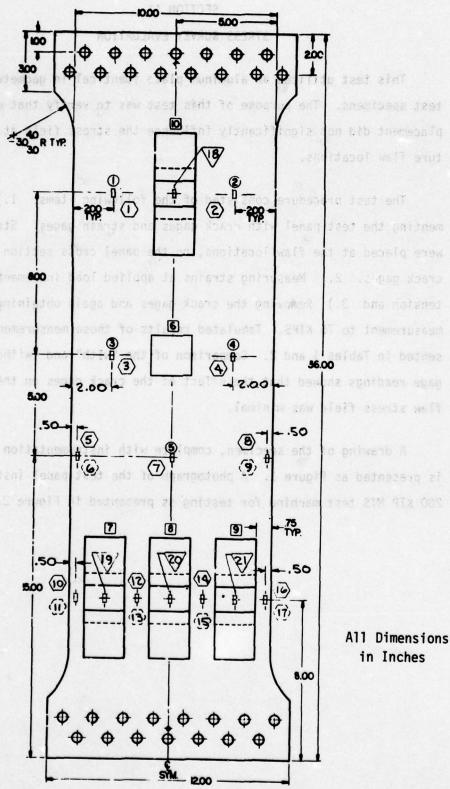


Figure 1. Stress Survey Specimen Details

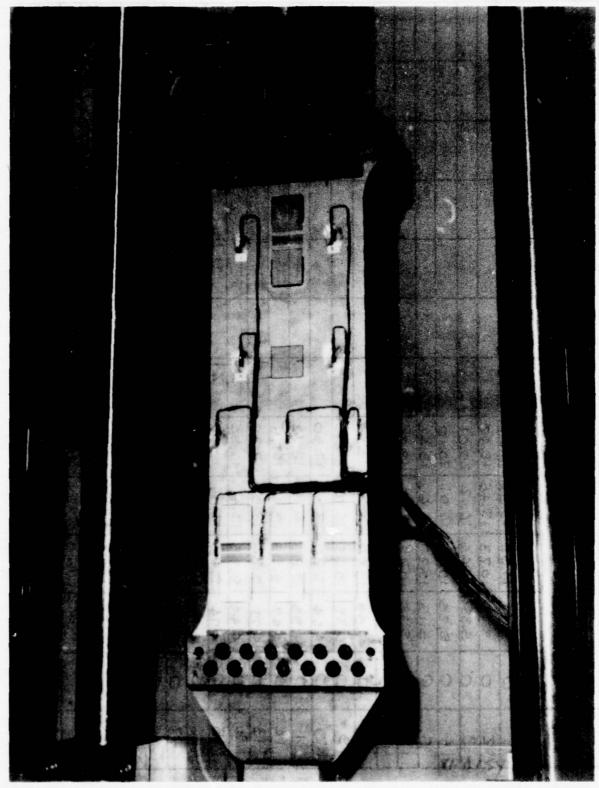


Figure 2. Stress Survey Specimer Installed in Test Machine

Table 1. Stress Survey Results with Crack Gages Installed 8.1. ~ BOLTED IN H.F. ~ HANGING FREE

																0								
KIPS (KIPS																								
NSTAL IAL LOA																								
SES L																								
AT APPL	75	19.61	19.42	20.01	20.10	19.42	19.26	80.02	19.67	20.19	17.30	18.23	16.78	17.39	16.94	17.75	17.64	18.13	1	31.22	1	31.17		
STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	09		15.45	16.12 20.01	16.01		15.66		-	16.07		14.73	13.43	13.99	13.47	14.18	-		50.87	24.93	27.30	24.85		
STRES	40	10.55		10.66	10.55	10.28	10.43	10.54	10.28					9.34	8.95	9.46	12.6	-161	19.57	16.77		16.72		
TEST CONDITION:	20	5.41	5.15	5.356	5,25	5.13	5.35	5.20	4.99	5.35	4.64	4.95	4.47	4.73	4.44	4.74	4.52	4.72	9.97	8.63	8.90	8.54		
TEST (0 81	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
STRAIN	.00		2	3	4	S	૭	7	89	6	Q	=	12	13	14	15	16	11	18	61	20	12		

Table 2. Stress Survey Results with Crack Gages Removed H.F. \sim HANGING FREE B.I. \sim BOLTED IN

STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)																						
REMOVED AXIAL LOAD (
LIED AX																						
CRACK GAGES KSI) AT APPLIED	75	20.23	19.76	20.04	19.78	19.72	19.53			19.96	19.13	20.02	19.47	20.14	19.50	20.19	19.12	19.61				
KSI)	9			16.02	15.76	15.76	15.72	15.80	15.50	15.94	15.31	16.06 20.02	15.56	16.13	15.53	16.13	15.21	15.61				
STRESS	40	10.89	10.46	10.67	10.43	10.49	10.60	10.46	10.18	10.60	10.24	10.71	10.38	10.75	10.32	10.71	10.05	10.30 15.61				
TEST CONDITION:	20	5.51	5.23	5.36	5.16	5.26	5.47	5.19	4.92	5.26	5.23	5.40			5.13	5.28	4.94	5.05				
TEST (OBI.	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0				
STRAIN	NO.	-	2	3	4	S	ڡ	7	6 0	O	0	=	12	13	14	15	١٥	17				

SECTION III

AND STRAIN MEASUREMENTS

Strain gages were utilized on all six specimens to measure specimen cross section stresses. Specimens AFCG-2, AFCG-3, and AFCG-4 were extensively instrumented with strain gages to measure, in addition to specimen stresses, loads transferred from the specimen through each crack gage type.

The strain gages were read at the start of testing on all specimens and, in addition, periodically throughout the test on Specimens AFCG-2, -3, and -4.

The instrumentation details of strain and crack gages are presented in Figures 3 through 8 for the six test specimens AFCG-1 through AFCG-6.

Photographs of each specimen presenting verification of instrumentation details are presented in Figures 9 through 32.

Tabulated measured dimensions of crack gages and structure flaws are presented in Tables 3 through 14.

Strain readings with the corresponding applied load values are presented in Tables 15 through 50.

Caution should be exercised in utilizing the strain readings in this volume. They are uncorrected raw test data. At longer crack lengths, strain gages close to the crack tip show stress readings greater than the yield point of the base material. It should be understood that such readings are

SECTION III

AND STRAIN MEASUREMENTS

Strain gages were utilized on all six specimens to measure specimen cross section stresses. Specimens AFCG-2, AFCG-3, and AFCG-4 were extensively instrumented with strain gages to measure, in addition to specimen stresses, loads transferred from the specimen through each crack gage type.

The strain gages were read at the start of testing on all specimens and, in addition, periodically throughout the test on Specimens AFCG-2, -3, and -4.

The instrumentation details of strain and crack gages are presented in Figures 3 through 8 for the six test specimens AFCG-1 through AFCG-6.

Photographs of each specimen presenting verification of instrumentation details are presented in Figures 9 through 32.

Tabulated measured dimensions of crack gages and structure flaws are presented in Tables 3 through 14.

Strain readings with the corresponding applied load values are presented in Tables 15 through 50.

Caution should be exercised in utilizing the strain readings in this volume. They are uncorrected raw test data. At longer crack lengths, strain gages close to the crack tip show stress readings greater than the yield point of the base material. It should be understood that such readings are

apparent stress values and should be recognized as being in the yield zone of the crack tip.

Other discrepancies may exist in the recorded strain data. When utilized and studied in the proper context, any irregularities, if they exist, will be recognized and should cause minimal problems.

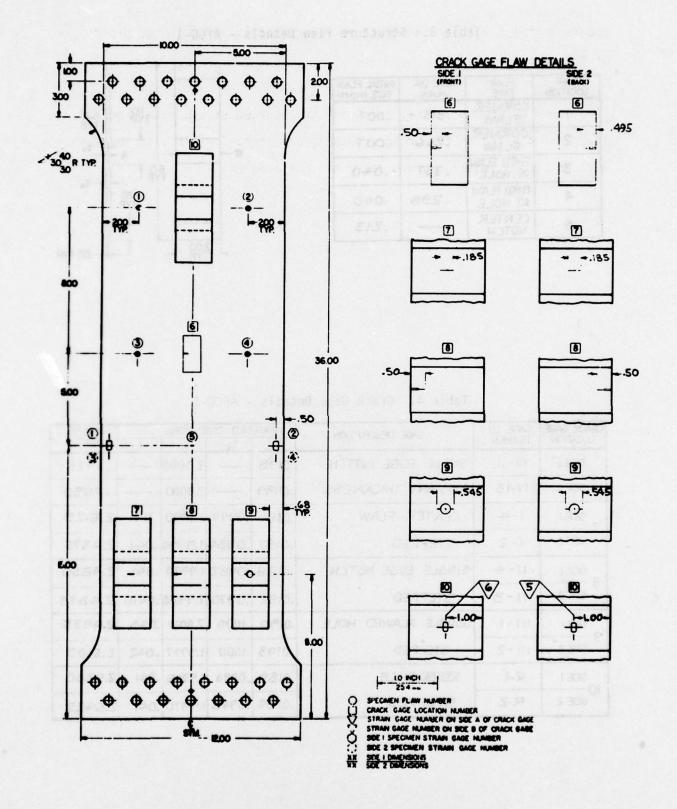


Figure 3. Instrumentation Details - Specimen AFCG-1

Table 3. Structure Flaw Details - AFCG-1

		34X211	
FLAW	FLAW TYPE	HOLE DIA.	INITIAL FLAW SIZE (INCHES)
t	CORNER	.315	-007
2	CORNER	.266	.007
3	THRU FLAW AT HOLE	. 357	.040
4	THRU FLAW AT HOLE	. 298	.040
5	CENTER NOTCH		.213

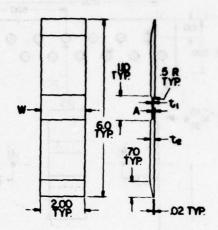


Table 4. Crack Gage Details - AFCG-1

CRACK GAGE	GAGE ID	GAGE DESCRIPTION	MEASL	FED DIN	ENSIONS		UNBOND
LOCATION	NUMBER	GAL DESCRIPTION	tı	t	W	A	LENGTH
SIDE I	1V-11	SINGLE EDGE NOTCH	800.	_	0000.S	-	.7925
SIDE 2	17-13	CONSTANT THICKNESS	.0199		0000.5		.7850
SIDE I	1-4	CENTER FLAW	.0186	.0999	0000.5	.041	2.5125
SIDE 2	1-2	STEPPED	.0187	.0984	1.9990	.04-1	2.4875
8 SIDE I	11-4	SINGLE EDGE NOTCH	8810.	.0982	1.9970	.041	2.4850
SIDE 2	11-3	STEPPED	.0192	.0970	1.9980	.0410	2.4875
SIDE	111-1	DOUBLE FLAWED HOLE	.0190	.1000	2.0000	.043	2.4925
9	111-2	STEPPED	.0193	.1000	1.9997	.042	2.5100
SIDE I	R-1	REFERENCE	.0189	-0996	1.9965	.041	7.5200
SIDE 2	R-2	STEPPED	.0184	.0998	1.9970	.041	2.5475

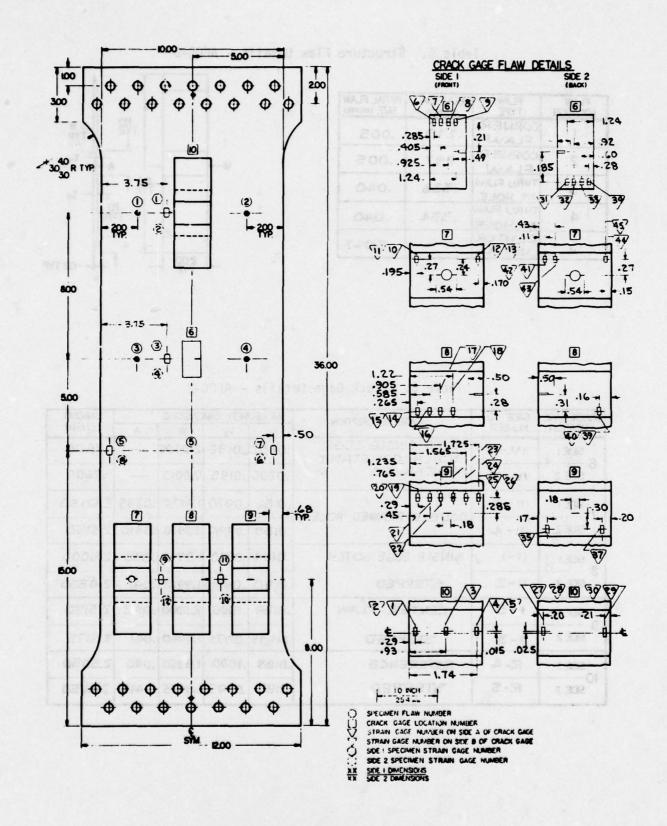


Figure 4. Instrumentation Details - Specimen AFCG-2

Table 5. Structure Flaw Details - AFCG-2

FLAW	FLAW TYPE	HOLE DIA.	INITIAL FLAW SIZE (INCHES)
1	CORNER	.270	.005
2	CORNER	.297	.005
3	THRU FLAW	.328	.040
4	THRU FLAW	.334	.040
5	CENTER		.2047

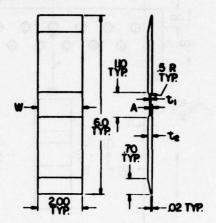


Table 6. Crack Gage Details - AFCG-2

CRACK GAGE		GAGE DESCRIPTION	MEASL		UNBOND		
LOCATION	NUMBER	GAGE DESCRIPTION	₹,	te	W	A	LENGTH
SIDE	IV-4	NOTCH CONSTANT	.0202	.0192	2.0000		.7500
SIDE 2	IV-3	THICKNESS	.0200	.0195	2.0013	_	.7600
SIDE	111-3	DALLEY S. EL BURED WOLF	.0186	.0970	1.9975	.0385	2.50 50
SIDE 2	111-4	DOUBLE FLAWED HOLE	.0189	.0990	2.0000	.0410	2.5150
SIDE	11-1	SINGLE EDGE NOTCH	.0194	.0980	1.9990	.038	2.5000
8 SIDE 2	11-2	STEPPED	.0190	.0990	1.9985	.041	2.4850
SIDE	1-5	CENTER FLAW	.0189	.1000	2.0000	.D42	7.5150
9 SIDE 2	1-3	STEPPED	.01895	.0975	1.9990	.041	2.5175
SIDE	R-4	REFERENCE	.0189	.1000	1.9950	.040	Z.5050
SIDE 2	R-5	STEPPED	D185	.0995	1.9975	.0415	2.4650

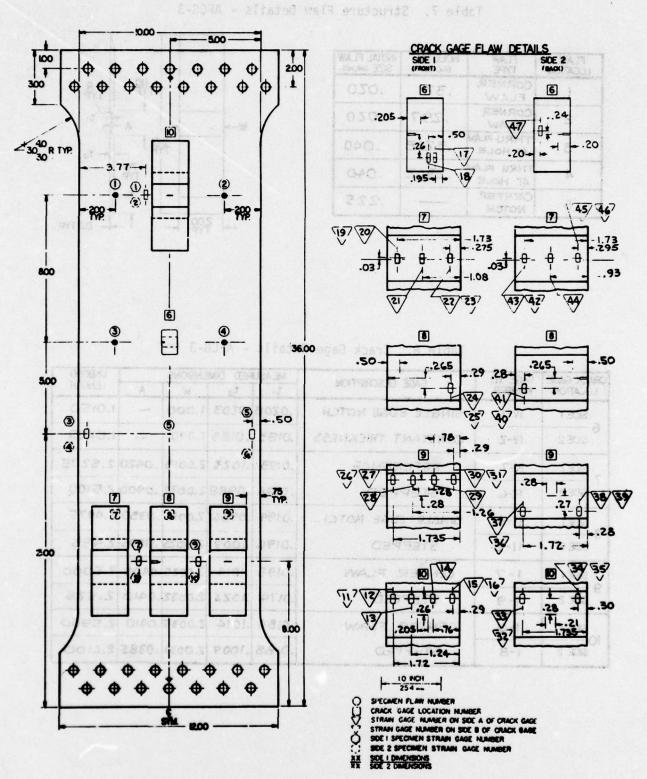


Figure 5. Instrumentation Details - Specimen AFCG-3

Table 7. Structure Flaw Details - AFCG-3

FLAW LOCATION	FLAW TYPE	HOLE DIA. (INCHES)	INITIAL FLAW SIZE (INCHES)
I 🖭	CORNER	.321	.070
2	CORNER	.297	.ozo
3	THRU FLAN	.3718	.040
4	AT HOLE	.7962	.040
5	CENTER		.225

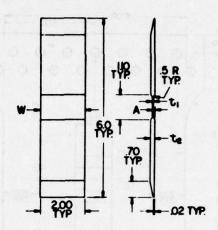


Table 8. Crack Gage Details - AFCG-3

CHACK GAGE		GAGE DESCRIPTION	MEASL		UNBOND		
LOCATION	NUMBER	GAGE DESCRIPTION	tı	t ₂	W	A	LENGTH
SIDE	/V-I	SINGLE EDGE NOTCH	.0208	.0703	1.000	-	1.0150
6 SIDE 2	IV-Z	CONSTANT THICKNESS	.0183	.0183	1.000		1.0125
SIDE	R-7	REFERENCE	.0193	.1023	2.0013	.0470	2.5275
SIDE 2	R-6	STEPPED	.0198	8860.	seaa.s	.0400	2.5100
SIDE	11-6	SINGLE EDGE NOTCH	.0199	.0986	20011	.0380	2.4975
8 SIDE 2	11-5	STEPPED	-0196	.1009	2.0025	.0405	2.495
9 SIDE I	1-7	CENTER FLAW	.0198	.1014	2.0025	.0405	2.5000
SIDE 2	1-9	STEPPED	.0179	.1026	2.0032	OLPO.	2.525
SIDE I	1-6	CENTER FLAW	.0184	.1014	2.D035	0100	2.5900
SIDE 2	1-8	STEPPED	8810.	.1009	2.0031	.0385	2.6100

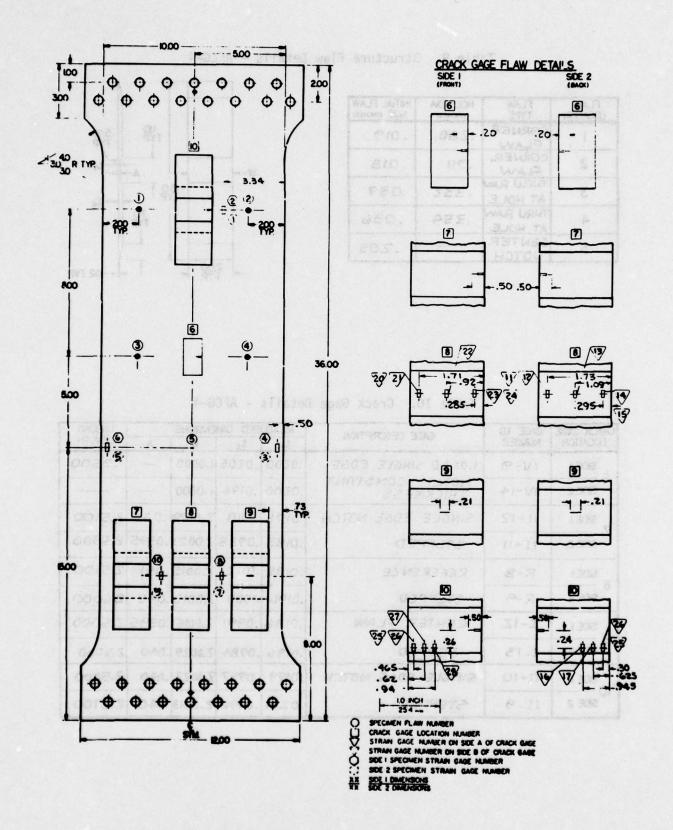


Figure 6. Instrumentation Details - Specimen AFCG-4

Table 9. Structure Flaw Details - AFCG-4

FLAW	FLAW TYPE	HOLE DIA.	INITIAL FLAW SIZE (INCHES)
1 -	CORNER	.280	.019
2	CORNER	.711	.018
3	AT HOLE	.337	.039
4	THRU PLAW	.354	.036
5	CENTER		.203

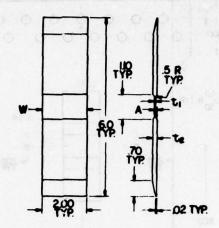


Table 10. Crack Gage Details - AFCG-4

CHACK GAGE	GAGE ID	GAGE DESCRIPTION	MEASL	RED DIN	ENSIONS		UNBOND
LOCATION	NUMBER	GASE DESCRIPTION	t,	t ₂	W	A	LENGTH
SIDE	14-9	1.0XZ.D SINGLE EDGE	0050.	.0205	1.0000	-	.9500
SIDE 2	IV-14	THICKNESS	.0200	.0194	0000.1	-	
SIDE	11-12	SINGLE EDGE NOTCH	.0176	.1010	Z.0029	.041	2.5100
7 SIDE 2	u-11	STEPPED	.0183	.0988	Z.0029	.0395	2.5900
SIDE	R-8	REFERENCE	.0195	5101.	2.0015	140.	2.5100
8 SOE 2	R-9	STEPPED	196	.1005	2.0015	.042	2.6000
SIDE	I-IZ	CENTER FLAW	.0196	.0991	2.0015	.0395	2.5000
9 SIDE 2	1-13	STEPPED	2010-	.0984	2.0029	.040	2.5000
SEE	Π-10	SINGLE EDGE NOTCH	.0199	.0997	2.0022	OAO.	2.5000
SIDE 2	11-9	STEPPER	.0201	.0996	2.0013	.040	2.5700

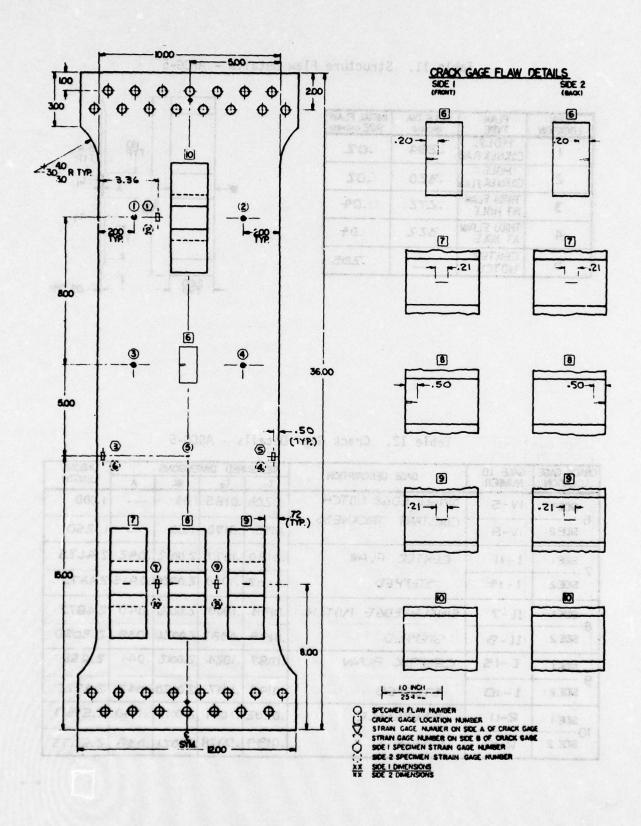


Figure 7. Instrumentation Details - Specimen AFCG-5

Table 11. Structure Flaw Details - AFCG-5

FLAW	FLAW TYPE	HOLE DIA.	INITIAL FLAW SIZE (INCHES)
1	HOLE CORNER RAM	.294	.02
2	HOLE: CORNER FLAN	.320	.07
3	THRU FLAW AT HOLE	.272	.04
4	THRU FLAW AT HOLE	.372	.04
5	CENTER		.205

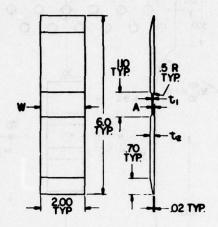


Table 12. Crack Gage Details - AGCG-5

CRACK GAGE	GAGE ID	GAGE DESCRIPTION	MEASL	RED DIN	ENSIONS		UNBOND
LOCATION	NUMBER	GASE DESCRIPTION	t,	tz	W	A	LENGTH
SIDE	14-5	SINGLE EDGE NOTCH	.0205	.0185	1.00	-	1.000
SIDE 2	1V-8	CONSTANT THEKNESS	.0195	.0190	1.00		1.1250
SIDE I	1-11	CENTER FLAM	.0180	.1027	2.0012	.042	2.4625
SIDE 2	1-14	STEPPED	SOZO.	.1000	2.0024	.0415	7.4875
8 SIDE I	11-7	SINGLE EDGE MOTCH	.0198	.1000	2.0016	.040	2.4875
SIDE 2	11-8	STEPPED	.0198	.0987	2.0076	.039	2.3050
SIDE	I-15	CENTER FLAW	.0187	.1024	2.0012	.041	2.455
9 SIDE 2	1-10	STEPPED	.0192	-1017	2.0020	.042	2.4925
SIDE I	R-11	REFERENCE	.0262	1001	2.0013	000.	Z.5150
SIDE 2	R-10	STEPPED	.0199	.0978	20021	.038	2.5475

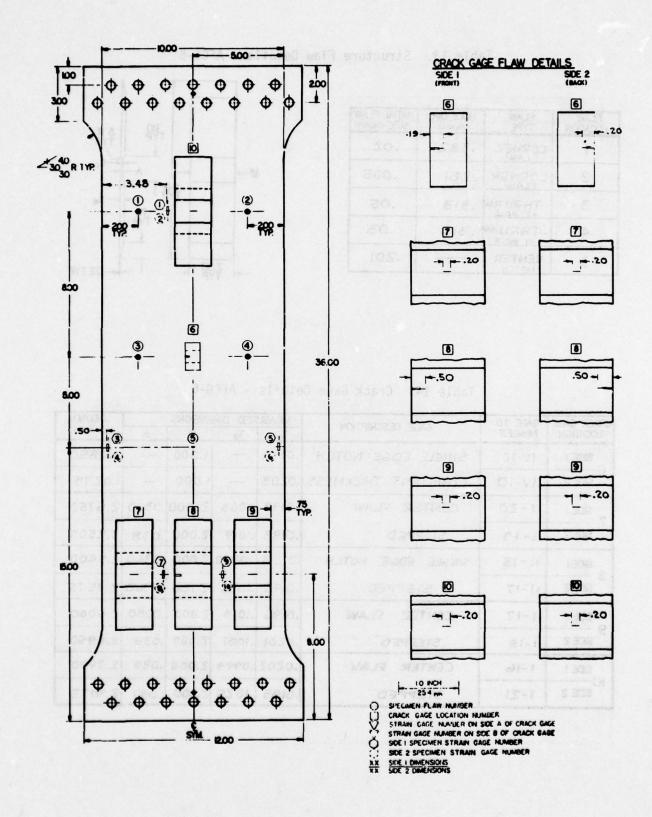


Figure 8. Instrumentation Details - Specimen AFCG-6

Table 13. Structure Flaw Details - AFCG-6

		(8)	
FLAW	FLAW TYPE	HOLE DIA	INITIAL FLAW SIZE (INCHES)
1	CORNER	.282	.02
2	CORNER	.281	.005
3	THRU FLAM	.313	.05
411	THRUM AT HOLE	.315	.03
5 -	CENTER	0.4	.201

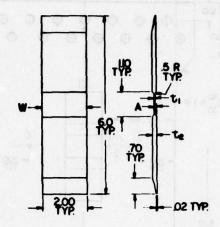


Table 14. Crack Gage Details - AFCG-6

CRACK GAGE	GAGE ID	GAGE DESCRIPTION	MEASL	RED DIM	ENSIONS		UNBOND
LOCATION	NUMBER	GASE DESCAIPTION	ti	te	W	A	LENGTH
SOEI	11-12	SINGLE EDGE NOTCH	.0198	-	1.000	-	1.0850
6 SIDE 2	IV-10	CONSTANT THICKNESS	.0203	_	1.000	_	1.0275
7 SIDE I	1-20	CENTER FLAW	.0199	.1005	000.5	.0360	2.5750
SIDE 2	1-19	STEPPED	.0193	.1019	2.000	.038	3.2500
SIDE	11-18	SINGLE EDGE NOTCH	.0233	.0990	2.000	.0360	2.5400
8 SIDE 2	11-17	STEPPED	.0193	.1018	2.000	0260.	2.1575
SIDE	11-17	CENTER FLAW	-0196	.1014	2.000	0880.	2.6000
9 SIDE 2	1-18	STEPPED	1050.	1001.	2.000	.038	2.5950
SIDE	1-16	CENTER FLAW	5050.	.0999	000.5	eE0.	2.7900
SIDE 2	1-21	STEPPED	.0193	.1025	2.000	.037	2.9175

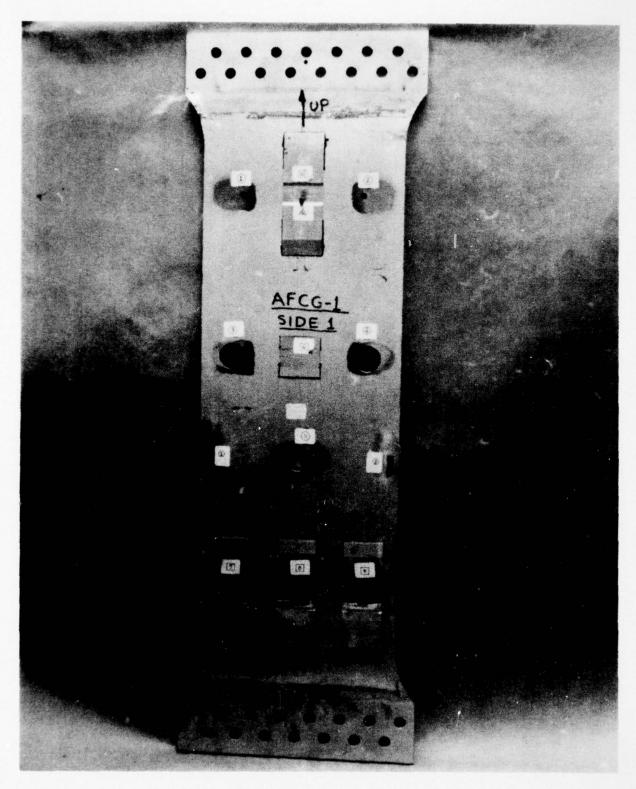


Figure 9. Photograph of Specimen AFCG-1 Side 1

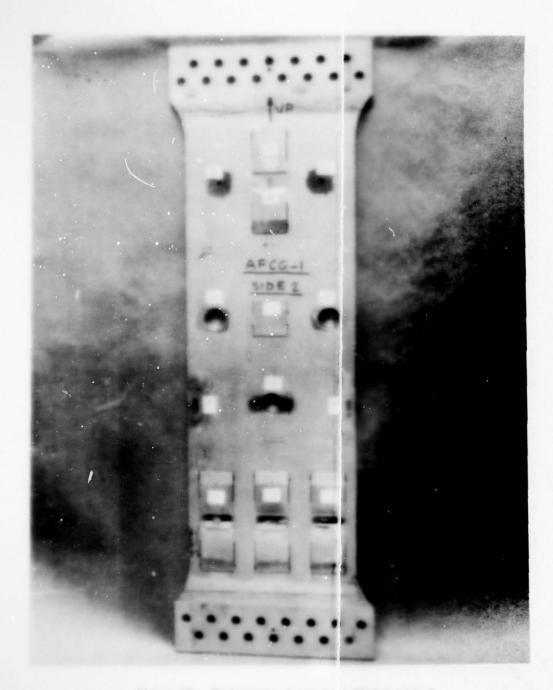


Figure 10. Photograph of Specime AFCG-1 Side 2

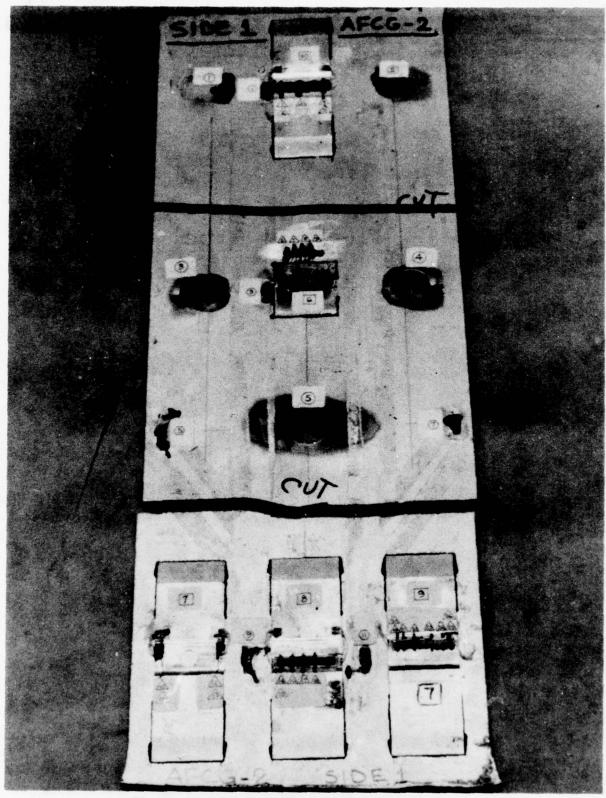


Figure 11. Photograph of Specimen AFCG-2 Side 1

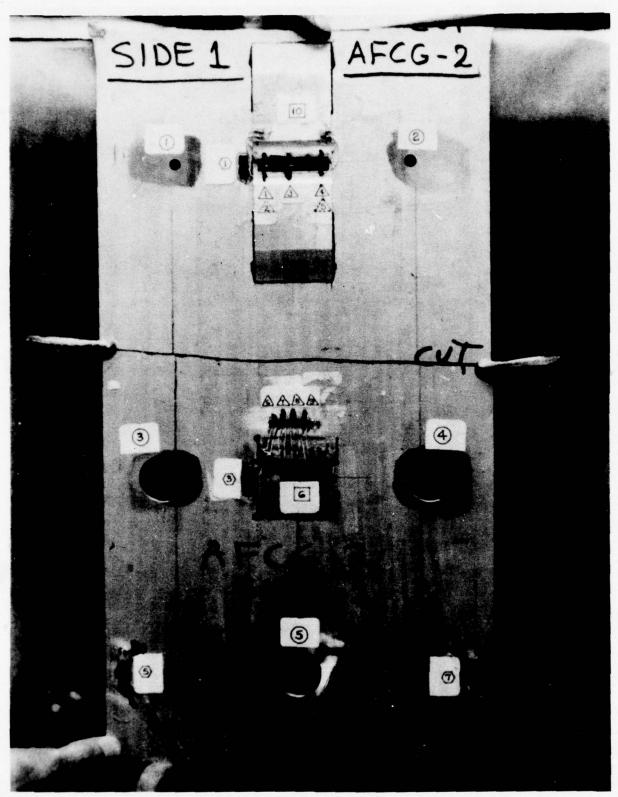


Figure 12. Photograph of Specimen AFCG-2 Side 1 Detail

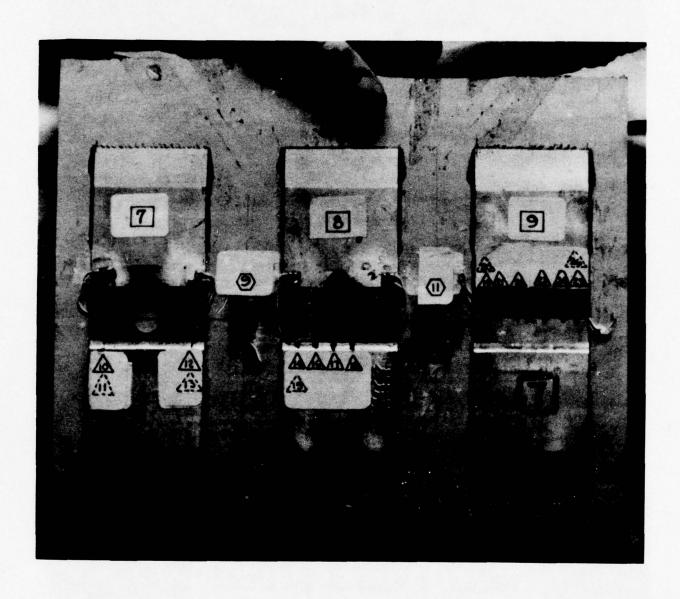


Figure 13. Photograph of Specimen AFCG-2 Side 1 Detail

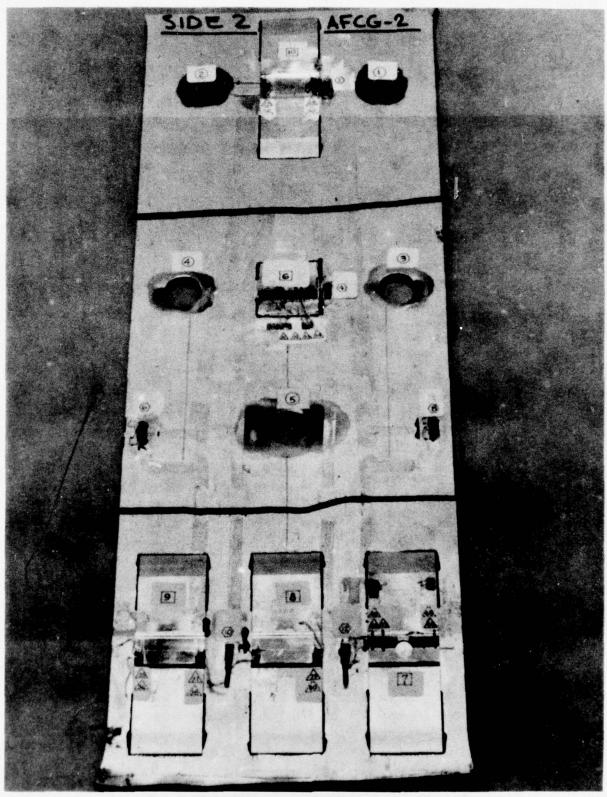


Figure 14. Photograph of Specimen AFCG-2 Side 2

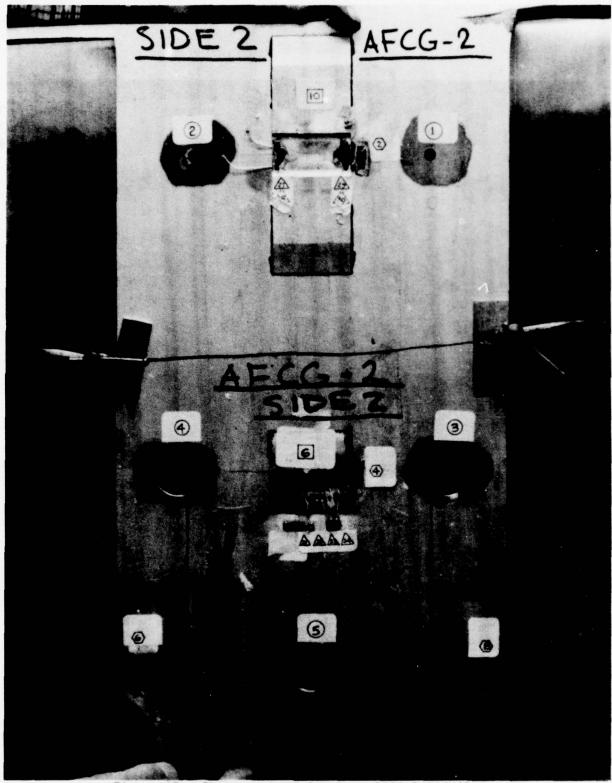


Figure 15. Photograph of Specimen AFCG-2 Side 2 Detail



Figure 16. Photograph of Specimen AFCG-2 Side 2 Detail

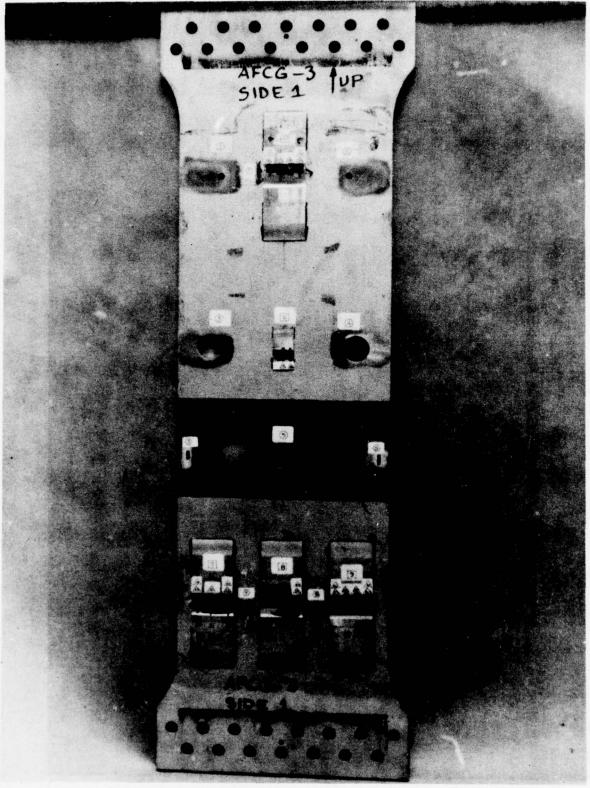


Figure 17. Photograph of Specimen AFCG-3 Side 1

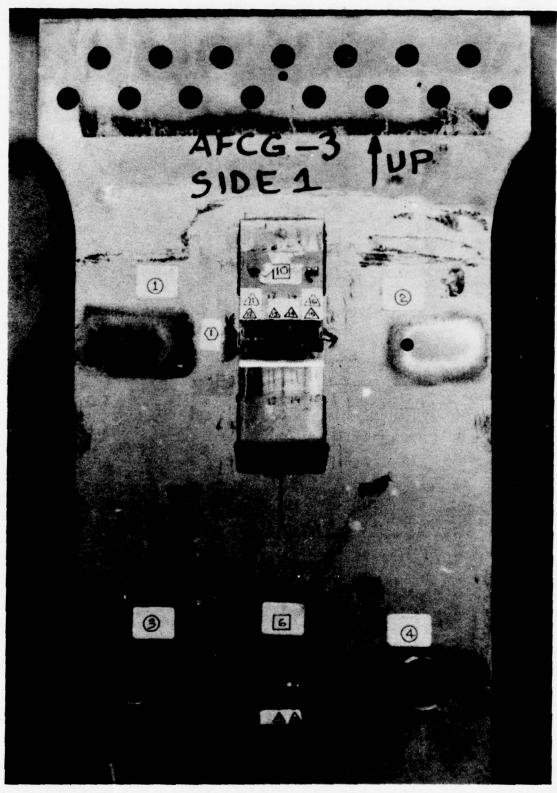


Figure 18. Photograph of Specimen AFCG-3 Side 1 Detail

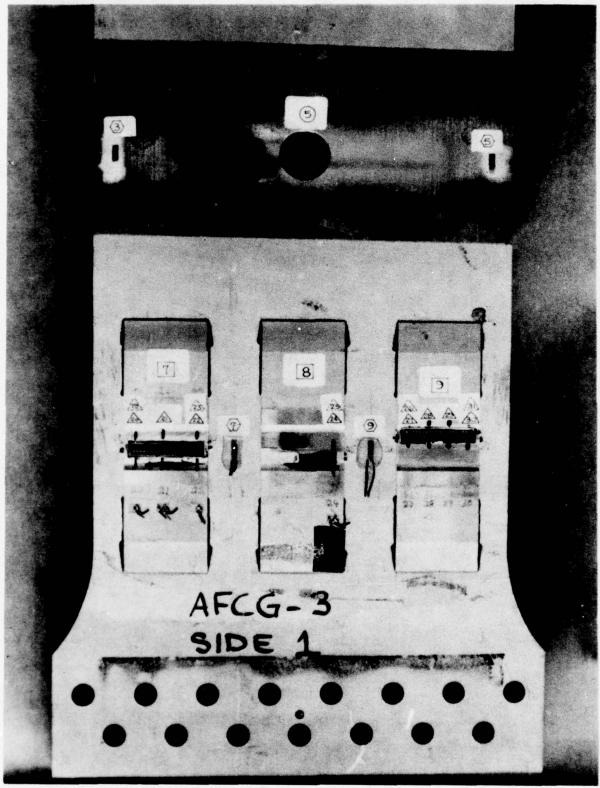


Figure 19. Photograph of Specimen AFCG-3 Side 1 Detail

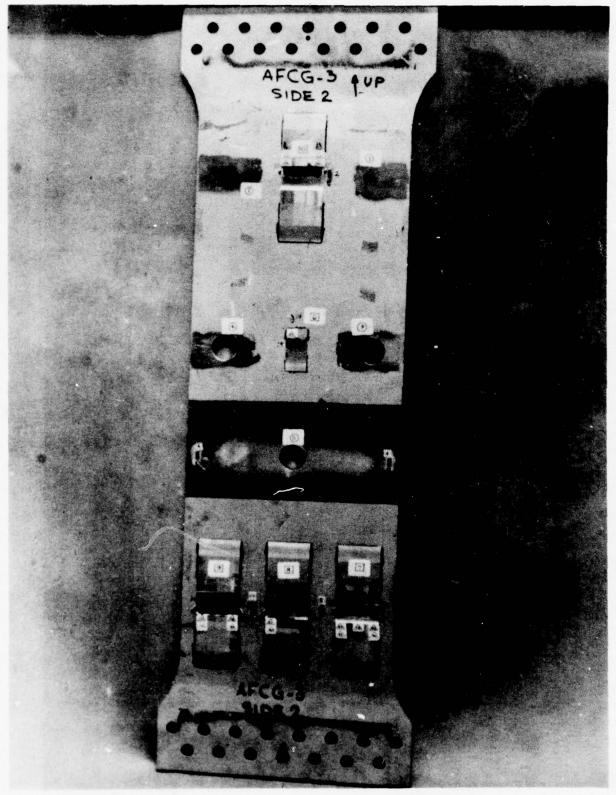


Figure 20. Photograph of Specimen AFCG-3 Side 2

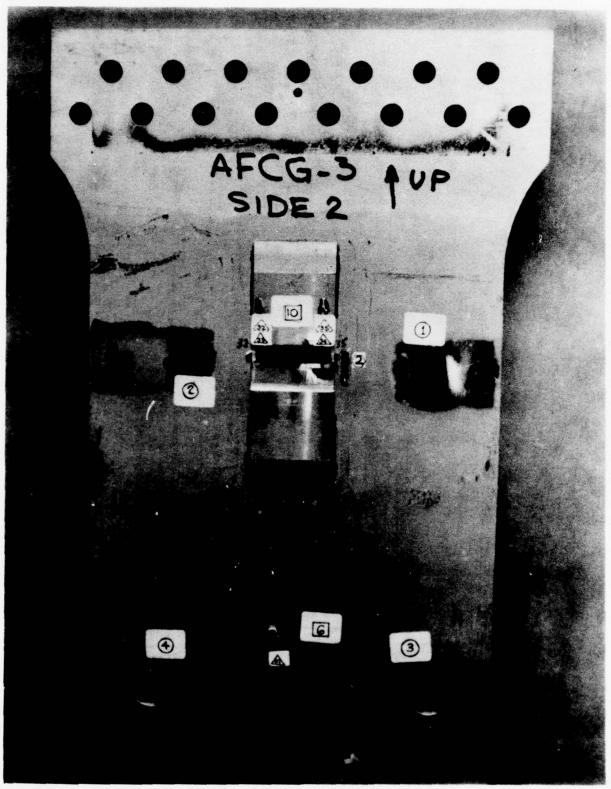


Figure 21. Photograph of Specimen AFCG-3 Side 2 Detail

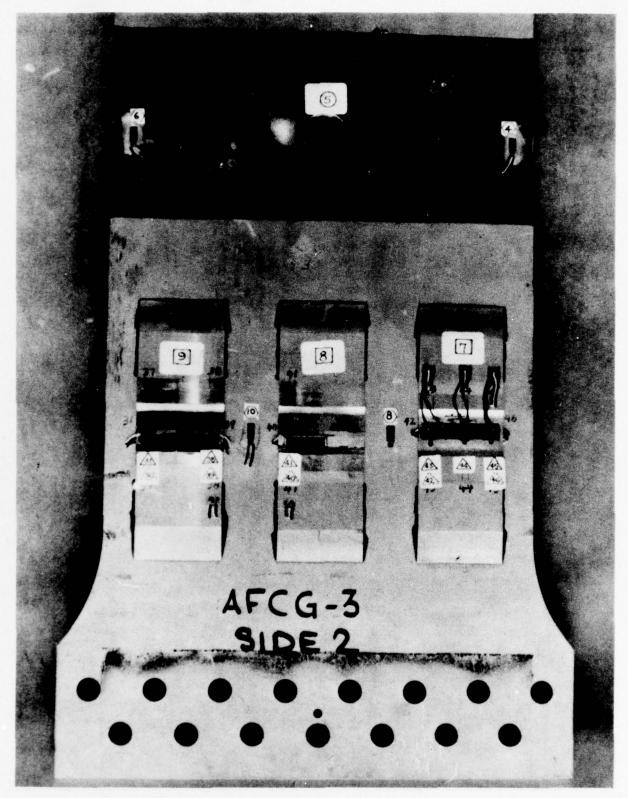


Figure 22. Photograph of Specimen AFCG-3 Side 2 Detail

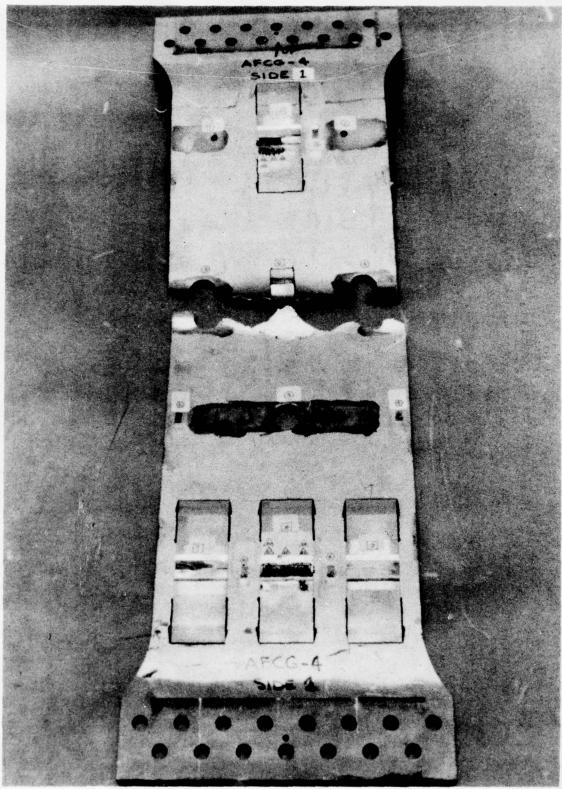


Figure 23. Photograph of Specimen AFCG-4 Side 1

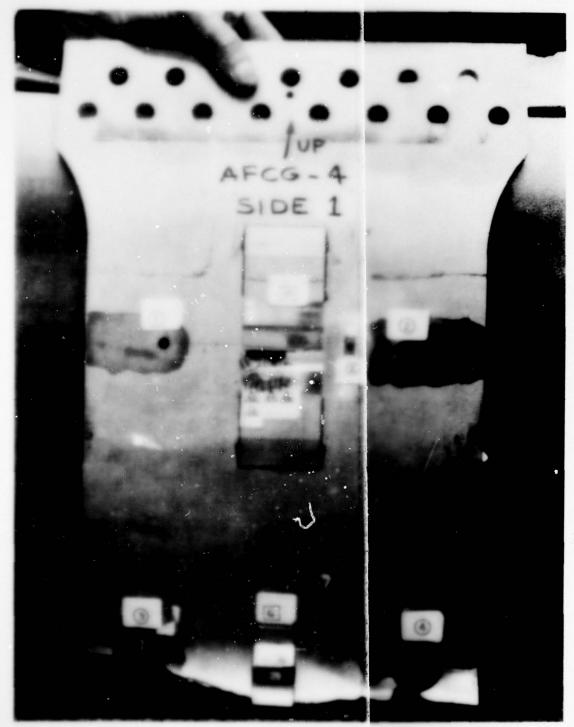


Figure 24. Photograph of Specimen AFCL-8 Side 1 Detail

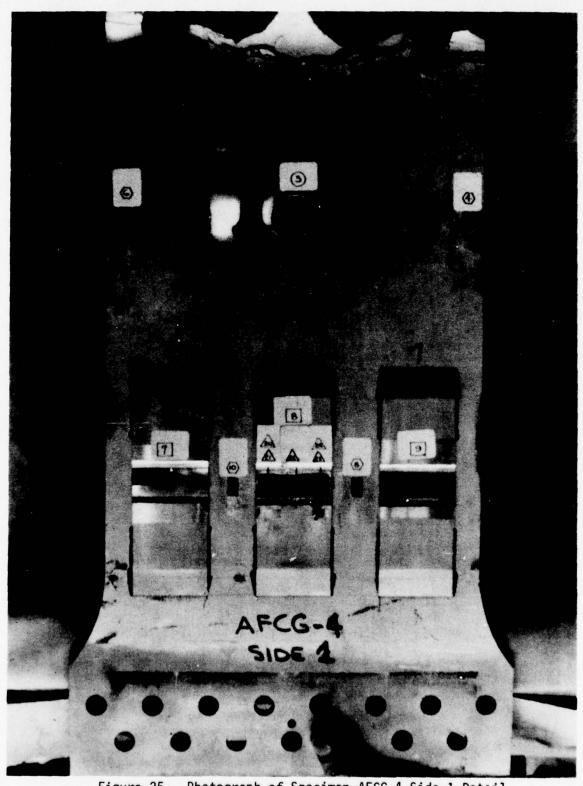


Figure 25. Photograph of Specimen AFCG-4 Side 1 Detail

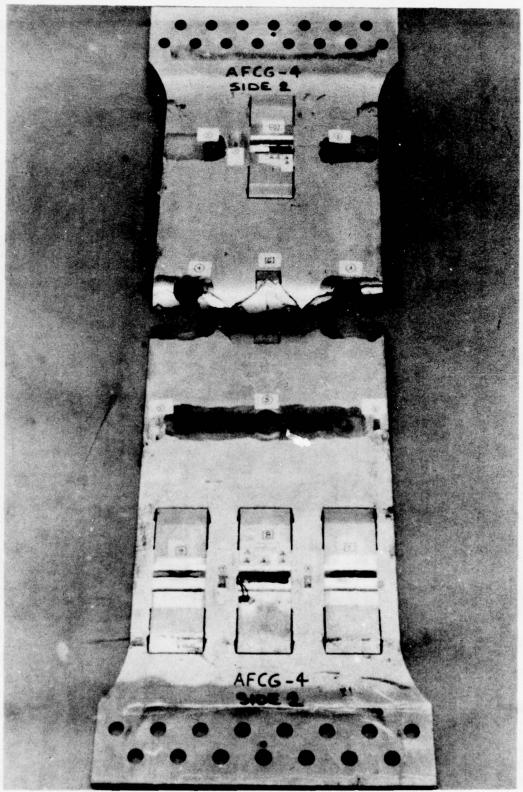


Figure 26. Photograph of Specimen AFCG-4 Side 2

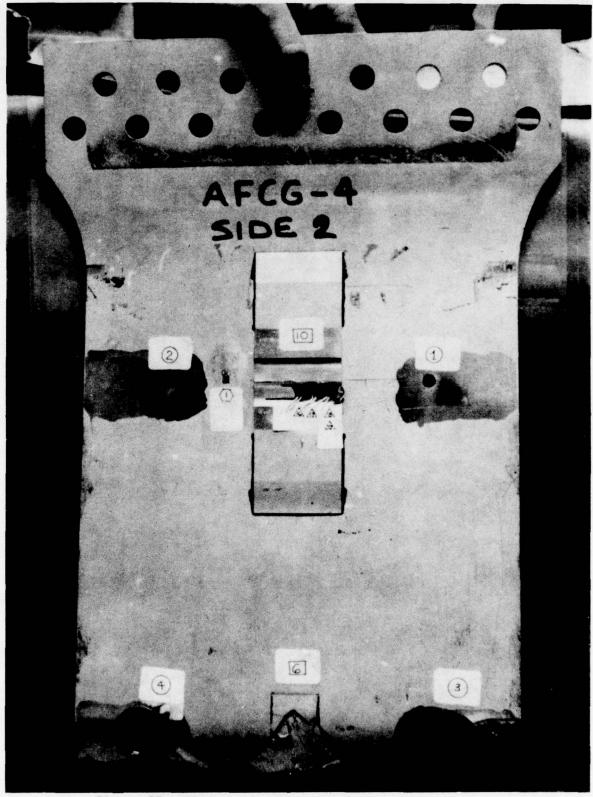


Figure 27. Photograph of Specimen AFCG-4 Side 2 Detail

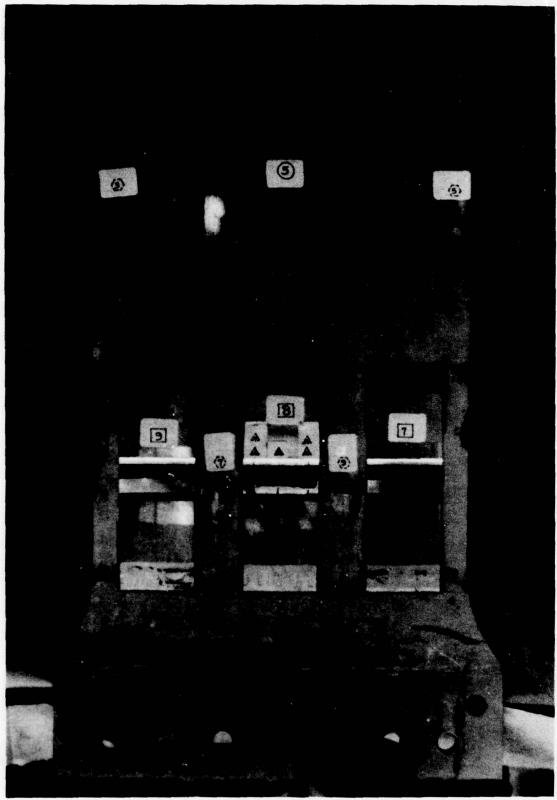


Figure 28. Photograph of Specimen AFCG-4 Side 2 Detail 42

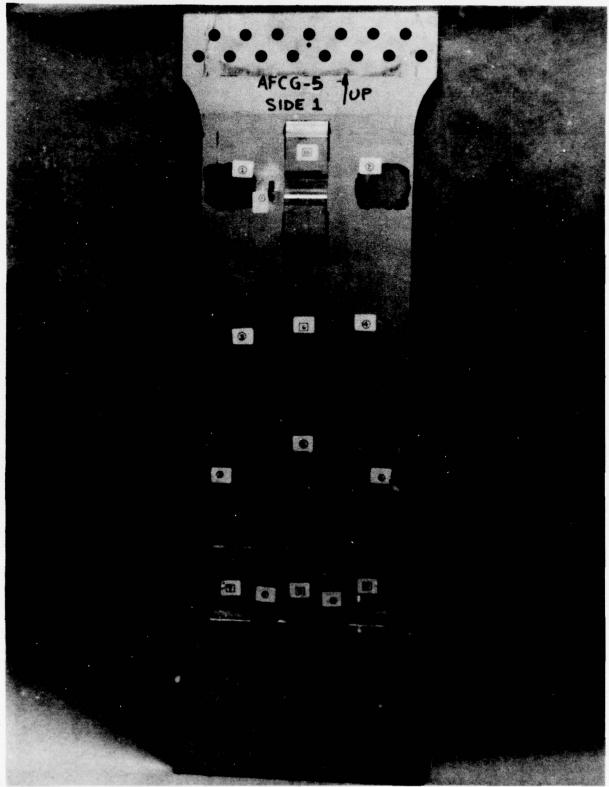


Figure 29. Photograph of Specimen AFCG-5 Side 1

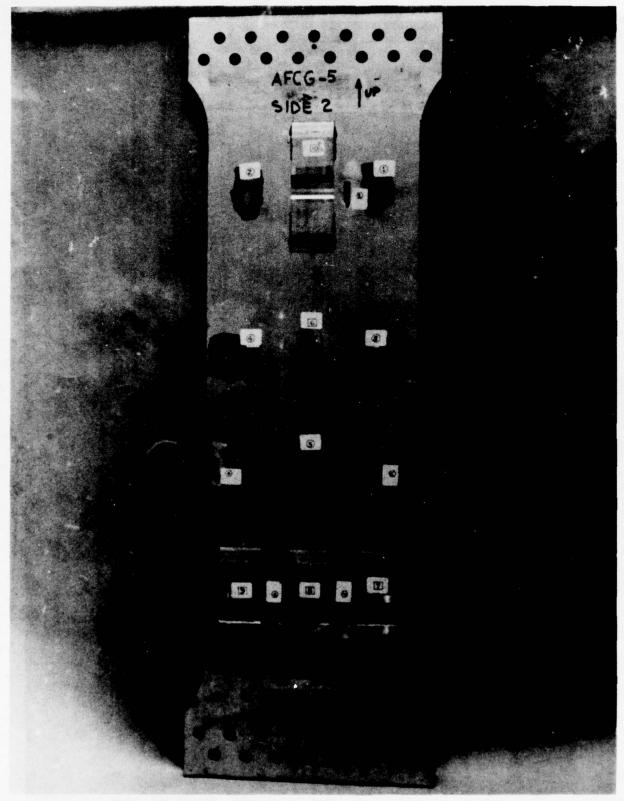


Figure 30. Photograph of Specimen AFCG-5 Side 2

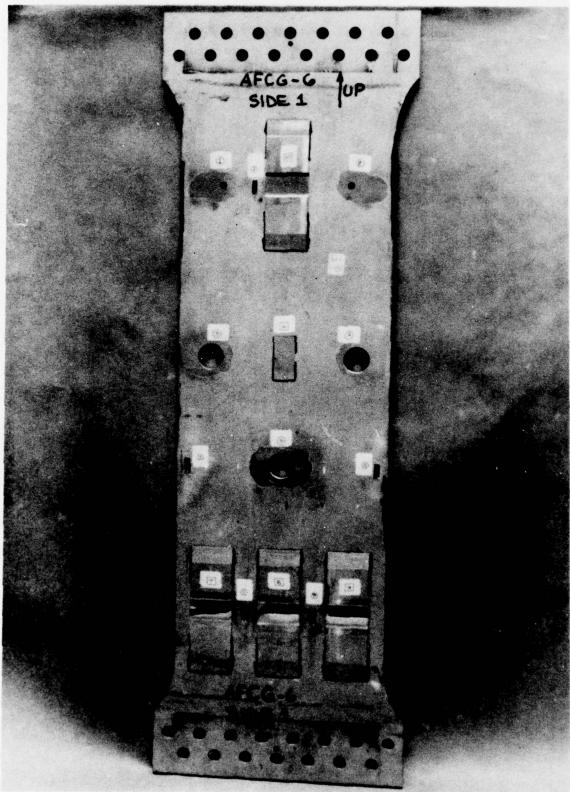


Figure 31. Photograph of Specimen AFCG-6 Side 1

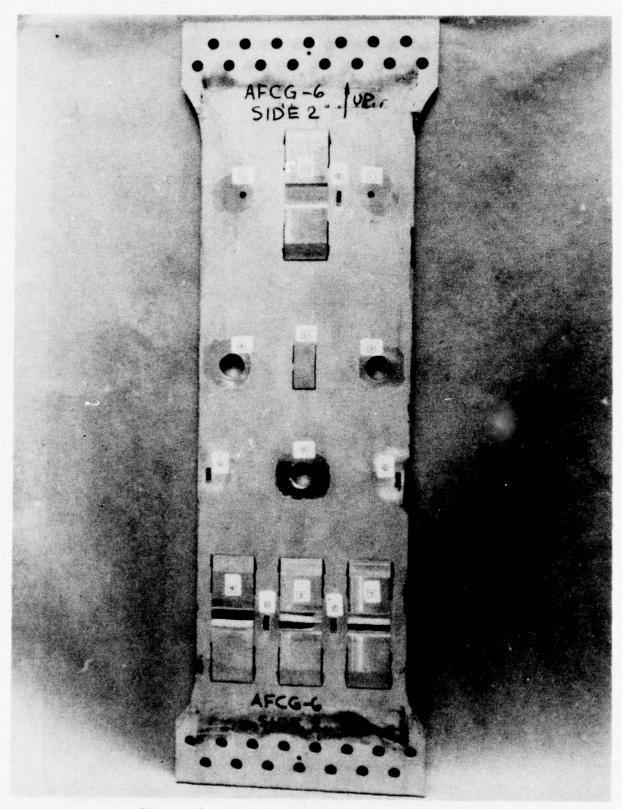


Figure 32. Photograph of Specimen AFCG-6 Side 2 46

Table 15. Strain Gage Results at Start of Test - AFCG-1

8.1. ~ BOLTED IN

H.F. ~ HANGING FREE

GAGE	3	MEASUREI	ED STRES	S (KSI)	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	LIED AX	IAL LOA	O (KIPS.				
8	O H.F.O B.	OBI	S	10	15	20	25	30	35	37.4	O B.I	
	10.	.07	1.18	2.33	3.55	4.76	6.01	7.24	8.48	3.05	10	
2	01	.28	1.37	2.55	3.73	4.93	6.17	7.42	8.69	9.32	.35	
3	10.	28	1.13	2.50	2.83	5.19	6.53	7.81	01.6	9.70	35	
4	0	04	1.35	2.70	4.05	5.36	01.9	7.99	9.32	9.97	20.	
2	0	97	1.61	4.33	7.14	9.95	12.84		18.60	18.60 20.00	90	
9	0	.94	37.9	6.63	250	12.30	15.17		20,79	22.16	.94	
200	300	S 2 2		0 0								
	200	9.50		51 1								
2	# W. W.			41.0		2000						
ta i			7 E								C A	
	8.5		200									
T				A.13 - A.14								
								200		5		
NA IN			1000									
							20.02					
5			0 0 0			7.00						
		0.000	10 mm					38.38	0.26	W 2544.25		
1			2	7								
1000	STILE	d D		200	J.				10.0		7 0	
1000		MEN	2500	\$17.00 \$1.00		8 (12)	99 <u>4</u> 1	C3.35 ()	1 1 1 K	CHAD	VIBS.	
N. S.	0.44	COM	101710	3.		30 7						
	77		250 200 300 400									

Table 16. Strain Gage Results at Start of Test - Crack Gages on AFCG-2 B. I. - BOLTED IN. HE~ HANGING FREE

STRAW	TEST		COND ITION:	TA :	START	T 0F	TEST					
GABE		MEA	SURED		STRESS (1	(KSI) A	AT APP	APPLIED	AXIBL	LOAD	LOAD (KIPS	
NO.	O H.F.	0 8.1.	5	10	15	02	25	30	35	38.5	OBI	O H.F.
-	.04	38	3.05	5.71	8.42	11.11	13.78	16.53	19.23	21.20	,50	
2	.00	.13	3.15	6.07	8.95	11.78	14.56	17.37	20,15	22.13		
3		-21	2.97	5.79	8.67	11.55	14.36	17.27	20.18	22.27	,27	
4	90.	.29	2.89	75.8	8.32	11.68	13.82	16.64	19.01	21.51	76'	
2	10.	.31	3.35	6.31	77.6	12.14	14.95	17.62	20,62	22.63	17	A
9	.63	. 20	1.42	2.68	3.97	5.26	6.52	2.82	9.10	10.02	119	
7	10.	*0.	1.27	2.50	3.76	5,03	6.28	2,55	8.81	9.72	100	
8	70.	.02	1.25	2.49	3.77	5.04	6.29	2.58	9.84	16.6	20.	
0	.62	40.	1.35	2.64	3.98	5.31	27.9	7.97	9.29	10.25	80'	
01	.02	.53	3.00	5.45	1.94	10.45	12.92	15.48	17.98	19.81	.59	
=	.03	182	3.55	6.19	8.83	11.43	13.99	19.91	19.17	21,62	1.08	
12	50.	. 22	2.65	4.91	7.24	9.55	11.85	14.21	16.55	18.25	79'	
13	41	02	2.55	80.5	7.66	10.20	13.71	15.29	17.81	19.63	40.	
14	10 -	250	2.73	4.96	7.28	9.62	11.96	14.39	18.81	1858	.83	
15	po'-	77	3.17	5.62	8.09	10.51	13.88	15.31	17.68	19.39	45,	
10	10	17	2.93	5.79	7.74	10.21	12.66	15.17	17.66	19.48	. 65	
-	1000	.65	2.93	5.28	2.70	10.13	12.54	15.03	17.50	19.29	89'	
81	70.	163	3.16	5.69	1.30	10.95	13,55	16.25	18.91	20.85	111	
19	00	.63	3.13	5.63	8.19	10.73	13.23	15.79	18.31	20.11	, 29	
02	00.	09.	3.03	5.48	8.00	10.50	12.96	15.48	17.97	19.77	.62	
12	5	.55	2.98	5.42	7.94	10.45	12.94	15.49	18.00	19.84	76.	
22	10' -	. 48	2.84	5.24	272	10,17	12.60	15.05	17.55	19.33	0%.	
23	10.	40	2.80	5.14	1.54	9.95	12.32	14,76	17.17	18.31	.37	
24	10.	. 44	2.81	5.24	1.75	10.25	12.73	15.27	17.78	19.61	, 33	

Table 16. Strain Gage Results at Start of Test - Crack Gages on AFCG-2 (Continued)

STICAL	TEST	Con	: NOITI O	1: AT	START	1 OF	TEST					
GAGE	ME	MEASURE	ED ST	STRESS	(KS1)	AT A	APPLIED		AXIAL LO	LOAD (K	(KIPS)	
5	O N.F.	OBI.	5	10	15	20	52	30	3.5	38.5	OB.I.	O N.F.
52	03	46	2.27	5.33	7.87	10.40	12.96	15.47	17.99	19.82	. 29	
92	.00	.25	2.60	4.95	7.37	9.78		14.61	17.03	18.78	61.	
12	- 103	115	2.66	5.22	7.87	10.52	13.14	15.83	19.49	26.40	20.	
82	.62	114	2.73	5:35	8.05	10.73	13.38	91.91	18.77	69.00		
62	1.06	1.25	4.08	88.9	67.6	12.46	15.18		20.66	22.62	1.28	
30	.02	113	777	5.21	7.88	10.55	13.22		18.68	39.08		
31	b2	.07	1.40	2.74	4.08	5.42	6.74		9.39	10.34		
35	101	105	1.32	2.59	3.89	5.17	6.44	2.72	8.99	96.6		
33	20	10.	1.28	2.54	3.84	2.11	6.36	177	8.89	9.80		
34	10	.67	1.36	3.66	3.97	5.27	45.9	1.84	9.11.	10.06		
35	04	67' -	76.7	3.68	10.7	1.33	10.63	13.00	15.34	17.03		
36	101	93	1.66	4.19	6.79	9.34	11.84	14.39	16.90	18.71	28	
37	10.	29	1.94	4.19	0.5.9	8.79	11.05	13.37	15.66	17.31	ph' -	
38	.64	01: -	2.35	4.84	7.38	68.6	12.37	14.89	17.38	19.18	80' -	
39	.02	- 12	2,33	4.71	7.22	9.67	12.07	14.53	16.94	18.69	10	
40	.04	\$0	2.20	4.48	6.39	9.11	11.40	13.76	16.08	17.78	11.	
14	04	32	2.49	5.32	8.20	11.02	13.80	16.64	19.42	21.43	10	
42	14	12.95	1.65	13.62	17.44	18.79	20.95	25.14	26.88	28.73	82.9	
43	19.	- ,53	2.36	5.23	8.15	11.04	13.87	16.77	19.61	21.66	25' -	
44	00	- 1.07	1.77	4.57	7.40	10.21	12.97	15.78	19.59	26,60	92	
45	10.	- ,92	1.78	4.43	2.10	9.75	12.35	10:51	17.60	19.46	11	
					The second second							

Table 17. Strain Gage Results at 8000 Cycles - Crack Gages on AFCG-2 MANSING FREE B.1. BOLTED IN

	TES	TEST CONT	DITION	80	8000 CYCLES	CLES						
8			D STRESS		AT APPL	IED AXI	(KSI) AT APPLIED AXIAL LOAD	(KIPS)				
	O H.F	0 8.1.	9	10	15	20	25	30	35	38.5	0 B.I.	0 H.F.
-		29"	3.3.3	10'9	8,65	11.33	13.99	19.91	19.31	21.24	11.	
2		18.81	24 1			1800				88/84/10	2000	
6	1000			2 20						20 55		
4		1.13	3.36	6.31	8.96	11.73	14.47	17.19	20.00	10.22	121	
5	Sec. 11	20.	3.14	6,18	9.12	12,07	14.93	17.74	20.58	65'22	20	
9		.49	1.74	3.03	4.30	5,59	6.88	8.15	9,44	10.37	75'	
7	ke and	.20	1.42	2.67	3.91	2,18	6,44	69.1	8,96	18.6	22'	
80	8.5	92'	1.48	2.74	3.99	5.27	6.55	7.80	9.09	00'01	62'	
၈		.28	1,55	2.87	4.18	5.52	6.85	8.17	9.52	10,48	18'	
01		.82	3.28	5.93	8.57	11.33	14.03	16.72	19.47	21.43	185	
113	30 20	1.15	3.86	6.68	9.46	12.29	15.07	17.80	65.02	85'22	81.1	
12		16,	3.17	5.57	7.97	10,46	16.51	15,34	17.84	89'61	86′	
13		.68	3.27	5.98	8.68	11,45	14.17	16.85	19,60	95'12	19.	
14		1.19	3,33	5,60	7.88	10,24	12,58	14.91	17.32	90'61	1.27	
(5		.65	3.20	5.72	8.17	10.66	13.10	15,50	17.93	13.65	29'	
91		1.16	3,49	10.9	8.53	11.14	13.72	16.30	18.93	20.83	61'1	
17		(,00	3.29	5.71	8.12	19.01	(3.09)	15.55	18,07	88.61	1,03	
80		.53	3,04	5,69	12.8	10.75	13.26	15,76	18.31	11.05	55'	
()		.50	3,08	5.78	8.33	11.00	(3.63	16.24	18.89	82.02	94'	
20		1.63	31	05.1				10.8			5	
12		.76	3.24	5.83	8,43	(1.10	13.73	16,36	19,04	86'07	61.	
22		.25	6.58	4.84	86'9	9, 16	11.32	13.46	15.65	17.19	92.	
23		0	2.23	4,32	6.34	8.41	1044	12.47	14,54	16,00	,02	
24		.80	3.23	5.79	8.37	11,02	13.66	16.28	18.97	20.90	18.	

Table 17. Strain Gage Results at 8000 Cycles - Crack Gages on AFCG-2 (Continued) W.F. MANGING FREE B.I. BOLTED IN

	O H.F.															0								
	0 B.I.	.64		10.	111"	1.27	0	.20	72.	1.	22.	72	19	- ,53	L)'-	50.	.27	92'	62'	12'-	20	.52		
	38.5	20.73		20.27	20.78	2249	29.02	10.53	10.12	9.97	10.16	17.51	19.39	17.65	19.51	18,82	17.90	22,69	96.02	22.49	22.24	21.73		
	35	18.82		18.35	18.85	20,55	18,65	15.6	5,20	90'6	3.25	15.74	17.50	15,95	17.66	17.08	16.22	20.57	19,00	20,40	20,12	19,74		
KIPS)	98	16.14		15,65	16.14	17.81	15,90	8,22	7.92	7.78	7.95	13.27	14.86	13.54	15,05	14.64	13.88	17.60	16.24	17.45	17.15	16.96		
CYCLES	52	13,52		13,03	13.49	12:11	13,22	6.83	999	653	89.9	16.87	12.29	61.11	12.52	12.24	11,60	14,71	(3.55	14.56	14.25	14.20		
APPLIED AXIAL LOAD	20	10.90		10.39	18'01	12.38	10,52	5.55	5.38	5.26	5,39	8.47	89'6	8.82	9.94	9,80	9.29	11.77	10.83	11.62	11.32	11.42		17.113
AT	15	8,25		7.72	8 10	9.59	7.81	4,18	60'4	3.97	4.08	509	7.03	6.42	7.32	7.34	6.95	8.78	8.08	8.63	8.35	8.59		
10 KSI)	2	5.66		5,14	545	6,85	5.21	2.86	18.2	2.71	2.79	3.71	4.45	4,08	4.78	4:92	4.69	5.87	5.41	5,68	5,46	5.84		
CONDITION ED STRESS (KS	2	3.10		2.56	2,80	4.06	2,62	1:21	1.53	1.43	1.49	1.43	1,85	1.75	2.24	2.47	2.46	2.36	2.80	2.63	092	3.12		
TEST (0 8.1.	.64		.08	61.	1, 28	01.	.20	.27	.16	.20	73	59' -	05' -	03	.05	.25	. 20	.3	- , 23	91, -	.52		
	O H.F																							
STRAIN	.0	52	92	27	28	62	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45		

Table 18. Strain Gage Results at 17800 Cycles - Crack Gages on AFCG-2 H.F. HAMSING FREE 8.1. BOLTED IN

3 3		MEASURED	STRESS	(KSI)	AL APPLIED	Æ	IAL LOAD	(KIPS)				
9	0 H.F	0 8.1.	\$	10	15	2	25	30	35	38.5	0 8.1.	0
_		55	3.17	5.86	8.48	11.13	13.78	16.45	19.09	21.0	.53	
2												
1"3												
		.98	3.42	809	8.75	11 48	14.23	17.00	13.75	-	00.1	
tr,		6	3.4	-	21.6			785	20.74	22.75	. 16	
,		69.	99		4.45	-	(3)	8.32	196	<5	99'	
7		C	15.1	-	4.01	This	203	287	906		.32	
100		35	145	80	406	EV.	-5	191	9.00	10,11	35	
O		.37	79	-	4.27	- 40	(T)	8.30	5.62	09.01	3.8	
0		- 13	2.27	4.82	7.30	980	12.31	4.8	17.28	19.04	91	
		80.	2.89	MCI	42.8	- 40	(43)	15.37	17.69	9		
12		1.16	3.46	ma	507	100	-	1757	50.35	777	1.23	
5		44	3.10	10	8.75	1147	14.17	6.84	85		42	
F/A		2	A	114		Market		MINIT	1101	17.		
15			2.17	85	8-8	3011	12.57	9	18.55	20.1	.74	
16		.95	3.20	di.	346	11.39	21.4	16.88	19.61	21.60	86	
1		52.	3.54	219	6,69	11.34	9	16.67	-	21.28	1.25	
9		-1.70	.53	14	96.	2.33	2.75	3.17	3.59	3.86	-1,66	
0		80	3.63	6.4	9.31	12.25	15.16	18.07	20.96	23.08	.75	
20												
21		.58	3.13	5.80	8,60	11.35	14.08	16.84	19.56	21.54	53	
22		1.27	154	1.10	1.53	1.96	2.44	26'2	3,40	3.72	-1.25	
23		12.1 -	18.	28.	1.22	1.62	2,04	2,47	2,89	3,17	12.1-	
24		4.2	787	661	9 . 5	10001	0861	11 11	000		1.	

Table 18. Strain Gage Results at 17800 Cycles - Crack Gages on AFCG-2 (Continued)

BOLTED IN

B. I.

HANGING FREE

New Neasure Stress (KS1) At Applied Axial Load (KII Stress (KII		TEST	TEST CONDITION:	<u></u>	-	17,800	CAC	CYCLES					
0 H.F 0 B.T. 5 10 15 20 25 95 3,50 6.34 9,20 2.14 5.07	GAGE		MEASUREI		(KSI)	AT APPL	IED AXI	AL LOAD	(KIPS)				
3.50 6.34 9,20 12.14 15,07 -10 2,44 5,03 7,60 10,24 12.88 1.12 3.96 6.76 9,49 12.23 14,96 1.14 2,77 5,36 7,95 10,61 13.30 1.37 1.69 3,05 4,19 5,48 6,77 1.37 1.63 2,92 4,19 5,48 6,77 1.37 1.69 3,05 4,19 5,48 6,77 1.37 2,06 5,00 9,66 10.86 13.08 45 2,06 5,00 9,66 10.86 13.08 45 2,06 4,76 7,50 10,28 13,05 45 2,06 4,76 7,50 10,28 13,05 45 2,06 4,76 7,51 10,00 12,47 1.5 2,59 5,06 7,51 13,08 16,37 2.5 2,76 5,50 8,38 11,30 14,20 - 2.16 5,8 3,02 4,41 5,17 12,49 15,79 1.6 3,44 6,32 9,17 12,49 15,79 2.6 3,44 6,32 9,41 12,56 15,69	NO.	I	0 8.1.	2	10	15	20	25	30	35	38.5	0 B.I.	0 H.F.
10	52		36.	3,50	6.34	9,20	12.14	15,07	18,03	96'02	11.82	.94	
-, 10	92						101	38.1					
1.12 3.96 6.76 9.49 13.63 1.12 3.96 6.76 9.49 12.23 14.96 1.12 3.96 6.76 9.49 12.23 14.96 1.14 2.77 5.36 7.95 10.61 13.30 1.37 1.63 2.95 4.19 5.75 7.10 1.37 1.63 2.95 4.19 5.75 7.10 1.37 1.63 2.96 4.16 5.45 6.77 7.10 2.5 2.96 5.00 9.66 0.86 13.05 45 2.06 5.00 9.66 0.86 13.05 35 1.96 4.76 7.50 10.00 12.47 1.10 1.25 2.59 5.06 7.51 10.00 12.47 1.10 1.25 2.55 2.56 5.05 1.36 1.30	12		3	2,44	5,03	7.60	10.24	12.88	15,53	18.18	60'02	01	
1.12. 3.96. 6.76. 9.49 12.23 14.96. 1.14. 2.77 5.36 7.95 10.61 13.30 1.37 1.69 3.05 4.19 5.46 6.77 1.37 1.63 2.95 4.19 5.46 6.77 1.36 2.06 5.00 9.66 10.86 13.28 1.35 2.06 5.00 9.66 10.86 13.28 1.36 4.40 6.89 9.44 11.61 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.5 2.59 5.06 7.51 10.00 12.47 1.6 2.84 5.95 9.17 12.49 15.79 1.7 2.84 5.93 9.17 12.56 15.69 1.86 3.44 6.32 9.41 12.56 15.69	82		,33	3.02	5,68	8.30	10.97	13.63	16.32	18'31	20,90	.31	
114 2.77 5.36 7.95 10.61 13.30 1,37 1.69 3.05 4.39 5.75 7.10 1,32 1.63 2.92 4.19 5.48 6.77 1,32 1.63 2.92 4.19 5.48 6.77 1,35 2.06 5.00 9.66 10.86 13.28 - 1,52 1.68 4.05 6.51 9.07 11.61 - 1,52 1.68 4.05 6.51 9.07 11.61 - 1,52 1.56 4.40 6.89 9.44 11.98 - 1,02 2.44 5.12 7.50 10.00 12.47 1,15 2.59 5.06 7.51 10.00 12.47 1,28 2.46 4.76 7.06 9.41 11.77 1,29 2.76 5.50 8.38 11.30 14.20 1,29 2.76 5.50 8.38 11.30 14.20 1,29 2.44 5.93 9.17 12.49 15.79 1,6 2.84 5.93 9.17 12.56 15.69	62		1.12	36'8	6.76	9,49	12.23	14,96	17.68	20,37	18.25	1,13	
7.37 1.69 3.05 4.39 5.75 7.10 7.37 1.63 2.92 4.19 5.46 6.77 7.36 1.59 2.90 4.16 5.45 6.72 7.36 2.06 5.00 9.66 10.86 13.28 7.37 1.69 4.05 6.51 9.07 11.61 7.38 2.06 4.76 7.50 10.08 13.05 7.19 2.44 5.12 7.83 10.61 13.36 7.15 2.59 5.06 7.51 10.00 12.47 7.16 2.36 6.54 9.79 13.08 16.37 7.17 7.20 2.46 5.50 8.38 11.30 14.20 7.18 2.84 5.93 9.17 12.49 15.79 7.19 7.86 3.92 4.41 5.74 7.00 7.19 7.86 3.94 6.32 9.41 12.56 15.69	30		114	2.77	5.36	7.95	19'01	13.30	10.91	18.71	20.67	1),	
.37 1.63 2.92 4.19 5,48 6.77 .35 2.06 5.00 9.66 10.86 13.28 .35 2.06 5.00 9.66 10.86 13.28 45 2.06 4.76 7.50 10.28 13.05 45 2.06 4.76 7.50 10.28 13.05 35 1.96 4.40 6.89 9.44 11.98 02 2.44 5.12 7.83 10.61 13.36 .15 2.59 5.06 7.51 10.00 12.47 .28 2.46 4.76 7.01 13.08 16.37 .29 2.76 5.50 8.38 11.30 14.20 .20 2.76 5.50 8.38 11.30 14.20 .20 2.44 5.93 9.19 12.49 15.79 .21 2.84 5.93 9.19 12.56 15.69	31		137	69'1	3,05	4.39	51.15	7.10	8.45	9.79	10,74	,38	
. 35 2.06 5.00 9.66 [0.86 13.28] - 35 2.06 5.00 9.66 [0.86 13.28] - 35 1.68 4.05 6.51 9.07 11.61 - 35 1.96 4.40 6.89 9.44 11.98 - 35 1.96 4.40 6.89 9.44 11.98 - 35 2.69 5.06 7.51 10.00 12.47 - 38 2.66 9.76 7.51 10.00 12.47 - 28 2.76 7.51 10.00 12.47 - 28 2.76 9.79 13.08 16.37 - 2.16 5.8 3.02 4.41 5.74 7.00 - 2.16 5.84 5.93 9.17 12.49 15.79 - 36 3.44 6.32 9.41 12.56 15.69	38		.37	1.63	26'2	4.19	5,48	6.77	8.05	9.32	10,24	.37	
35 2.06 5.00 9.66 [0.86 13.28	33		.32	65'	2.90	4.16	5,45	21.9	7.99	9.26	61.01	.34	
45	34		.35	90'7	5,00	9.66	98'0)	13.28	61.82	50,24	58'59	65'	
45 2.06 4.76 7.50 10,28 13,0535 1.36 4.40 6.89 9.44 1198 119802 2.44 5.12 7.83 10.61 13.36 7.15 2.59 5.06 7.51 10.00 12.47 7.28 2.46 4.76 7.04 9.41 11.77 7.29 2.76 5.50 8.38 11.30 14.20 2.16 5.58 3.02 4.41 5.74 7.00 7.16 2.84 5.93 9.41 12.56 15.69 7.16 2.86 3.44 6.32 9.41 12.56 15.69	35			1.68	4.05	651	9,07	11.61	14.20	16.78	18.67	49	
35 1.96 4.40 6.89 9.44 11.98 02 2.44 5.12 7.83 10.61 13.36 1.15 2.59 5.06 7.51 10.00 12.47 1.28 2.46 4.76 7.06 9.41 11.77 1.29 2.76 5.50 8.38 11.30 14.20 1.216 1.58 3.02 4.41 5.74 7.00 1.56 15.59 1.56 15.59 1.56 15.59 1.56 15.59 1.56 1	36			90'2	4.76	7.50	82'01	13,05	15,83	1853	09'02	14' -	
02	37		- ,35	1.96	4.40	6,89	9,44	11.98	14,53	17.07	18,91	-,36	
.28 2,46 4,76 7.04 9,41 11,77	38		20	2.44	5.12	7.83	19.01	13.36	16.14	18,90	20.88	,03	
.28 2,46 4,76 7,06 9,41 11,77 .62 3.36 6,54 9,79 13,08 16,37 .29 2,76 5,50 8,38 11,30 14,20 .2,16 .58 3,02 4,41 5,74 7,00 .14 2,84 5,93 9,17 12,49 15,79 .86 3,44 6,32 9,41 12,56 15,69	39		115	65'2	5.06	7.51	10.60	12.47	14,95	(7.39	19.16	91'	
.29	40		.28	2,46	4.76	7.06	9.41	11.77	14,13	16,49	(8.19	,31	
-2.16 5,50 8.38 11,30 14,20 -2.16 .58 3,02 4,41 5,74 7.00 .14 2.84 5,93 9,17 12.49 15.79 .86 3.44 6,32 9,41 12,56 15.69	4		29.	3.36	6.54	9.79	13,08	16.37	19.61	22.93	25,29	89.	
-2.16 .58 3,02 4,41 5,74 7.00 .14 2.84 5,93 9,17 12.49 15.79 .86 3.44 6,32 9,41 12,56 15,69	42		62'	2.78	5,50	8.38	11,30	(4,20	30.69	35.62	31,73	7.90	
. \$6 3.44 6.32 9.41 12.56 15.69 3.44 6.32 9.41 12.56 15.69	48		-2.16	.58	3,02	4,41	5.74	7.00	8.27	25'6	10,39	-2,16	
3.44 6.32 9.41 12,56 15.69	44		41.	2.84	5:93	116	1249	15.79	19,13	22.45	24.83	70'	
	45		.86	3.44	6,32	9,41	12,56	15.69	18/81	21,88	24,12	.86	
	STORY IS												
						3							

Table 19. Strain Gage Results at 26800 Cycles - Crack Gages on AFCG-2 HANGING FREE B.1. BOLTED IN H.F.

CTBATE	TEST	TEST COMDITION	:	26,800		CYCLES	S					
See.		MEASUREI	D STRES	STRESS (KSI)	AT APP	APPLIED AXIAL LOAD	TAL LOA	D (KIPS)	(
9	O H.F	0 8.1.	5	10	15	20	25	30	35	38.5	0 8.1.	O H.F.
-		.39	3,00	5.70	8.37	11.02	13.66	16.34	19.01	26'02	.39	
2				32.5		0.25	12.5		1000			
3		28.6	0					10.00	(M)		60	
4		.85	3,38	6.04	8.74	11.44	14.17	16.94	19,72	21.70	96	
5		.26	3,35	6.40	9,38	12,28	15,14	18,01	20,83	28.52		
9		55	1.79	3,09	4.39	2,66	56.9	8.26		10,47	25'	
7		62	1.50	2.77	4,03	5,29	55.9	7.83		10,00	.30	1
80		,46	1.79	3.23	4.89	6.04	LIL	89.6	(0,49	69'01	.72	
6		.23	1:21	2.90	4.25	5,58	16'9	8.27			.3	
9		-2,54	061-	-1.55	01.1 -	68	6' -	16	96' -	86	-2.50	
=		- : (8	161	62.2	\$5'2	89'2	2.70	27.2	2,75	2.76	b9° -	
12		-2,39	-1.31	167	12' -	50'	.03	20'	,03	40,	-2.35	
(3		-1.43	82'	89.	L8:	1.08	101	1.07	1.07	1.07	-1,38	
14		1.46	3.71	6.17	8.70	11.23	(3.8)	16.43	90'61	76'07	1.58	
15		1,00	3,62	6.38	11.6	11.80	14.51	17.22	19,89	21.78	36.	
5		-1.59	11.	2.24	3.28	4.21	5,11	20'9	16.9	15.7	-1,55	
17		1.43	3.86	6.68	35.6	12,43	15,34	18,28	22,12	23,32	1.47	
18		-1,39	,65	38,	.93	16'	(,00	.99	66'	86'	-1.33	
13		76	1.65	4.15	6.38	258	10,01	12,83	14.98	16.43	90'1-	
20	7 A G	6.00					109	9.0	132	2,88	I I K O	1 H C
12		90'2 -	61.	1,23	1,89	05'2	3.23	3,93	4,64	11.5	-2,03	
22		121-	10'	111	12' -	04	25' -	es' -	59	59' -	-1.16	
23		90'1 -	12	14	IT	12'-	-,23.	23	-, 20	02' -	2011-	
24		- 1,90	02.	121	16.1	2,58	3,27	3.97	19.4	5,14	-1.87	

Table 19. Strain Gage Results at 26800 Cycles - Crack Gages on AFCG-2 (Continued) BOLTED IN H.F. HANGING FREE

		O H.F.																							
		0 B.I.	96'-		61	.39	1.05	91:	.40	.42	131	27.	38	25	36	12.	.20	,43	-2,65	-2.22	-2,06	-1.75	88		
		38.5	15,84		20.03	21.04	22,24	20.78	0.84	[0,33	10,21	36	20,30	22.03	81'02	22.73	19,75	18.83	11:11	3.41	2.23	17.09	8.99		
		35	14.41		18.13	19.12	20,32	18.83	9,88	9.41	931		18.26	19.93	18.23	20,57	17.93	17.08	10,41	3.22	61/2	15,55	8,41		
	(KIPS)	30	12,34	2011	1546	1644	17.60	16.10	853	8.13	8,05	50,20	15,41	16.96	15,50	1755	(5,39	14.64	8.92	2.68	2.19	13.25	7.50		
S	APPLIED AXIAL LOAD (KIPS)	25	10,24	25	12.78	13.73	14.86	13.37	7.16	6.84	6.76	64,78	1257	13.98	12.73	14,51	12.82	(2.18	7.38	2.13	2.12	10,88	6.58		
CYCLE	IED AXI	50	8.15		10,13	11.05	12.13	10.67	5,80	5.56	5,48	54.27	5.77	11.02	(0.00	11.50	10.25	9.75	5.81	1,62	(.99	09.8	29'5		
		15	809		7.53	8.40	9,40	8,02	445	4.28	4.21	81.79	10.7	8.09	7.28	158	7.70	7.34	4.22	1.14	1.85	6.32	4,66		
26,800	(KSI)	10	3,94	16	16.4	5.72	663	5.37	3.09	86.2	26.2	127.97	4.27	5,10	4.54	5.50	5,12	4.91	122	.65	1.67	3,92	3.52		
	STRESS	5	1.55		2.33	3.06	3.84	2.77	1.73	(69)	1.57	14,90	1.79	2,24	1.96	5,65	2,60	2,58	91'	20'-	55	101	1.57		14
TEST CONDITION:	MEASURED	0 B.I.	93	Gallery Co.	81	,47	90'1	.27	,40	14	£2'	05'	39	62' -	30	1.7	02′	,39	152-	- 2.30	71.2-	01.1-	46. -		
TEST		O H.F																							
	GAGE	NO.	52	92	12	82	62	30	31	32	33	34	35	36	37	38	39	40	14	42	43	44	45	3 3 4 6 7 5	

Table 20. Strain Gage Results at 32200 Cycles - Crack Gages on AFCG-2 HANGING FREE B.I. BOLTED IN H.F.

	TEST	TEST CONDITION	;	32,	32,200	CACLES	S					
GAGE		MEASURE	D STRESS	S (KSI)	AT APP	AT APPLIED AXIAL LOAD (KIPS)	AL LOAI	(KIPS)				
NO.	0 H.F	0 8.1.	5	10	15	20	25	30	35	38.5	0 8.1.	0 H.F.
_		.40	3.10	574	8,40	01:11	13.69	16.40	19.04	96'02	.43	
2												
3								363	1601			
4		26'	3,43	40.9	8.73	11.49	14.17	16.91	19.72	11.12	96.	
5		12.	3.39	6.41	9.37	12,33	15.14	18.03	28'02	28.22	21.	
9		79.	1,90	3.19	4.48	5.80	7.07	6.40	89.6	10.62	89'	
7		13.	1.54	61.3	4,06	5:38	689	7.88	31.6	90'01	,34	
8		11.	340	7.42	23.61	16'12	17.44	49.12	19.30	16.53	1.97	
9		.34	1.63	76'7	4.30	99'5	86.9	8.35	69'6	99'01	,37	
01		-2.50	-1,84	25'1 -	80.1 -	98	C8. -	26	36' -	96' -	-2.46	
=		29'	11.2	2,38	2.66	2.75	2.78	18'2	2.83	2,85	- ,58	
12		-2.37	- 1.25	79	15	30°	.04	50'	50.	30.	-2,34	
13		-1.43	.32	79.	.86	01.1	(1.09	1.07	1.08	801	-1.39	
14		1.75	3.98	55'9	9.22	11.38	14.68	17.50	L2'02	22.36	1.85	
15		1.25	3.96	6.84	51.6	6921	15,52	18,43	21.25	23.25	12.1	
9)		1-1.67	.55	1.09	1.37	1.61	1.82	1.99	5112	2.27	- 1.63	
17		.22	2,62	5.21	7.56	9.95	12.25	14.65	6691	18.65	.22	
18		-1.18	. 79	16.	10.1	80'1	1.13	1.15	1.14	1.15	1114	
6)		1-4.77	-3.24	-2:32	91.1-	-1,49	- 1,56	711-	46'1-	+0'2-	- 4.63	
92							2.5					
12		1-2.31	-1.36	- (.19	- 1.12	60'1 -	-1.19	- 1.37	-1.53	791 -	- 2.24	
22		39	30	- ,43	58	59' -	11: -	78	98' -	89	16	
23		er	18	12	25	12' -	- ,28.	29	08' -	18' -	75	
24		171-	7.2	00	00		•	00	10	60	10 .	

Table 20. Strain Gage Results at 32200 Cycles - Crack Gages on AFCG-2 (Continued) H.F. HANGING FREE B.I. BOLTED IN

CTDATE		TEST CONDITION:	<u>.</u>	32,200		CYCLE	S					
GAGE		MEASURED	O STRESS	S (KSI)	AT APPL	IED AX	APPLIED AXIAL LOAD (KIPS)	(KIPS)	600			
NO.	O H.F	0 B.I.	5	10	15	20	25	30	35	38.5	0 8.1.	O H.F.
52		-2.04	40.	25.	.98	1.42	1.83	2.25	5,65	88.2	- 1.99	
92												
27		- ,13	2.39	4.95	7.56	10.22	18.51	15.52	18.16	20,05	51,-	
82		,43	3,07	5.70	8.38	80'11	13.70	16.43	60.61	2012	.35	
62		1,10	3.91	19.9	9.43	12.21	14.89	17.65	20.33	22.27		
30		.22	2.79	5.36	7.99	12.01	13.34	11.91	18.82	20,77		
31		.50	1.84	3.20	4.57	56,3	7.28	99.8	10.00	10.98	,43	
32		.45	1.73	308	4.31	29'5	6.88	8.19	946	10,39	.45	
33		,37	69'1	30'8	4.31	2,60	989	8.16	9,42	10.33	14.	
প্ৰ		1,20										
35		27	1.40	3.79	643	9.24	11.87	14,66	17.36	19.31	12 -	
36		-1,06	144	4.33	6.97	9.60	11.21	14.72	17.27	19.07	1.04	
37		76' -	1.31	3.80	6.26	8.74	11.10	13.58	15.98	01.71	201 -	
38		79	1.79	4.55	7.31	10.01	12.74	15.50	(8,19	80'02	59' -	
39		.37	2.80	5,36	8.03	10,73	13.35	90.91	18.69	20.53	35,	
40		25.	17.2	5,08	7.59	10.16	12,65	15,24	17.76	19.60	35.	
4		60'4-	791-	03	1,07	1.98	2.23	2.38	2,48	25'2	4004-	
45		- 2.35	11	72	- 44	18	25	- ,35	24' -	- ,43	-2:32	
43		96') -	82	10'2	2,18	2.30	2.42	2.49	2,53	25.5	-1.86	
44		1-4.21	202-	15, -	.58	1,53	1.96	1112	2,23	2,30	-4.11	
45		33	141	1,54	1.80	2,06	90'2	96'1	1,88	1.84	32	
								A CINCEPAC				

Table 21. Strain Gage Results at 37600 Cycles - Crack Gages on AFCG-2 HANGING FREE B.I. BOLTED IN

	TEST CONDITION	.:	37,600	0	CYCLES						
MEASURE		STRES	STRESS (KSI)	AT	LIED AX	APPLIED AXIAL LOAD (KIPS)	(KIPS)	The state of the s			
0 8.1.		5	10	15	20	25	30	35	38.5	0 8.1.	0 H.F.
.53		3.10	5.75	8.41	90.11	13.69	15.94	19,03	26'02	45	
									1000		
.89		3.37	5,99	8.68	11.39	14.12	24.91	59'61	21.67	.93	
.38		3.41	6.43	9.38	12,29	15.15	17.54	18'02	28.22	110	
.86		2.11	3.39	69.4	009	7.30	840	366	10.86	.88	
.37		1.58	2.84	4.11	5,38	99.9	7.74	9.22	10,15	.38	The second second
2.14		7.77	10.04	9.89	8.99	11.16	12.32	13,52	16'98	6.20	
.43		1.70	3.02	4.37	5,72	7.08	8.22	9.79	81.01.	44	
- 240		-1.79	- 1.48	- 1.03	83	98	<u>.</u> -	26' -	æ. −	-2.39	
05"		2.17	2,48	2.16	2.84	2.89	16.2	194	2.36	50	
- 2.33		- 1.22	- 53	13	20.	40'	50.	50'	. as	-2.31	
1.46		.23	,58	77.	1.00	1,00	66.	66.	.98	-1.45	
1.81		4.06	6.76	9.59	12.43	15,32	17.78	61'12	23,40	76'1	
60'		3.70	6.70	9.58	12.44	15,30	17.68	56'02	22.89	36 .	
- 1.45		. 69	.91	(.11	1.27	1.39	1.46	1,48	1.51	-1.42	
- 1.58		.64	1.93	2.81	3,66	4.49	2112	6.07	6.62	-1.56	
- 1,08		. 84	.95	1.09	1.19	1,28	1.34	1,36	1.37	-1.05	
+1'1 -		-8,03	-5,18	- 3,04	- 1.64	11.1-	91.1 -	-1.76	- 1.76	-11.11	
						6.3					27 7 10
- 6.45		-4.07	1-2.77	- 1.93	-1.32	- 1.46	- 1,52	-1,53	- 1,54	- 640	
- 1.34		11	79	76	02	100	88	- ,89	- ,90	- 1.34	
es		JI	41	1	6 - 1	12' -	- ,23	42' -	25	- ,49	
- 1.00		,15	71.	=-	70.	0).	=-	. 10	0	76' -	

Table 21. Strain Gage Results at 37600 Cycles - Crack Gages on AFCG-2 (Continued) H.F. HANGING FREE B.I. BOLTED IN

STRAIN		MEASURE	ED STRES	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	AT APPL	IED AXI	AL LOAD	(KIPS)				
9	0 H.F	0 8.1.		01	15	202	25	30	35	38.5	0 B. I.	O H.F.
52		- 1.40	62' -	01	11.5	25.	.33	.36	.37	.37	-1.39	
26			Care	3.1	190	CAN	0 11 2			40.1	W (1 C) W	
27		- ,07	2.39	4.94	7.55	[0,17	12.80	15,04	18.12	20,04	91: -	
28		15.	3,05	69'5	8:35	10.11	13.68	15,94	30'61	86.05	.34	
62		1,16	3,90	179	945	12.15	14.87	17.16	20,30	22.24	1,06	
8		.31	2.76	5,34	7.96	10,63	13.32	15,59	18.76	71.02	01,	
3		,62	1.92	3,28	99.6	20'9	7.39	8.54	10.12		80,	
8		اح.	1.76	3.05	4.35	5,64	6.94	8,02	55'6	10,45	.49	
33		,53	1.82	3.11	4.40	5.68	6.97	8,05	9.53	10.45	.49	
34		3.02									4.03	
35		- 1.86	.20	82'2	4.20	6.04	7.87	9,43	11.56	12,81	-192	
36		- 2.42	20.	65'2	4.16	29'5	11.7	8,36	10.07	11.07	15.2-	
37		- 2.36	75	62'1	2.38	3.44	15'5	5,42	6.7	7.43	- 244	
38		- 2.84	53	1.14	2.34	3,41	4.45	5,32	6.47	7.12	-2.83	
39		79'	3.05	21.5	65,8	11,43	14,24	16.63	1861	21.94	09.	
40		.72	2.89	2,36	8,05	10.74	13,45	15,74	18.30	20,88	12'	
4		-4.22	76'1-	82	101	2,03	2.28	2,40	2.53	2,57	14.18	
42												
43		-1.97	02.	2.00	2.24	142	2,55	2.59	Se3	2,63	-1.93	
44		-448	- 2.23	75	49.	1.62	21,5	2,25	240	2.48	- 4.49	
45		25	1.39	1.50	1.72	00'2	90'2	1.97	1.87	1.82	26	
		A		N CKC			10 F 4 01					
	100	5.00000										

Table 22. Strain Gage Results at 55000 Cycles - Crack Gages on AFCG-2 HANGING FREE B.I. BOLTED IN

CTBATE	TEST	TEST CONDITION	::	55,000		CYCLES						
GAGE		MEASUREI	0	STRESS (KSI)	A	LIED AX	IAL LOA	APPLIED AXIAL LOAD (KIPS)	1			
.O.	0 H.F	0 B.I.	5	10	15	02	25	30	35	38.5	0 B.I.	0 H.F.
-		.10	2.66	5,35	8.03	10.70	13,37	16.06	18.76	69'02	20.	
2												
2												
4		3	3.29	601	8.74	11.51	14.28	17.06	19.86	21.87	.83	
Ŋ		1.31	4,36	7.36	10,25	13.13	16.00	18.81	29.12	19.82	1.09	
G		,64	16/1	3.22	4.53	5.86	7.20	8.53	9.87	10.82	.64	
7		.18	141	2.68	3.95	5,24	559	7.84	9,15	10,07	<u>e</u> .	
80											1	
6		.20	1.48	2.83	4.22	5.59	6.97	8.35	11.6	10,70	.23	
(0)		-3,10	- 1.77	01.1 -	221-	۶6	Se	86	101-	- 1.03	-305	
		-1.79	1.04	60'2	2:37	2.50	2.54	2.56	2.58	65'2	17.1-	
12		-2.44	- 1.27	29' -	02' -	30' -	40	1	03	1.03	- 2.42	
13		1-1.26	19'	1.2.1	1,45	1.70	1.70	69'1	1,69	1.70	- 1.16	
14		-1.20	58	14	02' -	20' -	717	.23	.30	62.	- 1.17	
S		-1.17	49	.75	11.	99.	65'	64'	44	44	-1,15	
91		-2.20	0	.64	98'	1,03	1.16	1.20	61'1	61'1	-2,13	
17		-249	- ,23	.38	158	69.	.19	98.	88'	88'	-244	
<u></u>		-1.10	<i>S</i> 3.	01.	.86	26,	1,03	90'1	50'1	1001	-1,04	
61		-12,39	-8.83	bb'5-	10'8-	281-	161-	16:1-	16')-	16'1-	-12.32	
20	111111111111111111111111111111111111111	0.000								100	1 3 3	
17		- 9,60	92.9 -	-3.54	-2,44	161.	50'2 -	- 205	- 2,05	- 2,05	- 5.50	
22		20'2-	- (,30	- (.13	-1,16	-1.13	22.1 -	121 -	1.27	82.1 -	90/2 -	
23		55	46' -	- ,52	19	62	19' -	129	89' -	89	95' -	
\$2		74	0	ک٥, -	12	٦. اح	41	4), -	41	b1' -	- 49	

Table 22. Strain Gage Results at 55000 Cycles - Crack Gages on AFCG-2 (Continued) H.F. HANGING FREE B.I. BOLTED IN

New Neasure Stress (KS1) At Applied Axial Load (KIPS)			TEST CONDITION:		55,000		CYCLES					100	
OH.F OB.I. 5 10 15 20 25 30 35 35 35 35 35 35 3	GAGE		MEASURE		S (KSI)	AT APP	LIED AX	TAL LOAD	(KIPS)				
11	NO.	0 H.F	0 B.I.	5	10	15	20	25	30	35	38.5	0 B.I.	0 H.F.
65 .95	52		28	-	61		.05	9	1		7:	86	
65 9.4 9.5 11.2 12.6 15.3 18.02 08 2.82 5.67 8.47 11.29 14.09 16.66 08 2.82 5.67 8.47 11.29 14.09 16.66 08 2.82 5.67 8.47 11.29 14.09 08 2.82 5.12 7.12 10.41 08 2.84 5.12 7.12 10.41 29 1.70 3.71 4.63 6.06 7.49 8.89 10.31 - 2.13 1.44 3.50 4.40 5.73 7.06 8.38 9.70 - 2.13 2.15 2.15 2.15 2.15 2.15 - 2.13 2.15 2.15 2.15 2.15 2.15 - 2.13 2.15 2.15 2.15 2.15 - 2.14 2.15 2.15 2.15 2.15 - 2.15 1.15 2.15 2.15 2.15 - 2.17 2.15 2.15 2.15 - 2.17 2.15 2.15 2.15 - 2.17 2.15 2.15 2.15 - 2.17 2.15 2.15 2.15 - 2.17 2.15 2.15 - 2.17 2.15 2.15 - 2.17 2.15 2.15 - 2.17 2.15 2.15 - 2.17 2.15 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.17 2.15 - 2.18 2.15 - 2.19 2.15 - 2.10 2	92												
74 3.29 5.94 8.58 11.26 13.97 16.66 19.37 16.66 19.37 2.08 2.82 5.67 8.47 11.29 14.09 16.86 19.64 13.62 2.54 5.12 7.72 10.41 13.14 15.87 18.64 13.65 1.72 2.54 5.12 7.72 10.41 13.14 15.87 18.64 13.65 1.73 5.66 7.49 8.89 10.31 2.3 1.34 1.70 3.07 4.40 5.73 7.06 8.38 9.70 2.35 1.52 1.52 1.52 1.52 1.53 1.54 1.57 1.69 1.57 1.69 1.57 1.50 1.57 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50	12		39' -	961	4.58	7.22	16.6	15,51	15.31	18.02	76'61	56	
08	28		.74	3.29	5.94	85'8	92.11	13.97	99.91	19.37	21.31	35'	
7.2 2.54 5.12 10.41 13.14 15.87 18.64 7.36 1.78 3.0.1 4.63 6,06 7.49 8.89 10.31 7.29 1.64 3.00 4.33 5,66 7,00 8.32 9,65 7.39 1.5295 - 462229322927.32927.32927.32927.32927.42229322927.32927.2 - 1.22 - 1.46 1.07 1.09 7.345 - 2.72 - 1.87 - 1.22 - 1.46 1.07 1.09 7.345 - 2.72 - 1.27 - 1.22 - 1.46 1.07 1.09 7.345 - 2.72 - 1.36 - 3.26 - 3.4734343434 7.25 - 1.25 - 1.2741 1.241 1.2 1.29 7.347 - 3.39 - 1.1371 1.90 2.17 2.29 2.38 7.348 - 1.17 1.20 1.21 1.20 1.31 2.24 7.349 - 2.35 2.35 2.36 3.10 2.35 2.36	ຄ		80	28.2	2,67	8.47	11.29	60.4	16,86	19.64	21.62		
36 1.76 3.01 4.63 6.06 7.49 8.89 10.31 .29 1.64 3.00 4.33 5.66 7.00 8.32 9.65 .34 1.70 3.07 4.40 5.73 7.06 8.38 9.70 .34 1.70 3.07 4.40 5.73 7.06 8.38 9.70 -2.39 -1.52 -3.2 -3.2 -3.2 -3.2 -2.13 -3.45 -2.12 -1.22 -1.22 -1.46 1.07 1.09 -3.45 -2.12 -1.87 -1.22 -1.46 1.07 1.09 -3.45 -2.12 -1.87 -1.22 -1.46 1.07 1.20 -3.45 -2.12 -1.37 -3.46 1.07 1.21 1.21 -3.45 -2.12 -1.13 -3.45 -3.46 3.10 2.95 -3.46 -3.36 -1.17 -1.68 2.17 2.29 2.38 -3.44 -3.36 -1.17 -1.61 1.90 2.11 2.24 -3.44 -3.36 -1.17 -1.61 1.90 2.11 2.24 -3.45 -3.36 -1.17 -1.61 1.90 2.95 2.86 -3.16 -3.36 -3.36 2.86 3.10 2.95 2.86 -3.17 -3.26 2.36 2.86 3.10 2.95 2.86 -3.17 -3.26 2.36 2.86 3.10 2.95 2.86 -3.17 -3.26 -3.26 2.86 3.10 2.95 2.86 -3.17 -3.26 -3.26 3.10 2.95 2.86 -3.17 -3.26 -3.26 3.10 2.95 2.86 -3.17 -3.26 -3.26 3.10 2.95 2.86 -3.17 -3.26 -3.26 3.10 2.95 2.86 -3.18 -3.26 -3.26 3.10 2.95 2.86 -3.18 -3.26 -3.26 3.10 3.10 -3.26 -3.26 3.10 3.10 3.10 -3.26 -3.26 3.10 3.10 3.10 -3.26 -3.26 3.10 3.10 3.10 -3.26 -3.26 3.10 3.10 3.10 -3.26 -3.26 3.10 3.10 3.10 -3.26 -3.26 3.10 3.10 3.10 -3.26 -3.26 3.10 3.10 -3.26 -3.26 3.10 3.26 3.10 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.26 -3.26 3.10 3.26 -3.27 -3.26 3.10 3.26 -3.27 -3.27 3.26 -3.27 -3.26 3.10 3.26 -3.27 -3.26 3.10 3.26 -3.27 -3.26 3.10 3.26	30		.12	2.54	5.12	7.72	19,01	13,14	15.87	18.64	20,60	-,13	
2.59 1.64 3.00 4.53 5.66 7.00 8.32 9.00 3.4 1.70 3.07 4.40 5.73 7.06 8.38 9.70 -2.39 - 1.5295 - 4622293229 -2.1349 .22 .61 .95 1.04 1.07 1.09 -3.45 - 2.72 - 1.87 - 1.22 - 1.46 - 1.50 - 1.50 -14.68 - 1.105 - 7.36 - 3.6703 1.24 1.27 1.29 -2.03 .14 .95 1.1572 1.46 1.43 1.44 -2.21 - 1.29 - 1.1372 1.48 2.17 2.29 2.38 -3.4474 1.52 1.78 1.90 2.17 2.29 -3.443.50 - 1.17 1.0 1.21 1.90 2.95 2.86	31		,36		12.8	4.63	909	7.49	8.89	10.31	11.32		
-2,39 -1,5295 - 4622293229 -2,1349 .22 .61 .95 1.04 1.07 1.09 -2,45 - 2,12 - 1,22 - 1,22 - 1,46 - 1,07 1.09 -14,68 - 11,05 - 7,36 - 3,6503 1.24 1.27 1.29 -2,03 .14 .92 1.16 1.37 1.42 1.43 -2,21 - 1,29 - 1,1372 - 41343434 -2,21 - 1,29 - 1,1372 - 413434 -3,4477 1.52 1.90 2.17 2.29 2.38 -3,4477 1.52 2.58 2.86 3.10 2.95 2.86	32		62.		3.00	4.33	2,66	2,00	8.32	3,65	10,60	62.	
-2,39 - 1,5235 - 4622293529 -2,1349 .22 .61 .95 1.04 1.07 1.09 -3,45 - 2,12 - 1,87 - 1,22 - 1,46 - 1,50 - 1,50 -14,68 - 1,105 - 7,36 - 3,4503 1.24 1,27 1.29 - 2,03 .14 .95 1,16 1.37 1,42 1,43 1,44 - 2,21 - 1,29 - 1,1372413434 - 4,79 - 2,5664 .77 1,88 2.17 2,29 2,38 - 3,4474 1,52 1,71 1,18 2,10 2,95 2,46 - 5,74 - 3,38 - 1,17 1,10 1,21 1,90 2,95 2,86	33		.34	1.70	3.07	4.40	5.73	7.06	8.38	9.70	10,64		
-2,39 -1,52 - 35 - 46 - ,22 - ,29 - ,32 - ,29 - ,37 - ,27 -	34				2								
-2.7349	35		-2,39	1	36	96 -	25	62	- ,32	29	30	-241	
-345 - 2,72 - 1,87 - 1,22 - 1,46 - 1,50 - 1,50 -14,68 - 11,05 - 7,36 - 3,45 - 0,3	36		-2.73	1	,22	19.	36.	1.04	1,07	60')	60'I	89.2 -	
- 2,03	37		-345	1	-1.87	-1.22	- 1.22	1,46	- 1.50	-1,50	- 1.52	-3,66	
- 2,03 . 14 . 92 1.16 1.37 1.42 1.44 1.44 1.42 1.44 1.49 2.17 2.29 2.38 2 - 4.79 - 2,56 - 64 . 77 1.88 2.17 2.29 2.38 2 - 3,44 - 7,7 1.88 2.17 2.29 2.38 2 - 3,44 - 7,7 1.52 1.90 2.95 2.38 2 - 5,74 - 3,38 - 1,18 2.32 2.58 2.86 3,10 2.95 2.86 2.86 2.90 2.90 2.95 2.86 2.90 2.95 2.96 2.90 2.95 2.96 2.90 2.95 2.96 2.90 2.90 2.90 2.90 2.90 2.90 2.90 2.90	38		-14.68	-	1	- 3.65	03	1.24	1.27	62.1	1.30	-14.56	
- 2.21 - 1.29 - 1.137241343433479 - 2.5664 .77 1.88 2.17 2.29 2.38 3 3 3 3 3 3 3 3 3	8		- 2,03	11.		1.16	1.37	1,42	1,43	1,44	1,45	202-	
-344 - ,74 1.52 1.78 1.94 2.03 2.06 2.09 -5.74 - 3.38 -1.17 .10 1.21 1.90 2.11 2.24 - ,31 1.85 2.32 2.58 2.86 3.10 2.95 2.86	40		-2,2		-1.13	2T	14' -	±6, −	- ,34		100	-2,14	
-3.44 - ,74 1.52 1.78 1.94 2.03 2.04 2.09 -5.74 -3.36 -1.17 .10 1.21 1.90 2.11 2.24 - ,31 1.85 2.32 2.58 2.86 3.10 2.95 2.86	41		- 4.79	1		77.	88,	2.17	62'2	2.38	2.41	-4.81	
-344 - ,74 1.52 1.78 1.94 2.03 2.06 2.09 -5,74 - 3.36 - 1.17 .10 1.21 1.90 2.11 2.24 - ,31 1.85 2.32 2.58 2.86 3.10 2.95 2.86	42												
-5.74 - 3.36 - 1.17	43		-3.44	174 -	1.52	1.78	1,94	2,03	2.00	60'2	60'2	-3.35	
98.2 2.32 01.8 93.5 8.86	44		-5,74	1	1111-	0).	1.2.1	1.90	2.11	2.24	2.32	-5.77	
	45	2 1 2 1 3 1		1.85	2:32	85.5	2.86	3,10	295	98.2	18.5	22	
A STATE OF THE PROPERTY OF THE	The second			0.11			78.03						
		1231	2.1897.1.188										

Table 23. Strain Gage Results at 161200 Cycles - Crack Gages on AFCG-2 HANGING FREE B.I. BOLTED IN HANGING FREE H.F.

CTDATE	TEST	TEST CONDITION		161,200		CYCLES	(0					
GAGE		MEASURE	D STRESS	S (KSI)	AT	APPLIED AXIAL		LOAD (KIPS)				
NO.	0 H.F	0 8.1.	5	10	15	20	25	30	35	38.5	0 8.1.	0 H.F.
-		+1.	2.74	68'5	50'8	99'0	13.34	(6.00	18,68	29'02	01.	
2				K 10 10 10								
3											TRIF	
4		76.	3.48	6.13	28'8	11.51	14.26	10,71	19.78	er.13	11.	
5		1,18	4.31	7.34	82'01	13.14	16.02	18,84	21.65	23,66	1.20	
9		182	20'2	3.28	4,55	5,83	7.12	842	11.6	49'01	11.	
1		.32	1.49	11.2	36.5	5,20	6.46	7.12	8.99	966	52'	
8											() (0) ()	
6		.28	1.54	2,80	91.5	545	6.78	21'8	74'6	10,43	91'	
0)		-3,04	011-	49.1-	111-	56	- ,98	10'1-	- 1.03	1001-	-3.07	
-		691 -	1.23	2,18	2.48	55.5	2.59	2,60	29'2	29'2	01.1-	
21		-2.42	-1.22	63	02' -	80	10, -	To	80' -	08	1-2.44	
(3		99	1.15	1.70	(6.)	2,15	2,14	2.14	2.14	2113	99' -	
4)		-2.45	721-	65' -	81' -	.04	.23	.26	.25	:23	-2,53	
15		-3,29	60'1 -	60.	.65	19'	,54	,50	25'	.49	-3.27	
91		-3.85	- 1.55	.25	1.12	1.18	1.24	1.22	1.21	1.18	- 394	
IJ		-5.82	-353	00'1-	. 88	.89	46	56'	06'	88.	- 5.89	
18		19	.73	56'	16.	1.04	60'1	1.07	1.05	1.03	74	
61		-13.21	21.6-	-6.25	61.8-	-1.78	181-	-1,82	- 1,82	181-	-13,24	
02				01								
12		-11.67	-8,26	-4,96	- 2.60	181-	-1.93	-1.94	96'1-	16.1-	99.11-	
77		- 3.68	- 1.79	2411-	121-	61:1-	- 1.25	-1.27	- 1.30	-1.32	- 3.76	
23	100	14' -	40	05	-,59	65	68	- ,70	73	91' -	55	
42		22	21.	.04	07	0 1	0 -	کار -	+)	91	3/	

Table 23. Strain Gage Results at 161200 Cycles - Crack Gages on AFCG-2 (Continued) H.F. HANGING FREE B.1. BOLTED IN

CTDATE	TEST	TEST CONDITION:		161,200		CYCLES						
GAGE		MEASURED		STRESS (KSI)	A	APPLIED AXIAL LOAD (KIPS)	AL LOAD	(KIPS)				
WO.	O H.F	0 8.1.	5	10	15	50	25	30	35	38.5	0 8.1.	O H.F.
ડર		57	12	- 08	.03	.13	91.	9	41.	.13	- 155	
92												
n		- ,57	161	4.51	2112	91.6	12.45	15,14	17.84	19.78	17	
88		. 68	3.28	5,94	8.61	11.27	13,98	16.67	19.37	21.31	. وح	
S		10'	18.5	5,61	8.39	91.11	13,93	16.70	19,45	21,43	70	
8		20.	2,50	60'5	7.73	10,38	13.11	15,84	(8,59		01	
3		3.25	5,48	16.54	15.89	16'21	55,38				202	
32	0	167	1.96	3,28	4,60	5,88	7.18	8.47	9,80	10.72	09'	
35		1,85	3.76	18.47							.88	
34		Calle								0.000		
35		-2.29	-1.52	26. -	14 -	01	17	61	- 16	11	- 2.33	
36		-2.62	15, -	.25	.65	16	10'1	00'	1,02	101	- 2,63	
37		-3.28	- 2.72	96'1-	-1,28	- 1.38	- 1.54	- 1.58	- 1.60	191-	-3,50	
38		-14,38	61.01-	-7,18	-3,52	61.	1.25	1.27	1.27	1.27	-14.36	
33		- 1.85	.23	00'1	1.23	1.42	1.46	1,46	(.47	1,47	- 1.87	
40		- 2.08	12.1-	-1.13	75	144-	39	04	04	14' -	-2.13	
4		-5.27	-2.77	88	.75	20'2	244	95.5	2,60	242	-5.26	
42		188										
43	0	-4,45	-1.84	02	1.92	90'2	2.10	21.2	11.5	5,09	-4.51	
44	3.4.0	- 9.88	- 7.12	1000-	-,80	.80	66.1	2,36	142	2.41	-9,88	0 18 18 1
45		-3.98	-1.67	.71	12'2	249	2.74	27.2	2,68	2,68	-3.97	
N P P			K									
	1 3 3 3	Dept. 1										

Table 24. Strain Gage Results for Basic Panel at Start of Test-AFCG-2 MANGING FREE B.I. BOLTED IN H.F.

	O H.F.																		
	0 8.1.	140	011.	040	080	140	090-	010	010-	240	-160	200	057-						
	38.5	9500	9300	0196	9800	9800	9500	9410	9850	8660	8300	8650	8300						
	35	8660	84.50	8,740	0968	8960	8600	8.540	8950	0687	7510	0887	7560						Ī
(KIPS)	30	1460	0901	2510	2660	7660	7400	1300	7.700	6800	6410	00800	6480						
AL LOAD	25	6240	6,030	0250	6400	6400	oors	6040	6380	5,680	065	5690	5300						
IED AXI	20	5050	4880	5000	5150	5,50	4.900	48.10	5120	4610	4220	4590	4170					96 1	
TEST AT APPL	15	3810	3700	3770	3900	3900	3690	3610	3850	3560	3120	3520	3,150				}		
START OF TEST STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	10	2580	2480	0155	2630	2630	2410	2390	2520	2,480	0000	2450	2020						
	5	1370	1310	1300	(360	025)	1300	1200	0121	1380	920	1340	930						
TEST CONDITION:	0 8.1.	001	001.	020.	.050	070,	-040	020	160	082.	-160	360	-200						
TEST C	O H.F	0											0						
STRAIN	.O.	1.5	25	35	\$+	55	89	75	800	98	105	115	125						

Table 25. Strain Gage Results for Basic Panel at 161200 Cycles-AFCG-2 HANGING FREE B.I. BOLTED IN H.F.

STRAIN		TEST CONDITION:		IGH, 200	CYCLES							
GAGE		MEASURED		(KSI)	AI APPI	SIRESS (KSI) AI APPLIED AXIAL LOAD (KIPS)	AL LUAL	(KIPS)				
Q	0 H.F	0 B.I.	5	10	15	20	25	30	35	38.5	0 B.I.	0 H.F.
15		.450	1690	2910	2130	5290	6500	7.680	8,900	9.740	939	.690
25		0.0	0611	2390	3570	4710	5930	71.50	8350	9200	-040	09/
38		150	1380	2630	3880	5080	6350	7630	0688	0086	060	.260
5+		-140	0611	2510	3800	5080	6350	7630	8900	9840	-300	090
55		-,380	830	2010	32.50	4450	5660	6930	8170	9060	-450	-010
65		440	1.660	2900	4100	5300	6500	7730	8950	0586	.380	040
75		.640	1750	2910	4100	5240	6440	7640	88.50	9740	.560	030
88		-640	019.	2000	3360	4490	5740	7000	8260	9160	-700	-020
26		330	1450	2650	3790	4940	0609	7300	8440	9340	290	012.
105		./50	1210	2350	3510	46.30	5830	7040	8250	9110	011.	091,
115		.690	1,830	2950	4,130	5260	6440	7660	8810	9680	089.	300
125		100	0001	2140	3330	4500	5720	6910	8,140	0668	-040	905.
												15
		BEST CHE			e e							
							3					

52

985	
- 6	
1.0	
9	
-	
HE.	
- 8	
*	
100	
.00	
300	
-	
*	
-03	
-	
-	
- %	
- 75	
25	
5677	
44	
16	
-	
125	
#	
-	
- 2	
- 19	
nil.	
-	
8	
2	
48	
Ε	
- 20	-
- 80	*
Ë	×
'n.	N 1 N
r Te	ED IN
or Te	TED IN
r Te	200
for Te	200
a for Te	200
is for Te	7
its for Te	200
uits for Te	200
Suits for Te	200
esuits for Te	200
Suits for Te	200
Results for Te	200
e Sesuits for Te	200
ge Sesuits for Te	200
Age Results for Te	200
ge Sesuits for Te	200
Gage Resuits for Te	200
n Gage Results for Te	200
in Gage Resuits for Te	200
ain Gage Resuits for Te	200
rain Gage Resuits for Te	200
ain Gage Resuits for Te	200
rain Gage Resuits for Te	200
rain Gage Resuits for Te	EE 8.1. 80c.7
rain Gage Resuits for Te	200
. Strain Gage Resuits for Te	EE 8.1. 80c.7
rain Gage Resuits for Te	EE 8.1. 80c.7
. Strain Gage Resuits for Te	G FREE B. I. BOLT
. Strain Gage Resuits for Te	EE 8.1. 80c.7
. Strain Gage Resuits for Te	G FREE B. I. BOLT
. Strain Gage Resuits for Te	G FREE B. I. BOLT
. Strain Gage Resuits for Te	G FREE B. I. BOLT
. Strain Gage Resuits for Te	MAING FREE B. I. BOLT
. Strain Gage Resuits for Te	MAING FREE B. I. BOLT
. Strain Gage Resuits for Te	MAING FREE B. I. BOLT

3 :	ii.	MEASURED	STRESS	(KSI	AT APP	APPLIED AXIAL LOAD	AL LOAD	(KIPS)	
6	M H. F.		un	2	59	*	35		
1	20	35	1.50	2.14	5.36	1,81	306	87.6	
	10	51	.33	3.30	5.43	3.81	8.45	3.07	
	10	52	-81	213	5.49	7.10	10.5	9.15	
	8	4.2	1.44	2.74	5.19	9. kg	9.36	00.01	
	-03	20	1.33	2.55	5.13	7.92	9.36	3.91	
	20	4.3	141	2 79	5.53	9.30	40.6	10.32	
	.0.	171	1.23	3.33	19.4	16.9	800	5.00	
	107	:0:	1.09	-	4.57	6.93	8.11	See . Di Guid	
	50	07	1.18	2.33	30	97.0	7.99	12.0	
0	40	+0'	LOS	3.24	4.56	08.9	8 O.B	7.64	
	40	08	3.3.3	G-90	17.57	16.95	19.61	21.22	
		.15	3.69	6.73	12.72	19.13	32.15	23.65	
-	+0.	*6	3.13	18.9	13.37	18.44	41.30	22.78	
,	- 53	.9.6	3.79	6.71	12.52	24.91	4 :0	17 68	
	10.7	1.61	7.7	4.64	13.33	1.00	AG DE	22.23	
	20.	7.00	3,17	28.9	12.51	15.55	64.14	23.75	
-	10.	41.	1.14	14.5	4.42	2.19	8 54	3.14	
4	10	60.	1.12	1.22	4.50	48.0	8.03	8.60	
0	.03	315	3.00	5.38	9.66	14.76	17.33	18.46	
30	0	1.02	3.86	6.50	13.01	17.39	20.07	21.37	
3.	50.	.87	3.44	5.33	11.09	16.33	18.84	20.13	
77	50.	.72	3.50	6.38	11.71	17.04	19.70	21.00	
23	20.	49	2.60	4.81	9.40	14.16	16.61	17.82	
24	3		,	,,					

* With Buckling Restrainers Installed

Table 26. Strain Gage Results for Tension Loading at Start of Test-AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

MEASURED STRESS (KSI) AT APPLII 9 H.F. 9 B.I.* 5	D AXIAL LOAD (KIPS)
9 H.F. 9 B.I.* 5 19 29 5 -02 -02 2.31 4.72 9.56 1 6 03 1.07 3.41 5.63 10.69 1 7 .05 .94 3.35 5.92 11.04 8 .05 .94 3.35 5.95 10.69 9 .05 1.16 3.73 6.34 11.57 9 .04 16 3.73 6.34 11.57 9 .04 70 1.81 4.56 10.06 10 49 1.76 4.52 10.05 10 49 1.76 4.52 10.05 10 49 1.76 4.52 10.05 10 49 1.10 4.52 10.05 10 49 2.14 4.96 10.06 10 49 2.14 4.96 10.06 10 24 1.37 4.09 9.52 10 24 2.14 4.96 10.06	
03 1.07 3.41 5.83 10.69 05 .85 3.35 5.92 11.04 .05 .94 3.35 5.85 10.69 .05 .94 3.35 5.85 10.82 .05 .94 3.35 5.97 10.86 .04 1.16 3.47 5.98 11.04 .04 78 1.81 4.56 10.08 .04 78 1.97 4.59 10.08 .02 49 1.81 4.56 10.08 .03 12 1.27 4.96 10.09 .03 124 1.37 4.99 10.08 .04 49 1.24 4.96 10.09 .05 24 2.13 4.92 9.98 .04 29 2.14 4.82 9.98 .05 24 2.13 4.93 9.41 .04 13 2.34 4.82 9.48 .04 30 2.14 4.29 9.48 .0	19 35 37.5
.03 1.07 3.41 5.83 10.69 .05 .94 3.35 5.92 11.04 .05 .94 3.35 5.85 10.82 .05 1.15 3.52 5.97 10.86 .04 1.16 3.47 5.98 11.04 .04 70 1.81 4.56 10.08 .04 70 1.81 4.52 10.05 .07 49 1.16 4.56 10.05 .09 49 1.04 4.96 10.61 .03 -1.16 1.37 4.96 10.05 .03 -1.24 1.37 4.99 9.52 .03 -1.24 1.37 4.99 10.05 .04 29 2.13 4.94 9.95 .04 29 2.14 4.96 10.05 .05 24 2.13 4.92 9.98 .04 20 2.24 4.82 9.98 .04 20 2.34 4.82 9.48	14.42 16.88 18.09
05 94 3.35 5.92 11.04 05 94 3.35 5.85 10.82 05 1.15 3.52 5.97 10.86 04 1.16 3.47 5.98 11.04 02 1.01 3.47 5.98 11.04 04 70 1.81 4.56 10.08 04 70 1.81 4.52 10.08 0.0 49 1.76 4.52 10.08 0.0 49 1.37 4.96 10.08 0.0 49 2.14 4.99 9.52 0.0 49 2.14 4.99 9.52 0.0 49 2.14 4.99 9.52 0.0 49 2.14 4.82 9.88 0.0 24 2.13 4.82 9.88 0.0 13 2.45 4.39 9.41 0.0 34 4.24 9.48 0.0 12 2.16 4.24 9.48 0.0 20	.58 18.05 19.25
05 94 3.35 5.85 10.82 .05 1.16 3.52 5.97 10.86 .04 1.16 3.43 6.34 11.57 .02 1.01 3.47 5.98 11.04 .04 70 1.81 4.56 10.08 .04 70 1.81 4.52 10.08 .07 49 1.76 4.52 10.08 .07 48 1.97 4.96 10.61 .03 -1.16 1.51 4.96 10.68 .03 -1.24 1.37 4.99 9.52 .03 -1.24 1.31 4.99 9.52 .04 29 2.13 4.93 9.95 .04 13 2.34 4.82 9.88 .04 50 2.11 4.87 9.41 .02 37 1.92 4.24 9.48 .04 50 2.11 4.24 9.48 .04 50 2.11 4.24 9.48	11 18.65 19.89
.05 1.15 3.52 5.97 10.86 .04 1.16 3.47 5.98 11.04 .04 70 1.81 4.56 10.08 .04 70 1.81 4.52 10.08 .04 78 1.97 4.52 10.05 .02 48 1.97 4.52 10.05 .03 16 1.57 4.96 10.61 .03 -1.16 1.57 4.96 10.68 .03 -1.14 1.37 4.09 9.52 .05 24 2.13 5.02 10.68 .04 24 2.13 4.82 9.95 .04 13 2.14 4.82 9.41 .04 13 2.14 4.39 9.41 .04 50 2.14 4.24 9.48 .04 50 2.16 4.24 9.48 .07 31 4.24 9.48 .07 31 4.24 9.48 .07 31 <td< td=""><td>(8.25</td></td<>	(8.25
04 1.16 3.73 6.34 11.57 02 1.01 3.47 5.98 11.04 04 70 1.81 4.56 10.08 04 70 1.81 4.52 10.08 04 78 1.97 4.67 10.05 0.0 49 1.97 4.96 10.61 0.0 116 1.51 4.99 9.52 0.0 124 1.31 4.09 9.52 0.0 24 2.13 4.93 9.95 0.0 24 2.34 4.82 9.88 0.0 24 2.34 4.82 9.89 0.0 37 1.92 4.39 9.41 0.4 50 2.11 4.87 9.48 0.4 50 2.11 4.24 9.48 0.4 50 2.11 4.24 9.48 0.4 80 1.85 4.24 9.24 1.4 69 4.29 9.24	15.74 18.17 19.35
0470 .81 4.56 10.06 .04 .04 .04 .04 .06	16.73 19.32 20.58
.04 70 1.81 4.56 10.08 .04 78 1.76 4.52 10.05 .02 48 1.97 4.67 10.09 .02 49 2.14 4.96 10.61 .03 -1.16 1.51 4.34 9.95 .03 69 2.13 4.09 9.52 .02 24 2.13 4.93 9.95 .04 13 2.44 4.82 9.88 .04 50 2.11 4.87 9.41 .04 50 2.11 4.87 9.48 .04 50 2.11 4.24 9.48 .04 50 2.11 4.24 9.48 .04 80 1.85 4.24 9.44 .05 12 1.69 4.24 9.48 .04 80 1.85 4.24 9.24 .05 67 1.69 4.24 9.24	
	15.67 18.50 (9.30)
02 49 2.14 4.96 10.61 03 -1.16 1.51 4.34 9.95 03 69 2.13 5.02 10.68 02 24 2.21 4.09 9.52 04 13 2.46 5.19 10.37 04 80 1.85 4.24 9.48 1. 49 1. 10.37	18.38
.03 -1.16 1.51 4.34 9.95 .03 -1.24 1.37 4.09 9.52 .0224 2.23 5.02 10.68 .0224 2.24 4.82 9.88 .0413 2.46 5.19 10.56 .0237 1.92 4.39 9.41 .0450 2.11 4.87 10.37 .0480 1.85 4.62 10.15	32.02 21.61 72.9
.03 -1.34 1.31 4.09 9.52 .0369 3.13 5.02 10.68 .0224 2.27 4.93 10.33 .0413 2.46 5.19 10.56 .0450 2.11 4.87 10.37 .0450 2.11 4.87 10.37 .0480 1.85 4.24 9.48 .0480 1.85 4.24 9.48	15.53 18.33 19.69
.03 69 3.13 5.02 10.68 .02 24 2.21 4.93 10.39 .02 13 3.46 5.19 10.56 .02 13 3.46 5.19 10.56 .02 37 1.92 4.39 9.41 .04 50 3.11 4.87 10.37 .04 80 1.85 4.42 9.48 .04 80 1.85 4.62 10.15	.91 17.62 18.94
.0224 1.21 4.93 10.33 .0413 1.46 5.19 10.56 .0437 1.92 4.39 9.41 .0450 2.11 4.87 10.37 .0480 1.85 4.62 10.15	18.28 19.06 20.41
.02 .05 2.34 4.82 9.88 .0413 2.46 5.19 10.56 .0237 1.92 4.39 9.41 .0450 2.11 4.87 10.37 .0480 1.85 4.62 10.15 1 .0267 1.69 4.19 9.24 1	5.93 18.74 20.13
.04 13 3.46 5.19 10.56 .02 37 1.92 4.39 3.41 .04 50 3.11 4.87 10.37 .02 72 1.68 4.24 9.48 .04 80 1.85 4.62 10.15 .02 67 1.69 4.19 9.24	15.09 27.71 69.03
.0237 1.92 4.39 9.41 .0450 3.11 4.87 10.37 .0272 1.68 4.24 9.48 .0480 1.85 4.62 10.15 1	15.87 18.54 19.83
.0250 2.11 4.87 10.37 .0272 1.68 4.24 9.48 .0480 1.85 4.62 10.15	14.54 17.17 18.46
.0480 1.85 4.24 9.48 .0480 1.85 4.62 10.15	15.84 18.56 19.90
.0480 1.85 4.62 10.15	.81 17.53 18.56
.0267 1.69 4.19 9.24	18.46 17.51
	13.01
105 - 108 - 105 4.37 17.05	05 7.36 8.56

* With Buckling Restrainers Installed

Table 27. Strain Gage Results for Compression Loading at Start of Test-AFCG-3 H.F. HANGING FREE 8.1. BOLTED IN

GAGE		MEASURE	0	STRESS (KSI) AT AF		AT APPLIED AXIAL LOAD (KIPS)	AL LOAD	(KIPS)	
NO.	* 180	-5	-10	-15	-20	-25	-29	× 180	
-	.25	-1.00	-2.26	-3.55	-4.87	-6.27	-7.55	12.	
2	- 16	-1.38	-2.55	-3.76	-4.96	-6.10	- 6.82	61	
3	08	-1.26	-2.49	-3.73	- 4.92	- 5.98	- 6.51	عر. <i>-</i>	
4	33	98	-2.34	-3.73	-5.20	er.9 -	- 8.35	.05	
5	11.	-1.18	-2.41	-3.63	-4.81	- 5.85	- 6.32	01.	
v		-1.29	-2.64	-4.03	-5.49	- 7.07	- 8.64	07	
7	117	- 1.03	-2.14	-3.29	-4.47	- 5.68	- 6.75	50.	
8	.07	-1.08	-2.22	- 3.39	-4.56	- 5.69	- 6.47	02	
6	.09	-1.06	- 2.14	-3.27	14.41	- 5,59	- 6.64	.04	
0	10.	-1.14	-2.27	-3.41	-4.55	- 5.68	- 6.45	04	
=	.52	52 - 2.22	-4.92	-7.65	- 10.49	- 13,53	- 17.04	.28	
7	.96	-2.14	-5.25		-11.72	-15.04	- 17.33	5۲.	
13	1.05	-1.86	-4.76	-7.68	-10.68	- 13.71	- 16.09	.8.j	
14	76.	- 1.95	-4.88	-7.90	-11.07	- 14.54	- 18.26	.84	
15	1.07	- 1.80	-4.70	-7.7C	-10.90	- 14.48	- 18.45	68.	
16	1.13	- 1.81	-4.65	-7.50	-10.37	-13.20	- 15.22	. ا	
11	.20	46	- 2.01	-3.04	- 3.36	rr.4 -	- 5.00	.25	
9	.13	92	-1.93	-2.85	-3.76	- 4.48	-4.65	١٤.	
61	.76	-1.47	-3.54	-5.52	-7.31	- 8.67	-8.87	۲۲.	
20		-1.96	-4.87	-7.97	-11.36	- 15,25	- 19.68	.95	
21	.80	-1.80	-443	-7.18	-10.21	- 13.82	- 18.85	רר.	
22	69.	-2.17	-5.10	-8.22	-11.70	- 15.69	(3.07.	.55	
23	.52	-1.62	-3.64	-5.55	-7.22	- 8.53	25.8 -	.43	

Table 27. Strain Gage Results for Compression Loading at Start of Test - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

cade MEASURED STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS) road -5 -10 -15 -20 -25 -29 0BI * 26 -36 -10 -15 -20 -25 -29 0BI * 26 -36 -10 -15 -20 -25 -29 0BI * 26 -36 -143 -3.1 -6.03 -8.38 -1086 -15.27 -116 27 -13 -1.86 -4.35 -6.89 -9.49 -12.10 -14.29 -10 29 -1.41 -4.06 -6.35 -8.97 -8.91 -10.13 -10.23 -10.33 -10.23 -10.33 29 -1.01 -4.06 -6.54 -9.00 -11.35 -12.33 -10.43 -10 30 -1.01 -4.06 -6.54 -9.00 -11.37 -13.35 -10.33 31 -3.20 -5.85 -8.53 -10.27 -13.42 -10.33 32 -3.21 <th>AT APPLIE</th> <th>I IVIAV U</th> <th></th>	AT APPLIE	I IVIAV U	
.03 -2.40 -4.76 -7.20 .98 -1.43 -3.71 -6.03 .98 -1.43 -3.71 -6.03 .73 -1.86 -4.35 -6.89 .76 -1.45 -3.69 -5.97 .100 -1.45 -3.69 -5.97 .101 -1.61 -4.06 -6.45 .88 -1.68 -4.03 -6.45 .25 -3.31 -5.85 -8.5352 -3.16 -4.03 -6.45 .39 -2.91 -5.86 -8.5939 -2.91 -5.86 -8.9939 -2.91 -5.86 -9.3213 -3.99 -6.65 -9.3213 -3.99 -6.65 -9.3210 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5710 -2.59 -5.54 -8.5510 -2.58 -4.96 -7.3336 -2.59 -5.94 -8.83		חאואה ח-	LOAD (KIPS)
.03 - 2.40 - 4.76 - 7.20 .98 - 1.43 - 3.71 - 6.03 .73 - 1.86 - 4.35 - 6.89 .76 - 1.45 - 3.69 - 6.45 .70 - 1.45 - 3.69 - 5.97 .70 - 1.45 - 3.69 - 5.97 .70 - 1.61 - 4.06 - 6.54 .88 - 1.68 - 4.03 - 6.4552 - 3.21 - 5.85 - 8.5364 - 3.30 - 5.90 - 8.4939 - 2.91 - 5.34 - 7.6110 - 2.9 - 6.65 - 9.1510 - 2.61 - 6.67 - 10.0210 - 2.69 - 5.54 - 8.5516 - 2.58 - 4.96 - 7.3326 - 2.59 - 5.94 - 8.8536 - 3.09 - 5.94 - 8.8555 - 3.02 - 5.49 - 7.86	- 20 -	-25 -29	* 180 °
98 -1.43 -3.1 -6.03 -33 -1.86 -4.35 -6.89 -1.00 -1.43 -3.69 -5.97 -1.01 -1.61 -4.06 -6.45 -1.52 -3.21 -5.85 -8.53 -1.64 -3.30 -5.90 -8.49 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.59 -8.90 -1.14 -3.99 -6.59 -9.33 -1.6 -2.58 -4.96 -7.33 -3.6 -2.59 -5.94 -8.85 -3.6 -3.39 -5.94 -8.85 -3.6 -3.39 -5.94 -8.85	-9.76-1	-12.54 - 15.27	2716
	8.38	- 10.86 - 13.	26. 62.
	9.49	- 12.10 - 14.29	٥٢. ود.
1.00 - 1.43 - 3.69 - 5.97 1.01 - 1.61 - 4.06 - 6.54 2.82 - 1.68 - 4.03 - 6.45 2.52 - 3.21 - 5.85 - 8.53 2.64 - 3.30 - 5.90 - 8.49 2.39 - 2.91 - 5.34 - 7.61 2.13 - 3.99 - 6.65 - 9.32 2.13 - 3.99 - 6.65 - 9.15 2.6 - 2.13 - 4.40 - 6.54 2.6 - 2.13 - 4.40 - 6.54 2.6 - 2.58 - 4.96 - 7.33 2.6 - 2.69 - 5.54 - 8.55 2.6 - 2.58 - 4.96 - 7.33 2.55 - 3.02 - 5.94 - 8.85 2.66 - 3.38 - 6.3 - 9.11	8.82 -	11.13 -12.93	٦٦، ١٤٥.
.88 -1.68 -4.06 -6.54 .88 -1.68 -4.03 -6.45 52 -3.21 -5.85 -8.53 64 -3.30 -5.90 -8.49 39 -2.91 -5.34 -7.61 34 -3.14 -5.34 -7.61 -1.13 -3.99 -6.65 -9.32 -1.13 -3.99 -6.65 -9.15 -1.25 -3.93 -6.52 -9.15 61 -3.61 -4.87 -6.87 61 -3.61 -4.87 -6.87 16 -2.13 -4.40 -6.5 16 -2.58 -4.96 -7.33 36 -2.58 -4.96 -7.33 36 -2.58 -4.96 -7.33 56 -3.38 -6.3 -9.11	-8.21-1	- 10.33 - 11.75	10.1 57
.88 -1.68 -4.03 -6.4552 -3.1 -5.85 -8.5364 -3.30 -5.90 -8.4939 -2.91 -5.34 -7.6134 -3.14 -5.95 -8.90 -1.13 -3.99 -6.65 -9.31.15 -3.93 -6.5 -9.1561 -3.61 -6.67 -10.0210 2.61 -4.87 -6.5710 2.61 -4.87 -6.5716 -2.58 -4.40 -6.516 -2.59 -5.54 -8.5536 -2.69 -5.94 -8.8336 -3.09 -5.94 -8.83	-9.00-	11.37 - 13.	1.03
52 -3.31 -5.85 -8.53 64 -3.30 -5.90 -8.49 39 -2.91 -5.34 -7.61 34 -3.14 -5.34 -7.61 -1.13 -3.99 -6.65 -9.3. -1.25 -3.93 -6.65 -9.3. 61 -3.61 -6.67 -10.02 10 -2.61 -4.87 -6.57 10 -2.61 -4.87 -6.57 10 -2.61 -4.87 -6.57 16 -2.58 -4.96 -7.33 36 -2.69 -5.54 -8.55 36 -3.02 -5.94 -8.85 56 -3.38 -6.3 -9.11	-8.92 -	- 11.58 - 14.35	.35 .79
64 -3.30 -5.90 -8.49 39 -2.91 -5.34 -7.61 34 -3.14 -5.95 -8.90 -1.13 -3.99 -6.65 -9.32 -1.25 -3.93 -6.52 -9.15 61 -3.61 -6.67 -10.02 10 -2.61 -4.87 -6.57 10 -2.61 -4.87 -6.57 16 -2.13 -4.40 -6.55 16 -2.59 -5.54 -8.55 16 -2.58 -4.96 -7.33 36 -2.69 -5.94 -8.85 55 -3.02 -5.49 -7.86	-11.23 -	- 13.89 - 15.75	.7573
39 -2.91 -5.34 -7.6134 -3.14 -5.95 -8.90 -1.13 -3.99 -6.65 -9.32 -1.25 -3.93 -6.52 -9.1510 -2.61 -4.87 -6.5710 -2.61 -4.87 -6.5716 -2.13 -4.40 -6.516 -2.58 -4.96 -7.3336 -2.58 -4.96 -7.3336 -3.99 -5.94 -8.8555 -3.02 -5.49 -7.86	-10.01-	13.12 - 14	24.2175
34 -3.14 -5.95 -8.90 -1.13 -3.99 -6.65 -9.32 -1.25 -3.93 -6.52 -9.15 61 -3.61 -6.67 -10.02 10 -2.61 -4.87 -6.57 10 -2.61 -4.87 -6.57 16 -2.13 -4.40 -6.55 16 -2.59 -5.54 -5.55 36 -2.69 -5.54 -8.55 36 -3.09 -5.94 -8.83 55 -3.02 -5.49 -7.86	9.53	- 10.61 - 10.43	.4348
-1.13 -3.99 -6.65 -9.32 -1.25 -3.93 -6.52 -9.15 61 -3.61 -6.67 -10.02 10 .2.61 -4.87 -6.87 .26 -2.13 -4.40 -6.5 .05 -2.69 -5.54 -8.55 16 -2.58 -4.96 -7.33 36 -2.58 -4.96 -7.33 36 -3.09 -5.94 -8.83 55 -3.02 -5.49 -7.86	-12.03-	- 15.44 - 18.10	S3
-1.25 -3.93 -6.52 -9.15 61 -3.61 -6.67 -10.02 10 -2.61 -4.87 -6.57 .26 -2.13 -4.40 -6.55 16 -2.59 -5.54 -5.55 16 -2.58 -4.96 -7.33 36 -3.09 -5.94 -8.83 55 -3.02 -5.48 -7.86 66 -3.38 -6.25 -9.11	- 11.89 - 1	- 13.33 - 10.53	011 - 85
61 -3.61 -6.67 -10.02 10 .2.61 -4.87 -6.87 .26 -2.13 -4.40 -6.5 .08 -2.69 -5.54 -5.55 16 -2.58 -4.96 -7.33 36 -3.09 -5.94 -8.83 55 -3.02 -5.49 -7.86	-11.92 - 15	000	21.43 - 1.08
10 2.61 -4.87 -6.57 .26 -2.13 -4.40 -6.55 .08 -2.69 -5.54 -5.55 16 -2.58 -4.96 -7.33 36 -3.09 -5.94 -8.83 55 -3.02 -5.49 -7.86 66 -3.38 -6.25 -9.11	-13.83 -	- 18.49 - 23	22.1358
.26 -2.13 -4.40 -6.5 × .08 -2.69 -5.54 -8.55 - 16 -2.58 -4.96 -7.33 -3.69 -5.94 -8.83 -5.55 -3.02 -5.49 -7.86 -3.38 -6.2 × -9.11	- 8.24 -	8.06 - 6	6.4813
.08 - 2.69 - 5.54 - 8.55 16 - 2.58 - 4.96 - 7.33 36 - 3.09 - 5.94 - 8.83 55 - 3.02 - 5.49 - 7.86 66 - 3.38 - 6.35 - 9.11	8.42-	9.69-9	9.1103
16 - 2.58 - 4.96 - 7.33 36 - 3.09 - 5.94 - 8.83 55 - 3.02 - 5.49 - 7.86 66 - 3.38 - 6.25 - 9.11	11.78 -15	- 77	18.1214
36 -3.09 -5.94 -8.83 55 -3.02 -5.48 -7.86 66 -3.38 -6.35 -9.11	9.64	- 11.82 - 13.37	.3739
55 -3.02 -5.49 -7.86 66 -3.38 -6.23 -9.11	- 11.74-	-14.57 -16.37	.3752
66 -3.38 -6.23 -9.11	- 10.09 -	- 11.37 - 12.	(3 187.51
	- 11.95 - 1	- 14.66 - 16.23	.2965
4644 -2.53 -5.38 -7.84 -	10.30	- 12,74 - 14.64	13 73.
47 - 10 - 1.13 - 2.12 - 3.05 -	1000	4 × 1 - 4	70 1 7

* With Buckling Restrainers Installed

Table 28. Strain Gage Results for Tension Loading at 410 Flights - AFCG-3 HANGING FREE B.I. BOLTED IN H.F.

GAGE	* E.	MEASURED		STRESS (KSI)		LIED AX	AT APPLIED AXIAL LOAD (KIPS)	
NO.	*ø B.I.	5	19	20	30	35	37.5	
1	.32	1.58	28.2	5.38	7.95	22.6	18.6	
2	54	.63	1.83	4.37	6.94	02.8	8.5%	
3	74	.29	14.1	4.00	16.69	200	8.73	
4	-1.19	07	- 1-	3.82	0.50	26.6	19.61	
5	1.11	2.32	13.51	16.04	20.8	16.6	95.01	
9	1.00	2.32	3.05	62.0		6201	16.01	
7	38	.72	1.85	12.4	85.0	27.76	3.30	
8	.31	1.35	2.46	19.79	7.13	18.81	16.8	
6	10	ا.	82.2	4.58	18.0	10.8	15.61	
01	.73	98. 1	16.2	22.6	15.7	3000	7.23	
//	2.02	4.77	7.52	13.27	19.10	cu 22	23.53	
12	3.10	6.22	9.32	15.67	66.12	21.13	16.71	
13	-3.51	06'-	95.1	5.94	98.6	18:11	61.21	
4	-2.73	10	2,03	7.59	50.51	L7.4!	104.41	
15	-190.00	-190.00-186.85	213.79	216.96-198.41	14861-	-107.32	-232.15	
16	3.47	6.34	91.18	15.08	66:02	13.73	14.105	
7.	.75	1.80	2.88	12.0	697 L	16.8	65.6	
18	ماها.	1.65	2.69	4.95	22.7	8.31	8 .98	
19	-1.04	99.	3.28	8.13	13.15	1201	16.79	
20	44.1-	1.33	4.25	10.03	CL.61	13.51	19.74	
21	76	1.50	4.16	13.6	14.89	17.09	18.71	
22	-1.03	1.77	4.66	10.40	16.91	18.73	20,102	
23	11	1.25	3.42	8.19	13.03	17.53	10.77	
	61	238	10 9E	10.17	15.36	17.97	66 61	

Table 28. Strain Gage Results for Tension Loading at 410 Flights - AFCG-3 (Continued) W.F. HANGING FREE 8.1. BOLTED IN 8.1. BOLTED IN

SIRESS (KSI) AI APPI	LIED AX	AI APPLIED AXIAL LOAD (KIPS)
30	32	37.5
9.05 14.53	16.97	12.81
12.01 105.	87.81	20.02
16.86		-
32. 21 88.	44.41	12.25
Pr. 11 80.	13.85	14.88
07.71 54.51	2034	19.12
163 16.79	19.39	11:02
17.29	20.10	49.12
13.20 18.92	21.79	23.25
10.70 16.50	19.52	21.03
PF. 31 80. 11	19.87	21.36
2r. TI 05.51	20.40	12 .85
12.76 18.11	08:02	71.22
19.85 20.38	28.15	34.55
18.61	21.36	22.76
14.01 08.	18.96	12.02
15.71 14.	\$1.02	44.12
16.41 66.	12.54	18.86
28.011 18.	60.61	14:02
78 15.12	18.71	2.2
10.10 15.68	12.47	19.99
14.28	16.90	19.281
10 01	011 6	ור מ
	19.28	31,

Table 29. Strain Gage Results for Compression Loading at 410 Flights-AFCG-3 . HANGING FREE B.I. BOLTED IN

STRAIN	MEASURE	MEASURED		STRESS (KSI)	AT APPI	LIED AX	IAL LOAI	AT APPLIED AXIAL LOAD (KIPS)	
.0	* .1.9	-5	-19	-15	-29	-25	-29	øB.1. *	
	.32	06:-	112-	-3.47	-9.74	FC. 27	-7.28	18.	
2	16	Ur. 1-	86:2-	-4.25	10.85	-6.00	001 L -	63	
3	01	PP.1-	18.8-	19.4-	- 15.80	-6.9	27.68	21.17	
ð	-1.19	45.2-	268-	-5.39	-6.30	18.8-	11.6-	\$ - 7	
2	1.03	PO	1.29	-2.53	-3.08	一つ・ナー	2011-	.85	L
9	.98	12	1.52	2	12.4-	2	21.7-	88.	
7	85	1.55	-2.72	18.39	- 11.0	-6.35	-7.43	24	
8	62.	08. 7	-1,93	-8.10	-4.18	08.11-	-6.10	22.	
6	10:	= -1	-203	-3.39	トマッカー	10.74	-6.78	20' -	
0	27.	1.30	す、 -	-2.53	-3.59	60.4	- 5.48	69	
=	20.2	13 -	-3.28	-6.02	07.8-	-11.38	02.01-	161	
21	13.11	.13	-3.03	62.07	2.6-	18.91	-19.30	10.8	
13	-3.50	10.07	16.8-	11.87	18.91	19.22	22.22	-3.56	
19	-2.73	10.39	-8.30	-11.33	-14.40	19.07	26.06	21.5-	
15	-7.85								
10	3,47	.70	-2.12	14.99	91.7-	10.04	06:11-	75.2	
17	21.	78' -	-1.39	12.39	- 3.32	01.4	09.4-	0)0).	
18	.63	- ,33	-1.31	12.2-	- 3.11	18.37	4.20	00).	
13	196	13.25	- 5.32	20.7-	808-	04. 1-	3.65	16	
02	-1.38	-9.73	11.8	78.11-	16.09	20.22	30.36	851-	
12	06	-3.83	18.01	-10.00	-13.80	19.70	12.08	1.08	
22	-1.00	19.23	7.02	-11.19	-15.20	-20,30	25.22	12.1-	
23	65	08.2-	-4.71	-6.43	7.65	06:1-		-75	
22	11.1	17.21	12.01-	17.77	11.01-	1271-	80.01-	73	

Table 29. Strain Gage Results for Compression Loading at 410 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

CTBAIN	TEST (TEST CONDITION:		410 FLIGHTS COMPLETED	COMPLETED					
GAGE		MEASURED	STRESS	S (KSI)	AT APPL	AT APPLIED AXIAL LOAD (KIPS)	AL LOA	(KIPS)		
NO.	ØB.1. *	-5	91-	-15	-20	-25	-29	Ø8.1. *		
25	01	04:2-	4.95	1511-	-10.13	-13.00	15.96	02		
90	1.27	-100-1-	-3.46	- 15.88	-8.31	10:01-	-13.58	1.24		
27	pp.	85:1-	-4.18	-6.83	04.6-	16.11-	13.81	.93		
28	1. 1.7	81.8-	-6.11	-8.45	TO.01-	10.21-	-13.53	- 1.43		
62	61.1-	-3.38	-5.63	- 7.83	-9.89	(10): 11-	12.29	- 1.13		
30	25.1	16-	-3.51	300-	P\$.8-	Pr.01-	- 12.22	65. 1		
31	01.1	- 1:33	-3.82	15:0-	06.8	CL. 11-	14.49	1.12		
28	79.	76-1	17.4-	841-	-10.46	18.94	17.32	32.		
33	28.2	8	-2.89	20.00	40.7-	10.6	06.8-	60.2		
38	1.16	29. 2 -	-4.99	1001-	-8.22	28: L-	02.4-	28' -		
35	82	1.8-	01.0-	-9.38	-12.98	-17.83	22.59	05		
36	12.1	10.1-	10.8-	21.0-	8.37	10.14	10.89	1 30		
37	1.85	25	-3.01	01.19-	-8.42	22:11-	15.13	26. 1		
38	3.49	.93	16.1-	- 15.13	- 8.36	22.21-	-15.96	3.47		
83	2:59	10	-1.89	4.04	-12.72	10.00-	10.55	2.53		
53	10.	29 -	-2.77	4.99	16.9-	-8.55	9.35	1.94		
7	2.00	35	-3.01	- 5.39	-3.67	11.37	14.41	1.36		
21	12.	80.2-	-4.53	16.0-	9.18	1-11.47	13.26	20		
6.3	15.	12:2-	10.6-	26 L-	10.555	13.21	19.96	02:		
46	03	28:2-	4.74	86.0-	-8.37	10.42	16:01	0):-		
100	53	161.8-	10.00	1	1.37	-13.84	15.27	- :55		
3	84	162-	6.58	80.8-	10.52	-13.14	15.37	- 15		
47	22.	- 18L -	21.1-	01.2-	3.5€	62.4-	27. 2	22	-	
	0 1 1 10									

* With Buckling Restrainers Installed

Table 30. Strain Gage Results for Tension Loading at 565 Flights - AFCG-3 H.F. HANGING FREE B.I. BOLTED IN

GAGE	MEASURE	MEASURED	D STRES	STRESS (KSI) AT APPI	AT APPL	IED AX	AT APPLIED AXIAL LOAD (KIPS)	
NO.	9 B. I.	5	19	20	30	35	37.5	
-	.32	1.57	2.83	5.40	7.96	9.76	88.6	
2	58	19	1.81	4.37	6.93	822	8.85	
3	92	.23	1.38	4.01	6.73	2,08	8.76	
+	-1.05	.20	1.43	4.16	6.90	8.27	8.95	
5	1.18	2.30	3.43	5.93	8.51	9.79	10.43	
9	1.09	2.29	3.56	6.20	8.80	10.10	10.74	
7	46	69.	1.84	4.21	6.59	7.78	8.35	
8	.32	1.40	2.51	4.86	7.31	8.38	8.35	
9	00.0	1.12	2.24	4.53	6.82	7.96	8.53	
0/	.78.	1.84	2.95	5.21	7.49	8.62	81.6	
"	2.20	4.95	7.74	13.53	19.47	22.47	23.96	
12	3.51	6.62	9.76	16.19	22.61	25.82	27.40	
13	- 4.72	- 2.14	.34	4.39	7.52	8.97	9.65	
+	- 4.30	- 1.58	01.1	5.18	9.60	11,35	15.51	
15)		1				
16	3.70	6.53	9.40	15.31	21.27	24.30	35.76	
17	.57	1.60	2.70	5.09	7.53	8.76	9.36	
18	19.	1.58	2.62	4.86	7.16	8.3%	8,89	
19	-1.32	86.	3.38	72.8	13.30	15.86	01.71	
20	-1.13	1.40	4.46	10.28	15.95	18.78	40,14	
21	-1.32	1.44	4.19	9.67	15.00	17.72	19.04	
22	- 1.32	1.7.1	4.68	10.45	16.04	18.80	20.14	
23	- 1.01	1.09	3.34	80.8	12.93	15.50	16.73	
2.	- 40		4.00	0	15 10			

Table 30. Strain Gage Results for Tension Loading at 565 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

CTOATM	1	is constitution.		SOS I LIGHTS CONFECTION	2011			
GAGE		MEASURED		STRESS (KSI)	AT APPL	IED AXI	AT APPLIED AXIAL LOAD (KIPS)	
	9 B. I.*	2	1,9	20	30	35	37.5	
25	31	2.08	4.50	9.40	14.30	16.77	17.97	
26	1.23	3.62	6.07	11.06	16.12	18.69	19.94	
77	16.	3.48	6.11	11.41	16.71	19.30	20.68	
38	- 2.39	+0	2.24	6.53	10.56	12.54	13.49	
29	- 2.09	91.	2.30	6.29	9.99	11.82	1/L.E1	
30	1.44	4.14	6.78	12.08	17.42	20.12	31.42	
31	1.06	3.67	6.20	11.35	16.56	19.22	20.50	
32	4	3.35	6.00	89.11	(7.49	20.41	21.85	
33	10.72	13.27	15.90	21.83	27.70	30.69	32,18	
34	10.	2.53	5.16	10.92	16.86	19.89	21.38	
35	41	2.59	5.41	11.31	17.29	30.28	41.14	
36	1.60	4.22	6.85	(2.32	17.85	20.66	22.04	
37	2.15	1.7.4	7.27	12.61	17.98	10.71	33.04	
38	3.87	6.60	9.33	14.91	20.48	23.28	24.65	
30	2.19	5.23	7.75	13.07	18.55	21.33	ا ا ا ا ا ا	
9	1.65	3.91	6.27	11.26	16.30	18.27	20.13	
4	2.13	4.62	7.14	12.32	17.45	30.01	31.18	
47	81.	2.46	4.87	9.96	15.11	גר.רו	19.00	
43	.23	2.80	5.46	10.97	16.43	19.15	20.50	
44	30	2.07	4.57	9.84	15.18	17.89	19,23	
45	70	1.96	4.69	10.29	15.86	18.63	20.00	
16	72	1.67	4.15	9.31	14.51	17.14	18.44	
47	.06	1.10	2.17	4.47	6.1	8.07	8.61	

* With Buckling Restrainers Installed

Table 31. Strain Gage Results for Compression Loading at 565 Flights-AFCG-3 (.F. HANGING FREE B.I. BOLTED IN H.F. HANGING FREE

TOATE								
GAGE		MEASURED		STRESS (KSI)	AT APPL	AT APPLIED AXIAL LOAD (KIPS)	AL LOAD	(KIPS)
NO.	Ø 8.1.*	-5	ØL-	-15	-20	-25	-29	Ø B.I.*
-	.33	93	- 2,20	-3.49	- 4.78	0.9 -	-7.28	.34
7	09	- 1.81	- 3.06	-4.32	- 5,52	+ 6.74	-7.64	59.
3	16	- 2.17	- 3.45	- 4.73	- 5.95	- 7.10	- 7.83	- 1.16
4	-1.02	- 2.38	- 3.78	- 5. 14	-6.62	- 8.12	- 9.50	- 1.23
5	1.14	08	- 1.30	- 2.52	- 3.71	- 4.82	- 5.52	1.03
9	1.10	21	- 1.52	- 2.89	7-4-7	- 5.74	- 7.07	1.10
7	45	19.1 -	- 2.80	- 3.99	- 5.19	- 6.42	- 7.49	
8	.33	18: -	- 1.95	- 3.08	- 4.19	- 5.28	- 6.04	9 c .
6	.02	- 1.11	-2.27	-3.42	- 4.58	- 5.77	- 6.30	.02
0)	91.	32	-1.42	- 2.52	- 3.62	- 4.68	- 5.49	18
"	2.25	43	-3.16	-5.83	- 8.45	- 10.71	- 8.82	2.30
12	3.55	.48	- 2.73	- 5.94	- 9.18	-13,06	- 20.22	3,50
13	- 4.66	-7.30	-10.18	-13.17	16.45	- 21.03	-32.20	- 4.74
4	- 4.24 -	- 6.97	- 9.93	- 12.99	- 16.36	- 20.82	- 29.62	- 4.25
5								
16	3.78	96.	16.1-	- 4.73	- 7.52	- 10.10	11.31	3.66
17	.58	52	- 1.58	- 2.60	- 3.54	- 4.38	- 4.83	55
80	.58	44	- 1.44	- 2.38	- 3.25	- 4.01	14.4.	.57
6	- 1.24	- 3.39	- 5.43	- 7.10	-8.06	- 7.28	- 3.52	T.2.1 -
20	- 1.74	- 4.87	-8.31	-11.98	-11.98 - 16.40 - 22.51		-30.77	- 1.54
21	- 1.28	- 4.06	-7.0e	-10.29	-14.26	- 20.44	-31.14	- 1.36
22	- 1.30-	- 4.41	- 7.80	- 11.35	-15.50	- 20.60	- 25.86	151 -
23	95	- 3.00	- 4.93	- 6.62	- 7.78	- 7.97		101

* With Buckling Restrainers Installed

Table 31. Strain Gage Results for Compression Loading at 565 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

2 2 2						-		1	
GAGE		MEASUREI	STRESS	S (KSI)		AT APPLIED AXIAL LOAD (KIPS)	AL LOAD	(KIPS)	
NO.	9 B.I.*	-5	ØL-	-15	-20	-25	-29	9 8.1.*	
25	26	- 2.68	- 5.19	- 7.75	-10.40	- 13.31	- 16.23	31	0.0
36	1.26	11-1-	- 3.54	- 5.97	- 8.45	- 11.07	סר.13 -	1.38	
37	.92	- 1.65	-4.32	- 6.96	- 9.57	- 12.12	- 13.91	.97	
38	-2.35	- 4.68	-7.06	-9.39	-11.61	- 13.54		- 2.30	
39	- 2.05	- 4.28	-6.57	-8.78	- 10.84	- 12.54	- 12.99	-	
30	1.47	- 1.06	- 3.66	-6.23	or.8 -	- 10.99	- 12.37	1.55	
31	1.12	- 1.34	- 3.89	-6.45	- 9.04	- 11.82	-14.60	1.12	
32	.78	- 1.94	- 4.71	- 7.60	-10.63	- 14.33	16.71-	09.	
33	11.01	8.36	5.76	3.28		70,	. +8	16.01	
34	. oė	. 1	-4.72	-	- 7.50	- 6.05	- 2.77	40	
35	21	- 3.10	- 6.17	1	- 13.35	- 18.50	-23.29		
36	1.66	97	- 3.57	-6	- 8.36		- 10.20	1.59	
37	2.17	42	- 3.05	- 5.79	- 8.63.	- 12.01	- 15.43	2.16	
38	3.90	1.06	- 1.88		- 8.34		- 15.44	3.85	
39	2.85	14.	- 1.87	- 3.97	- 5.64	- 6.54	- 6.42	2.74	
40	1.69	29	- 2.88	- 5.05	- 7.02	19.8 -	- 9.40	1.56	
4	2.15	45	-3.15	- 5.94	- 8.83	- 11.93	- 14.49	3.06	
42	,23	- 2.17	- 4.56	-6.92	- 9.21	- 11.42	-13.17	60.	
13	.23	- 2.49	- 5,25	- 8.02	-10.74	- 13.31	- 15,10	,18	
44	26	- 2.67	- 5.04	- 7.27	- 9.25	- 10.82	_	35	
15	72	- 3.44	- 6.22	- 8.95	-11.57	_	- 15.46		
46	67	- 3.14	- 5.64	- 8.11	- 10.59	- 13.08	- 15.23	51	
47	70.	97	- 1.96	- 2.89	- 3.75	- 4.49	- 4.33	90.	

Table 32. Strain Gage Results for Tension Loading at 721 Flights-AFCG-3 H.F. HANGING FREE B.I. BOLTED IN BOLTED IN

CTDATM	TEST (TEST CONDITION:		721 FLIGHTS COMPLETE	COMPLETE						
GAGE		MEASURED	ST	STRESS (KSI)	AT APPL	APPLIED AXI	AXIAL LOAD	(KIPS)			
NO.	ØB. I.*	5	10	20	30	35	37.5	40	9	9	
-	.36	1.58	2.86	0	10.8	3.28	793	10:01	13.16	15.73	
0	15'-	8	1.93	4.37	6.94	12.0	8.8	953	12.09	14.67	
r	16	62.	1.44	4.3	670	20.0	8.73	9.93	12.12	14.32	
+	136-1-	1	10.1	3.00	04.0	37.33	2 76	9.18	11.93	14.62	
0	1.18	08.0	3.45	08.0	17.0	イント	1000	06. 1	13.63	16.29	
9	1.09	b8: 2	3,60	6.17	87.8	10.01	10.74	13.11	00 11	16 63	
7	74	OL.	1.36	22. 4	67.0	7.77	337	8.38	11.34	13.70	
a	26.	44. 1	2.55	٠.).	12.7	8 38	668	9.58	11.33	14.29	
6	10.	21.1	12.2	4 . 54	16.9	796	nor	9.13	20.11	13.72	
0	79	18.1	162	52.6	61.7	3.63	026	9.79	12.07	19.36	
j.	2.83	40.0	8.35	16.03 82.01	18:03	23.40	16:50	26.56	32.78	39.14	
2	19.4	130.7	10.88	17:50	86.25	2735	29.03	3002	37.25	43.85	
13	-6.32	19.8-	1-1.07	21.2	12° +	517	503	6.09	7 35	9:50	
+	16.19	15.5-	20 -	3.12	20.0	6.3	7 42	200	10.27	12.52	
2									9		
0]	432	J.06	9.96.	15.95	40.22	1162	50.75	28.28	34.93	69:00	
17	J.	1.83	16.2	12.9	01.7	166	acity	61:01	12.72	152.30	
3	00.	69. 1	01.2	CE D	7.19	8 33	116.6	04.6	11.88	18.91	
6	12.1-	99.	3.94	8.36	13.35	15 90	1721	13.55	23.65	68.82	
on	05.1-	1.65	18.4	8901	16.52	19161	19 62	66:12	20:12	33.09	
12	93	1.74	4.52	997	15.32	18.02	1937	22.32	11:02	31.62	
22	1.00	1.94	46.4	01.01	16.20	19.00	10 62	06.12	6212	2928	
23	19:	.18	3.94	8.16	13.00	10 54	16.33	13.12	23.13	28.82	
72	22' -	12.2	4.85	00:01	15.29	17 33	19.23	81. 23 22.55 25.98	81.03	31.03	
	The same of							1	1		

* With Buckling Restrainers Installed

Table 32. Strain Gage Results for Tension Loading at 721 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

TEST C	TEST CONDITION	10	STRESS (KST) AT API	AT APPI	IFD AX	TAI I DAT	APPI IED AXIAI I NAD (KIPS)			
*	,	2		6	1		3			
0	1.7	4.64	266	20.5	16.00	6.9	19.40	20.31	29.30	-
44.	3.23	62.0	1.33	16.0	19.02	2039	79.12	26.36	32.13	
8	3.74	6.39	al. 11	01.1	19.78	21 15	25.22	18.73	33.26	
200	8:1-	18:	4.61	7 99	9.60	10.52	05: 11	19.79	60.81	
.99	28	1.20	4.88	8.07	9.65	10%	11.27	14.4	17.8	
or.	4.20	7.02	12.40	81.71	64.03	96 12	12.82	69.62	34.16	
62.	3.72	150	10.	16.39	19.29	20.32	62.22	27.63	33.08	
.98	3.61	6.28	11 99	26:61	20.89	25 22	23.95	29.92	35.98	
Ī										
3	3.10	69.69	15:	74. TI	20.56	\$1.52	27.23	27.98	36.31	
01.	2.96	17.79	11.78	17.73	CO.12	22.56	21.42	20.29	36.51	
·84	4.43	7.12	12.58	18.19	76:03	25.52	13.97	19.62	35.27	
2.34	4.92	7.54	12.89	13.33	21.07	72.57	13.99	04.62	34.99	
12.17	1967	01.01	16.33	6613	08 22	26.24	27.69	33.33	39.02	
3.02	5.46	100	13.33	18.86	19:12	23.14	14. 22	30.24	36.01	
1.77	4.8	6.44	11 36	14.01	19.95	20.26	16.12	01.05	31.90	
187	4.93	194.7	12:57	17.71	20 20	75 12	22.99	79 75	33.11	
12.	2.63	10.01	10.03	15.16	17.78	60.61	28.02	20 02	36.08	
85.	3 05	50.03	11:11	03.31	12 61	630.02	22.02	27.9×	32.88	
11.	2 .33	18.7	10:00	15 30	17.97	19.37	11.02	26.19	11:18	
15.	2.14	16. 4	25.01	15.95	1811	20.13	05.12	80.72	89.28	
1651	1.79	4.26	9.37	14.54	17.17	18.43	19.98	80.42	30.41	
13	1.18	2.25	4.52	18.9	8.08	8.65	12.6	11.73	19.29	

* With Buckling Restrainers Installed

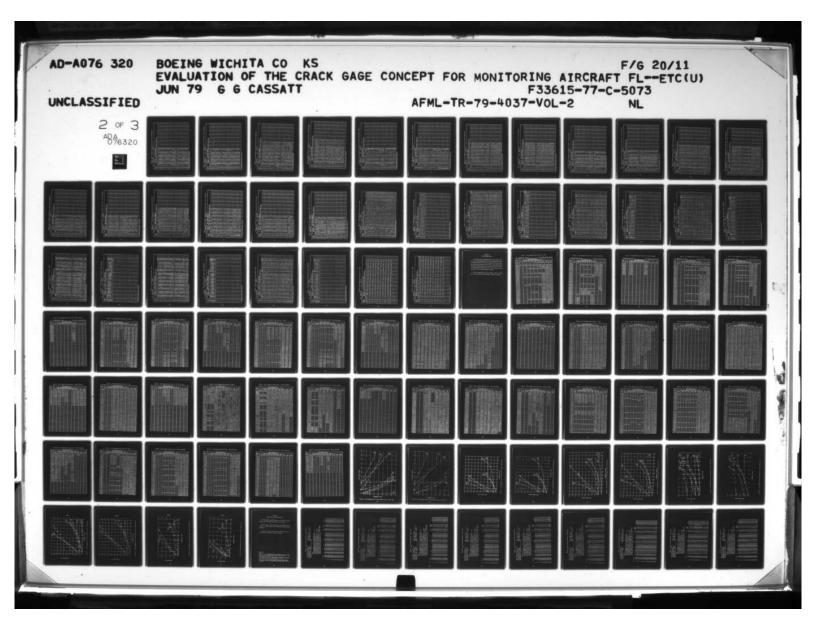


Table 33. Strain Gage Results for Compression Loading at 721 Flights-AFCG-3 H.F. HANGING FREE B.I. BOLTED IN

GAGE	Σ	MEASUREI	ST	STRESS (KSI) AT APP	AT APPL	AT APPLIED AXIAL LOAD (KIPS)	
NO.	ØB. I.*	-10	-20	-29	ØB.I.*		
	. 33	- 2.18	1-4.70	62.7-	.38		
2	08	-307	16.61	1-7	- (F)		
2	160 -	-3.94	15.95	1-	1.1-		
4	97 1-	-4.2	12.02	-9.83	OF. 1-		
0	1.16	- 1.31	-3.73	-5.06	26		
6	1.13	- 1.50	\perp	1	1.09		
7	26	-2.79	15.16	-7.43	98		
8	32	- 1.93	10.10	11-0-	.28		
0	20.	922-	Щ		20		
10	ā	16.1-	-3.59	15.54			
	2.85	-2.94	1	1	2.83		
16	4.53	1.80			4.45		, P. C.
13	12.9-	-12.24	-2032	-39.20	-6 53		
19	6.19	-12.21	19.95	1	- 6.20		
15							
16	4.34	18:1-	·11.0-	19.13	9.15		
17	.73	-1 45	-3.37	-4-73	67		
18	(79.	-1.34	-3.15	4.35	.60		
9	-1.12	-12.27	10.8-	-3.63	-1.04		
20	10:1-	- 7.89	18.61	-29.83	-1.00		
	16	-6.62	-13.62	19.62	93		
22	1-1.08	12.1-	7	24.42	1-1-15		
23	88	-4.83	17.79		06 -		
20.	- 35	-6.33	10.20	10.26-13.92	22		

Table 33. Strain Gage Results for Compression Loading at 721 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

GAGE		MEASURE	D ST	STRESS (KSI) AT APP	AT APPLIED AXIAL LOAD (KIPS)	AL LOAD (KIPS)
NO.	98.1.*	-10	-20	-29	Ø8.1.*	
u	13	- 505	10.21	16.02	61	
260	1.96	-3.43	F 8.21	-13.53	1.40	
27	9-	F 4.05	- 9.29	-13.95	1.21	
28	59 € -	1	-12.65	P1.291-4	-3.49	
29	26 2-	48.7-	7-1.95	-13.05	08:2-	
30	89. 1	15.57	14.8-	06:117	1.35	
18	1 :29	Ta. 5-	1-8.79	1439	8. 1	
32	16.	FG. 63	10.92	10.61-	99.	
3\$		AND E				
34	79.	1965-	18:4-	20	2	
3.70	10	-6.13	18.81	-24.34	<u>.</u>	
360	1.92	-3.23	1230	87.8-	1 .83	
37	2.37	16:2-	18.76	16.68	28:2	
38	17:11	TO	1	TI:31 -	100	
39	3.12	1.55	1-5.11	650-	462	
40	1.94	21.5	16.35	1-9.16	1.62	
41	2.42	16.2-	- 8.60	09.11-	12.2	
42	.33	14.47	-9.12	-13.23	21.	
48	.58	- 5.10	-10:00	10.21-	12.	
44	03	11.4-17	18.93	1.08	0]: -	
400	65	60.09-	2811-	- 15.39	16	
46	56	16.67	10.46	12.61	TS	
47	.12	B. 1 -	-3.40	-4.34	.13	

Table 34. Strain Gage Results for Tension Loading at 1000 Flights-AFCG-3 HANGING FREE B.I. BOLTED IN H.F. HANGING FREE

GAGE	2	MEASURED	STRES	STRESS (KSI)		IED AX	AT APPLIED AXIAL LOAD (KIPS)	
NO.	ØB. I.*	10	20	30	40	20	09	
1	3.	297	1257	II	10.79	13.36), o	
2	10: -	1.87	4.12	7.00	9.63	12.21	14.53	
3	12	64.	6.03	6.78	4.87	12.16	× × · ↓	
4	121-	1.22	3.98	e	9.39	12.10	37.7	
13	1.23	13.51	591	12.6	FC =	13.67	15:31	
6	1.16		6,19	8.83	24:11	16.01	€°.	
7	35	1 99	4.31	21.0	9.09	() p. 11	13.25	
2	.39	2.58	4.39	727	3.63	= c	6.39	
7	Bi	18:2	19.4	6.73	82.6	11.53	13.95	
0	16.	3.05	084	20.7	066	12.19	5.53	
	3.6	3.65	19 75	80.12	27.65	3425		
13	6.42	13.34	20.00	27.70	34.63	41.61	40.63	
13		12.5-	72	1.32	78	236	2.8%	
,	-1.79	09.1-	26	1.90	85.2	3.33	1.07	
				10. OF 10.				
10	88.5	11.12	14.71	00.43	30.60	87.13	13.75	
17	8	10.8	5.30	7.83	10.31	12.38	15.93	
0	.73	2.73	06 5	7.23	416	11:31	19 35	
5	1.16	3.96	8.37	13.42	13.54	40.8%	26.82	
00	63	10.99	11.35	17.07	150 22	23.8.2	33 33	
12	85	5.06	12.96	15.39	18 12	C 31 47	81 28	
22	79 -	CE 5	11.07	17.31	22.22	27.63	33.09	
23	74	3.95	3.23	13.29	18.27	23.33	28.53	
74	22	65.25	100	_	11111	110.39	21.74	

82

Table 34. Strain Gage Results for Tension Loading at 1000 Flights - AFCG-3 (Continued) H.F. HANGING FREE 8.1. BOLTED IN

GAGE	The state of	MEASUREL	_	SIRESS (KSI)	AI AFF	LIED AN	APPLIED AXIAL LOAD (KIPS)	
NO.	9B. 1.*	10	20	90	40	50	90	
10	<u>9</u>	6.9	4.84	14.94	19:61	24.73	m 67	
26	1.90	21:0	06 11	17.71	22.54	27.89	33.34	
17	1.78	160	12.94	18.03		1000	34.61	
82	17.4	- 53	2.27	4.77	7.15	1	= .93	
62	2.94	10'	12.5	4.75	6.94	かった	35. 11	
30	08:2	1	13.08	18.70	24.23	50.67	35.52	
31	1.72	26.90	12.20	05.71	23.19	. '99	34.34	
32	1.28	59.0)	99.21	18.97	25.25	64.18	37.36	
33								
34	1.57	82.0	06.11	18.29	24.80	18:18	37.98	
355	64.	16.37	12.71	19.56	25.87	5.2.28	18.97	
360	24.2	19.1	13.13	18.32	24.73	40.08	36.48	
37	3.03	2.8	13.76	14.61	2013	208	36.62	
38	829	08: 11	17.65	23.56	68.62	1066	10.14	
34	3.83	21.8	19.14	16.61	20.72	21.57	37.58	
20	2.00	090	19.11	16,77	26.12	60.12	88:28	
21	2.76	7.75	12.91	18.15	23.31	· 1.60	33.67	
42	.33	00.6	20:01	15.22	20.43	00.63	16 CS	
45	3	28.6	11.26	81.91	22.23	55 22	33.13	
7.4	21.	260	10.11	15.59	20.89	28 0%	31.37	
750	37	009	10.54	16.16	21.72	N. 15	35.36	
30	85' -	4.20	936	14.60	19.83	250	32 63	
17	62.	18.3	40.0	6.99	9.40	1 25	14.37	
				I		-	The second secon	

* With Buckling Restrainers Installed

Table 35. Strain Gage Results for Compression Loading at 1000 Flights - AFCG-3 BOLTED IN B.I. H.F. HANGING FREE

SIKAIN		MEACHDEN		DECC (VCI) AT ADD	AT ADDI	CTDECC (VCI) AT ADDITED AVIAL LOAD (VIDC)	
GAGE		LASON		CICAL CO	AI ALL	בורה איואר בטאה (אורא)	
9	ØB. I.	-10	-20	-29	08.I.*		
-	345	11.2-	17.4-	7.41	ょ		
1	53	-3 X	15.5-0	1-7.67	9		
3	75	-3.29	1-5.2	17.7-	BZ 1-		
4	-1.24	PF. 2-	1-6.33	8-9.69	1.56		
5	1,22	12'1 -	-3.63	12.4-	06.		
6	1.16	TP: 1-	12.1-1	10.1-	1.00		
1	- 36	P01.5-	1-5.73	1-7.39	15 -		
8	.38	181-	J- 4.10	109-	57.		
9	B	61.57	CG. 1-10	51.9-0	.05		
10	186	F 1.31	- 3 53	1-5-47	180		
11	3.57	5T	2-1.73	3.13	3.34		
12	6.38	12.17	1-11.63	1	5.77		
13	8.91	19.11-	1-31.63	1. 33	-9.55		
10	17.7-	-1533	3-25.85	142.40	-8.42		
15							
16	15.51	Č.	- 4.55	1-5.57	45		
17	.87	12.1-	1-3.23	1-4 51	.73		
13	07.	12 1-	11-3.00	1.4.23	09.		
13	-1.03	-5.20	16.1 - 2	-3.54	86 -		
30	72	-718	- 15.13	-2933	63		
21	38	200-	P-13.77	1.29.43	15 -		
22	- 69	01.7-	J-14.72	-25.7	82		
23	- 70	29 4-	2-753		BL: -		
74		1.4.20	7-927	112 27	80.		

Table 35. Strain Gage Results for Compression Loading at 1000 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

GAGE	MEASURE	MEASUREI	STRES	STRESS (KSI)	RESS (KSI) AT APPL	AT APPLIED AXIAL LOAD (KIPS)
NO.	ØB.1.	-10	-20	-29	ØB.1.*	
20	71.	-6.70	1001-	-16.9	0	
20	E. 1	-2.30	56: L-	1	1.87	
27	Tr. I	14.8-	- 3.63	-12.31	177	
23	69.4-	61.6-	-13.39	C1.41-	F4.4-	
63	2018-	126-	51.21-	-12.23	-375	
3.1	12.29	CE:2-	11.7 L	-10.73	オナン	
3:	1.73	528-	116-	24.11-	18	
32	92.1	C9.1-	8611-	19.12-	(2)	
33						
34	1.56	21.5-	オセ・ーー	20.7	1.53	
35	.39	-6.37	Co.21-	25.92-	€. 1	
36	CA. 2	952-	00 0-	18:9-	2.36	
37	10.8	11.2-	11.8-	16:11-	2.89	
35	12.0	E'	06.9-	21:31-	6.00	
3.1	3.35	CL' -	-3.35	29.8-	3.62	
90	OC 2	25.5-	29.07	76.6-	1.73	
41	21.2	CO: 2-	14.6-	169.11-	2,42	
42	.36	21.1-	FC. P-	-13.19	.00	
43	45.	21.4-	10.39	16.91-	.31	
44	.13	-4.58	-3.67	51.61-	80	
49	11	C6'S	22:11-	16.29	65	
46	53	L1.5-	10.42	15.27	7.	
41	25.	-1.73	- 3.50	19. 1-	130	

Table 36. Strain Gage Results for Tension Loading at 1405 Flights-AFCG-3 HANGING FREE B.I. BOLTED IN H.F.

3	MEASURE DE	15	DEC /VCI) AT ADDI	AT ADD	74	100 VIV. 040 I IA	
	MEASURE	-	SIRESS (KSI)	AI APP	LIED AX	AI APPLIED AXIAL LOAD (KIPS)	
98.I.	.* 10	20	30	40	05	09	
2.	12 % 32	2 5.48	18.19	18:01	13.54	02. 91	
	1.21	_	7.92	35:01	02.81	15.83	
3.	18:2 W	N 5.42	11.8	18:01	13.53	02.91	
`.	12 2.19	9 15.22	361	89:01	15.21	16.10	
7,	154 2.79	1 5.25	7.30	10.90	13.02	15.61	
4	51.2 08	5 5.38	PP 7	10.60	13.26	15.30	
	84.2 LI		7.26	9.65	12.03	19.91	
61.	P 2.39	P1 4.79	11.7	686	88.11		
1.	7 2.82	21.9 2	7.05	9.38	21.11		
7	23 239	1 4.63	613	9.30	29. 11	13.94	
2.3	23. 66.	2-1.13	12:1-	10.1-	59	- 39	
-37	34 05	8 3.33	12.0	6,63	7.89	10.6	
130	58.8	16.6 2	10.17	10.25	10.30	10.3%	
151	1.93	8 8.73	9.30	9.40	84.6	25.p	
					-		
-1019	91.5	.24.2	158	12.00	18.71	16:22	
503	3 2.77	1 5.16	19.7	10.09	12.5	22.41	
12	1256	17.77	7.00	9.90	08:11	22.41	
01	18.9	69.61	19.72	19.80	36.22	110%	
75	2600	0 12.75	18.44	29.02	29.59	35.11	
72	12.0 2	09.11	00.TI	22.39	27.80	22.88	
39	960 3	58.21 6	199. TI	23.42	68.82	62.08	
132	11 9 2	1 9.63	14.00	19.79	0052	30.22	
57	7 60	000	1 9 - /1	1 02	12 20	20.0	

* With Buckling Restrainers Installed

Table 36. Strain Gage Results for Tension Loading at 1405 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

COMPLETE AT APPLIED AXIAL LOAD (KIPS)	09	30.72	35.39	34.87	84.0	40.6	35.02	32.66	35.11		06.2	30.36	35.85	37.00	38.30	35.80	31.31	3212	11:08	33.07	32.39	33.68	82.18	14.67	
IED AXIA	20	25.61 3	8 11.73	3	9.49 110	8.15	29.13 3	28.763	28.89 3	İ	06:22 31.61	29.99 3	29.72 3	30.96 3	32.19 3		26.01 3	26.90 3	25.07 3	27.68 3	26.93 3	28.16	26.08 3	12.13 1	
1405 FLIGHTS COMPLETE RESS (KSI) AT APPL	40	02.02	22.05	23.28	8.30	7.23	72.27	16.22	22.63		13.36	19:50	13.67	18.37	26.95	23.38	20.70	21.65	19.97	22.23	85.12	12.01	20.75	9.60	
STRESS (KSI)	8	15.40	14.51	17.47	7.22	18.91	17.40	17.09	16.33		0.6	13.39	17.65	18 22	19.73	17.29	15.96	16.38	19.90	81.91.	16.07	17.00	15.53	7.22	
ST	82	10.34	10.38	11.00	1999	648	11:52	11.30	9.78		4.09	7.99	27.11	12.80	13.52	11.33	10.20	11.11	186	11.33	10.75	00:11	10.36	06.4	
TEST CONDITION	10	5.33	5.54	40.0	4.24	4.16	5,35	5.74	2.79		06.	.25	6.21	16.91	7.30	5.86	5.23	5.86	4.95	5.82	5.52	266	5.23	C0: 2	
TEST C	98.1.*	.5	10.	.78	32.	14.	00).	Ğį.	-3.38		06.1-	-7.15	1.24	1.35	1.92	1.14	29.	18.	.39	157	00%	12.	.36	166	
STRAIN	NO.	12)	110	17	23	13	3.0	3/	25	33.	34	35	30	27	32	39	03	13	24	43	11	12	40	1.7	

* With Buckling Restrainers Installed

Table 37. Strain Gage Results for Compression Loading at 1405 Flights-AFCG-3 H.F. HANGING FREE B.I. BOLTED IN

GAGE							
NO		MEASURED		S (KSI)	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	JAD (KIPS)	
	ØB.I. *	-10	-20	-29	* 08.1.		
_	22.	85.2-	- 5.12	1811-	22"		
7	.29	12.29	TL 9-1	760-	Q1.		
3	:43	50.5 -	-9.93	280-	80,		
بر.	80	11.2-	-6.48		92		
S	507.	102-	159-	11	02'		
7	- 28.	88: 2-	1 5.09	78.7-	61.		
1	81.	1.2-	12.91	81.0	3.		
af :	12.	01.5-	- 4.33	9-	01.		
7.	11.	60 2-	1	840	<i>3</i> :		
u.	62:	86 1-	02.4-	01.0	11.		
11	28.2	18.8	19.23	27.33	4.03		
21	128-	-20.03	1	31.81-90.02	-9.80		
13	8.	-12.03	10.02-	-35,83	₽ 1.		
16	19	-10.33	6262-	-35.08	01		
13							
9)	-6.12	66-	21.7	1662-	55.65		
17	.03	951-	12.96	DL: D-	Oct.		
10	166	1-1,53	-3.28	<u>ب</u>	26		
11	02:	-3.92	6.33	18:2-	26.		
02	.78	-5,62	-13.30	-27.10	40.		
12	.18	-9.33	61.21-	55.92-	or.		
22	15.	-5.33	- 13.22	08.82-	189		
22	13.	-3.63	9-	14-6.47	.36		
12	525	1.	19.19	-12.13	153.		

Table 37. Strain Gage Results for Compression Loading at 1405 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

CTDATA	IEST	LEST CONDITION:	1	1403 FLIGHTS COMPLETE	Jul 6616		
GAGE		MEASURED		S (KSI)	AT APPLIED A	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	
NO.	ØB.I.*	-10	-20	-29	* ØB.I.		
200	0,00	Fq 38	29.60	5201-00.	18	20,63	
20	60	12.4-	22. 6-	26.31-	20.		
27	18	-4.39	-9.38	18-11.60	.92	30.4	
23	35	-3.93	B1-	V5.30	45.		
23	.40	-3.00	7 _	-3.75	20.		
30	63	-9.36	-608-	02.01-	26'		
31	50	1-	19.83	-16.79	99.		
32	18:5-	1-10.96	-21.35	-31.46	-4.03		
33							
34	04.1-	10	10.03	10.03 19.92	201 -		
30	11.7-	FIG. 78	-29.35	29.3939.17	-8.03		
36	18.1	1-3,10	15.52	01.5-	1.21		
3.7	14:1	61.2-	-12.93				
38	03.1	10.12	-13.09	08-22-80	1.19		
39	12.1	06 2-	16.99	-3.20	.99		
8	10).	-3.93	1.09	19.75	.42		
9.1	.96	09 b-1	10.28	0.52-17.22	20.		
92	74.	52 b -	- 8.73	-12,69	9		
43	00.	1-9.95	1	10.34-19.75	.36		
44	.75	-4.03	1-8.18	10.34	05.		
45	,53	1-4.99	-10.30	-19.23	24.	THE TONE CREEK	
46	960	16.52	19.41	19,12	12.		
11	64.	105	B2.8-	16.7-	85.		

Table 38. Strain Gage Results for Tension Loading at 2520 Flights-AFCG-3 BOLTED IN HANGING FREE H.F.

S COMPLETE AT APPLIED AXIAL LOAD (KIPS)	09	14. 01	16.32	16.75	16.31	15.64	15.78	64.41	14.43	14.35	12.79	-2.36	8.20	02.01	60° b		907-	15.25	14.91	30.03	43.64	35.72	38.47	30.32	37.62	
IED AXI	50	13.74	13.60	13.56	13.61	13,03	13.17	12.39	12.09	11.97	12.33	-2.35	8.13	10.23	9.03		-4.05	12.69	11.50	18.87	38.12	30.30	33.20	2507	31.43	
2520 FLIGHTS COMPLETE ESS (KSI) AT APPLI	40	16:01	19.33	10.32	10.95	10.41	25:01	3.60	7.65	1.57	20.0	-2.33	3.16	10.21	1.04		-4.03	10.03	90.6	19.67	125.47	16.42	40.72	17.77	25.17	
FLIGHTS (KSI)	30	42.6	8.10	3.15	8.15	7.26	7.94	7.26	7.24	C2. T	ーナー	61.3	00.6	420	11.1		-4.05	7.53	1119	+.53	26.33		16.53	7.0. Y	19.73	talled
STRESS	20	15.51	5.36	5.39	5.38	5.22	5.32	1.87	4.93	18 1	4 75	-1 33	01.7	19.15	3.39		-3.44	5.02	1.37	7.63	TS 15	40 tl	14.21	362	13.71	ners Installed
TEST CONDITION:	10	2.77	UL 3	2.73	2.63	2.35	2.70	2 +8	2.46	25.5	2.55		4.33	14.6	151		12.1-	2.60	2.15	4.73	15 47	3.64	19.65	15/ 1		_
TEST CC	ØB.I.*	9	64.	10.	191.	(0)	07	11.	.23	. 26	28	01.1	16-4-	20	88: -		70	,53	.13	05	9.19	40.2	bs: b	.26	69.2	With Buckling Restra
STRAIN	NO.		1	12)	2	**		30		-		. 21	13	٠,٠	2	9	17	13	11	02	17	2	23		* With

Table 38. Strain Gage Results for Tension Loading at 2520 Flights - AFCG-3 (Continued) H.F. HANGING FREE 8.1. BOLTED IN

		80					8																		
(KIPS																									
AL LOAI	09	35.21	29.19	29.73	4.89	20.4	18.83	19.00	3.69		24 -	4.33	20.	16.92	7,63	15.	36.26	39.26	30.51	33.67	32.60	39.10	31.90	29. 11	
E. IED AX	50	29.34	13.35	19.77	4.35	3.33	15.13	15.34	3.67		16	48.4	35	16.31	7.72	.43	32.18	33.25	25 35	23.22	11.72	28.56	26.12	12.07	
S COMPLETE AT APPLIED AXIAL LOAD (KIPS)	40	23.25	14.53	15,19	4.78	3 75	11.36	11.57	3.63		12. 1	4.36	137	633	7.33	12.	80.93	61.73	20.15	F0. 25	85 12	22.93	58.02	9.56	
2520 FLIGHTS COMPLETE STRESS (KSI) AT APPLI	30	CZJ. [1	7.67	10.40	4.70	3.12	7.53	7.80	3.65		1.54	4.52	73	6.33	11:0	I.E.	13.11	61.13	15.00	C2.71	10.17	17.37	15,62	7.14	
STR	20	1 30	4.39	5.51	4.73	4.05	3.75	3.62	3.65		.05	3.30	00 -	6.9	4.31	64.2	12.24	1514	4.33	11.66	19.73	11.79	12.43	4.73	
TEST CONDITION MEASURED	10	6.57	-1.69	.53	5.12	6:4	- 45	12.2-	80 2-		3.22	-4.37	2.53	20.2	1.67	4.17	6 93	826	40.3	01.0	599	22.9	5.32	15.5	10000
TEST (ØB. I.*	1.39	-6.10	-4.33	1.36	1.75	-5.32	-7.95	11.61		7.14	15.51-	15.5	CF. T-	16.9-	IT. L	2:32	3.78	44.	16.	63	16	ナ	.36	
STRAIN	NO.	200	3.5	2.1	40	62	30	3/	32	33	3;	35	30	37	35	89	01	<u> </u>	12	:3		125	27	17	

* With Buckling Restrainers Installed

Table 39. Strain Gage Results for Compression Loading at 2520 Flights-AFCG-3 HANGING FREE B.I. BOLTED IN H.F.

GAGE		MEASUREI	D STRES.	S (KSI)	AT APPLIE	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	
NO.	98.1.*	-10	-20	-29	08.1.		-
-	ā.	-2.93	-5.20	1.87	81.		
1	.35	-2.28	1	1.12	81.		
3	J.	16.1-	-4.34	62 9-	C1:		-
4.	12.	662-	-534	0	Ø1		
5	.62	90.1-	15.4-	02.0-	22' .		
9	35	12.31	_	-7.35	91.		
7	22.	11.2-	-4.55	-4.73	5.		-
8	22	80.2-	-4.42	19.9-	61.		
9	.31	161-	51.4-	16.37	92.		
10	.38	002-	64.4-	-653	62.		
11	14	16.8	19.94	2323	2.02		
12	15.6-	-17.31	12.62-	-37.02	-5.79		
13	64.	-13.73	45.92-	-3543	16		
19	10	-12.79	29.02-	5558-	62.1-		
5				İ			
16	53	6.02	15.15	19,22	38. 1	700	
17	1 (5)	00.1-	13.54	ne.1 -	.39		
5	12	116.1-	-3.72	18.4-	10		
-	17	8	-68.9	-3.13	.23		
22	9.31	08:2	17.4-	11.61 -	9.38		
1	22.8	24.2-	-9.15	15 23.59	3.16		
22	9.73	-1.72	TC. F-	19.81-	4.55		
23	24		-665		.33		
76	1877	1-1-16	-5.30	-5.67	2.70		

Table 39. Strain Gage Results for Compression Loading at 2520 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

URED STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	-20 -29	-9.79 -18.08	-17.98-	10-11.94-5.80-4,00	33-3.70 5.90 2.15	59-3.13 6.56 2.05	18-11-91-4.96-4.89	77.7-828-17.59-19.59	75.51 26.92	37 34.56 4.38 10.90		28.05 35.44	140 - 31.88 - 38.89 - 8.05	92-2789-34.0 -7.69	00 23.88 29.77 9.32	96-4.53-4.25 2.10	01.11-1	02. 08.21-08.8-11.	-10.30	03 - 8.30 - 10.09 .50	-1019 -14.23	41 -9 43 -14.23 .26
STRESS (KSI)	20	19-18	98-	1.99-11	5	0	1	1											-10.30 -1892	8.30-10.08	10.19	1
E -	-10	- 3.73	1	-8.76	.98-1.73	-87-1-59	-12.21 - 9.48	-7.77-15.25	11.26-26.11-	0.99 21.37	-15.09 -3792	5.24 16.26	-6.55 -0.40	-6.38 -17.92	3.04 15.06	196-1-01.2	452-	1117-65	10-4-01	_	64-4.70	57 - 9.41

* With Buckling Restrainers Installed

Table 40. Strain Gage Results for Tension Loading at 3640 Flights-AFCG-3 HANGING FREE B.I. BOLTED IN H.F.

	LICASONE	D STRES	CICA)	AI APPI	-ICD AA	SIRESS (KSI) AI APPLIED AXIAL LOAD (KIPS)
ØB.1.*	10	20	30	40	50	09
<u>e</u> .	2.85	1550	8.30	11.0%	13.79	10.51
.32	2.82	9.38		10:36	15.58	16.30
.72	3.2	25.0		10.30	13.49	12.91
8	2.47	10.0	7.22	10.50	13.26	15.48
8.	2.88	42.0	7.35	10:40	66.21	12.6
123	2,77	65.63	LEL	10.58	13.19	15.83
19	2.53	Cb.4	7,34	9.77	12.18	14.60
42	2.50	1.33	L	2.60	12,07	64.4
14.	2.72	11.9	00. T	10.20	12.73	15.26
24.	7.67	10.0	641	10.08	12.57	10.08
1.13	17	Cb:1-	02:2-	62.2-	-2.31	-2.33
12. 1-	3.76	15:11	11.39	11.98	199	11.99
90	7.19	10.85	0601	1989	00.00	10.93
10 -	8.36	990	7.72	686	9.87	186
9	-2.13	-3.99.	16.8-	-3.99	4.00	207-
21.	2.30	15.17	11,7	10.22	12.80	15.61
.43	2.48	4.67	00'1	9.36	21.11	19.22
9.	10.0	666	14.91	01:03	25,20	30.94
13.6	17.24	64.62	29.97	25.95	40.86	96.50
13.35	24.40	30.17		-	46.88	5235
.39	4.93	9.75	14.83	10.03	20.00	30.54
11,7	117		00			

Table 40. Strain Gage Results for Tension Loading at 3640 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

STRAIN		MEASIIBET	_	CTDECC (KCI) AT APPI IED		I TEN AV	AT APPI IED AYTAI I DAN (VIDE)	
GAGE		TOS TO				W 1	INC LUMB (NIFS)	
6	*0B. I	0	20	30	040	50	09	
250	-11.36	-4.19	3.	176	13	17.	66.	
200	19.57	1-6.50	30.	01	61	82: -	33	
27	-1.00	40	-1.63	65-1-1	751-	1.27	-1.23	
23	15.44	100	4.33	01.1	66.5	68.4	4.96	
12	4.39	10.34	4.13	8.39	86.8	4.97	294	
30	10.	1- 39	19.1-	OL: 1-	3031-	1.43	-1.43	
31	-13.72	19.01	12	202	77.	18'	\$	
3.	-10,95	1-1.07	4.24	120 1	4.10	4.25	4.25	
35								
3;	9.18	3.00	36	02-	<i>eo</i> -	03	16	
31.7	11011-	-4,13	5+	642	58.0	5.26	25.62	
30	6.25	19.2	33	16	36.	40%	20.	
37	4.63	12.72	10.70	81.01	bL 01	10.90	06:01	
53	-4.22		196	19.77	ab	216	11.6	
29	11.F		LLI	LL.	BE.	10:1	0.	
64	6.17	16.2	24	86.	po	90' -	10	
41	bc. 2	066	19.75	115.16	157.25	15.27	15.27	
42	200.	10.22	10.09	15.18	10.29	2002	30,58	
43	69. 1	10.04	12.97	18.02	23.52	00.62	39.48	
44	16.	1593	01:11	64.91	06.12	98'12	35,35	
45	61.1	11.0	12.21	17.92	12.82	23.96	39.53	
46	74.	15.90	10.01	15.73	36.C2	26.13	31.95	
47	.43	76.5	16.2	7.10	9.58	10.21	12.60	

95

Table 41. Strain Gage Results for Compression Loading at 3640 Flights - AFCG-3 H.F. HANGING FREE B.I. BOLTED IN

STRAIN		MEASURED	100	TRESS (KSI) AT APPLIE	AT APP	AT APPLIED AXIAL LOAD (KIPS)	
M	*0B.1	-10	-20	-29	*0B.1.		-
1		- 2.40	02.4-	1	8-		7
2	.32	-2.33	1.4-	11.1-	11.		
3	315	-1.92	-4.34	- 6.25	36.		
4	20	18.5-	1007-	12.6-	79		
0	P.C.	46.1-	62.4-	-6.23	8		
0	.35	28.2-	10.09-	-7.88	少、		-
7	02.	01.5-	4.02	PC. 7 -	5		-
e	22.	01.2	-4.36	02.0	01.		
4	14.	1 - 1 -	- 4.53	41.7-	68.		
10	24	UP 1-	-4.30	9-	62.		-
	4	900	19.36	27.75	2.23		
12	- 93	-13.31	-24.25	22.78	-1.79		
13	.75	-13.96	-25.79		69		
14	.20	-13.42	-1569	-34.65	199		
(7)					•		-
2	25	21.9	14.09	27.28	75		
17	.72	19.1-	-3.31	165.4 -	,53		
18	.42	19.1-	-3.35	74.9-	26		
19	153.	-3.87	-6.75	88:2	3.		
02							-
12	13.29	803	1.13	-15.26	13.61		-
22	18.39	11.95	4.17	-0.37	18.16	The same of the sa	
23	74.	-3.53	10.01		.39		
20	7 60	1.13	72 75	27 19	272		

Table 41. Strain Gage Results for Compression Loading at 3640 Flights - AFCG-3 (Continued) H.F. HANGING FREE B.I. BOLTED IN

GAGE	MEASURE	MEASUREI	D STRES	STRESS (KSI) AT		APPLIED AXIAL LOAD (KIPS)	
NO.	ØB. I*	-10	-20	-29	MB. I.*		
u	-11.13	-10.18	-38.49	-50.55	00:21-		
20	-19.35	-2289	-44.81		-15.57		
1.7	-1.00	4.30	26.90	40.39	.02		
22	17.0	7.25	80.62	06:24	2		
29	4.90	82.0			93		
30	08	3.24		3804			
31	-13.53	8 252-	40.24-		-14.48		5.6
32	01:01-	-26.36	-40.55	100	-12.93		
33							
36	8.8	23.35	35.19	02.20	12.58		
R	15.00-30.8	-30.87	18.29-		- 18.90		
360	10.01	16.04	01.75	33.95	7.53	over Book Espirated and against	11.5-1
37	12.4-	-17.62	98:12-		- 5:58		10.50
38		-15.40	1632	-3033	- 5.25		5-1
39	6.98	19.60	23.15	6982	8.10		3.0
00	21.4	20,9	01.12	61.62	02.0		0.5 3 %
17	2.30	1	1522-	11.62-	000.		
42	63	-4.15	19.6	-12.52	.23		
43	80.1	-394	-9.35	-13.62	1.32		
44	1.79	- 5.78	-7.83	-9.86	77.		
3	1.19	-4.36	-9.53	-13.17	1.03	TAN DAO FERMANA GROOM	
20	S.	- 4.45	-9.40	-19.19	20		
17	.43	- 1.55	-3.27	-4.35	₽.		

Table 42. Strain Gage Results at Start of Test - AFCG-4 B.I. ~ BOLTED IN H.F. - HANGING FREE

GAGE		MEASURED		SINESS (NSI)		MELLICD MAINE	IAL LUA	LUAD (KIPS)	,			
3	O H.F.	TA O	2	10	20	30	35	37.5	OBI	1,	01-	71-
-	0	22	1.07	2.36	4.91	7.46	12.8	9.34	52:-	-1.42	152-	-3.01
2	0	.25	1.46	2.10	5.21	17.6	8.96	2.58	.25.	2.38	-205-	-7.53
2	10.	07	1.2.1	2.52	5.12	7.75	9.08	-1.5	207	-1.20	212-	-2.57
4	10.	.09	1.38	17.7	5.37	8.02	0.33	866	60.	6111	-776	75.2-
S	0.	83	.34	1.63	4.24	6.87	2.17	8.83	1.69	66.1-	-356	1400
٩	10.	.54	1.84	3.19	5.89	8.56	9.88	10.54	.57	87	-2.60	3.23
7	10.	113	1.23	2.34	4.58	6.82	7.93	8.49	0.	1.38	-2.65	-2.50
80	0.	1.01	1.12	2.27	4.57	6.89	40.8	8.62	20.	-1.00	51.2-	-760
0	0.	6).	1.30	2.42	4.64	6.88	7.99.	8.54	21.	.95	-2.15	-7.62
10	10	21	1.05	2.25	4.63	7.01	8.30	8.79	07	-1.26	-2.52	-3.01
=	0	.45	2.80	5.16	9.82	14.51	(8.9)	18.07	.53	16.1-	-4.51	-5.60
12	0	.4.5	2.76	5.14	9.97	14.91	17.46	18.71	.36	-1.85	-3.94	-4.76
13	-0.	.47	2.80	5.23	10.18	15.24	17.83	19.11	.38	-1.84	-3.95	404-
+	10.	.55	3.09	5.67	18.01	15,97	18.58	19.88	T.4.	-2.06	164-	-5.75
15	0.	47	2.76	5.10	9.78	14.53	16.32	1812	.49	1.94	1435	-535
و	10.	1.67	2.25	5.18	11.01	16.84	19.74	21.20	73	-3.47	-6.33	-7.50
17	.02	62	5.19	5.00	10.60	16.22	19.00	26.41	68	-3.34	-6.17	-7.30
18	0.	-65	2.22	5.09	20.01	16.38	19.7	20.55	76	-3.52	-6.54	-7.73
19	0	53	1.97	4.48	9.44	14.43	16.91	18.16	55	-2.98	-5.65	697
3	jo.	B1	2.30	4.51	9.77	14.73	17.20	18.45	30	-2.54	-5 30	-447
77	.01	20	2,26	1.81	9.96	15.20	17.87	19.14	80.	-2.52	409	25.78
22	70.	81	2.25	4.80	10.03	15.39	.81	19.45	50	-2.41	-4 50	5.5
23	.02	41	2.47	5,15	10.52	15.35	10.	20.00	101	-7.61	-506	203
24	10		7.32	4.4	0 10	16 41	100	7 - 6	5		V C	2

Strain Gage Results at Start of Test - AFCG-4 (Continued) 8.1. BOLTED IN Table 42. H.F.

.04	Ø H.F.	Ø BI.	3	01	20	30	35	37.5	JBI.	- 5	01-	-12
25	10.	.59	2.94	5.42	10.45	15.53	18.07	19.35	.57	-2.03	-4.68	-5.67
36	80.	89.	3.28	00.9	11.47	16.55	13.65	21.01	.58	-2.26	-5.11	-6.19
27	127	68.	3.54	6.30	11.87	17.44	20.19	21.57	.77	-2.11	-4.45	-6.04
28	.26	90	3.61	6.45	12.15	17.84	20.66		37.	-2.14	21.4-	-6.21
								13 Pri				T.
100				3	100						Y	100
						- T	(A 4)					
	0							Die Co			9	
					100 100 100 100 100 100 100 100 100 100							e.
		100					IIA					
					43							
1	1000	The state of										
		1 1 1 1										
	Section 1											
						H H						
		25.7.38							2			
		Cespita	Shirt .			2003						
Andrew Market		The second second	Commence of the Commence of th		The second second second	Secretary of the second	Section of the latest section of the latest	The second secon	The second second second second			

Table 43. Strain Gage Results at 2 Flights - AFCG-4

BOLTED IN HANGING FREE

STRAIN		TEST CONDITION MEASURED	STRESS	S (KSI) A	AT APP	2 COMPLETE APPLIED AXIAL	PLETE AXIAL LOAD	(KIPS)				
NO.	Ø H.F.	Ø B.1.	ō	20	30	40	50	09	ØBL*	-10	-12	ØBI.
-	0.39	.50	2.93	5.45	7.95	10.48	13.03	15.57	.53	-1.73	-2.21	.48
7	0.38	1.14	3.53	6.07	8.63	11.23	13,84	16.43	1.15	-1.25	-1.74	1,02
m	06.0	12.1	3.40	5.87	8.44	11.02	13.65	16.28	1.23	64	-1.09	1.01
4	66.0	1.83	4.14	6.70	9.28	11.86	14.48	17.10	1.86	14	64	1.69
Ŋ	-1.49	59	1.83	4.39	٦.٢	9.79	12.48	15.16	·. sa	-3.90	-4.44	-1.05
O	-0.24	.63	3.26	5.96	8.72	11.42	14.13	6.83	.67	-2.84	-3.46	15.
7	,33	65.	2.78	5.05	7.30	9.59	11.89	14.18	19.	- 1.52	-1.97	.54
œ	99.	1.03	3.15	5.41	7.67	9.94	13.23	14.51	1.04	86	-1.42	.92
0	(5	.13	2.43	4.77	7.07	9.39	11.71	14.02	91.	-2.43	- 2.91	01.
0	01.	1.54	3.85	6.25	8,63	11.00	13.40	15.76	1.56	- 1.00	-1.48	144
=	16.	.73	5.43	10.23	14.93	19,68	24,46	29.22	16.	- 4.21	- 5.37	.59
12	1.01	.94	5.67	10.67	15.67	20.78	15.97	31.12	.90	- 3,58	- 4.39	98.
13	.58	\)					
14	.52	.28	5.54	10.93	16.21	21.54	26.91	32.21	.30	-5.39	-6.46	61.
15	.45	.50	5.23	10.11	14.93	19.83	24.79	29.73	.64	-4.58	-5.63	.39
9	.30	2,01	7.73	13.66	19.69	25.89	32,19	38.47	2.07	-3.68	-4.86	1.93
	00.	.84	6.30	11.93	25.71	23,22	28.99	34.74	89	-4.64	-5.74	11.
8	30	9 .	5.78	11.49	17.07	22.69	28.34	33.94	91.	-5.67	-6.82	60.
6	37	.24	5.10	10.10	15.02	20.00	25.03	30.06	.31	-4.76	- 5.78	16
20	.97	1.49	6.31	1 - 1 - 1	15.95	20.80	25.08	30.53	1.59	-3.72	- 4.80	1.25
71	.92	1.50	6.33	11.47	16.63	31.85	27.11	32,35	151	-3.45	-4.32	1.28
22	1.18			1		1			(1
23	1.64	2.14	7.09	12.38	17.66	23.00	29.38	33.73	2.13	£7.5-	-3.66	1.89
24	1.70	2.06	6.63	11.48	16,34	21.24	26.20	31.14	2.17	-2.53	-3.52	1,83
+ Wi	th Buckl	With Buckling Restrainers		Installed								

Table 43. Strain Gage Results at 2 Flights - AFCG-4 (Continued)

STRAIN	TEST	TEST CONDITION:		STRESS (KSI)	The second second	AT APPLIED AXIAL LOAD (KIPS)	AL LOAD	(KIPS)				
NO.	Ø H.E.	Ø 8.1.	0/	20	30	40	50	09	# POBIL	- (0	-12	ØBĪ
25	51		4.63	9.85	15.09	20.39	25.76	31.10	21	1	-6.77	53
26	32	.07	5.47	11.17	16.86		28.39	34.12	.10	- 5.83	-6.93	21
27	01 -	27.1	6.62	12.41	18.31		30.04	35.94	1.19	12.4-	-5.80	.87
						f						
		TO A SALES		1345				18.0				
		The state of										

Table 44. Strain Gage Results at 499 Flights - AFCG-4

H.F. HANGING FREE

STRAIN		MEASURED	STR	SS (KSI)	1	AT APPLIED AXIAL LOAD	D AXIAL LOAD	(KIPS)		П	
a	ØBI	01	20	30	40	50	09	ØB.	-10	-12	ØRI.
4.	\$	2.92	5.43	7.93	10.50	13.01	15.58	15,	- 1.76	- 2.21	.47
1.17	7	3.61	01.0	8.66	11.29	13.87	16.50	81.1	-1.24	07.1-	1.07
1.15	2	3.48	5.81	8,35	11.00	13.59	16.26	1.17	4r	517-	96.
1.80	0	4.2	6.66	9.22	11,86	14.43	17.09	1.83	20	66	1.67
49	64	1.98	4,46	7.12	9.87	12.53	15.24	52	-3.85	-4.36	96
9	.65	3.34	5.95	8.67	11.43	14.09	16.82	.67	-2.86	-3.43	.33
	09.	18.8	5.05	7.29	19.6	18.11	14,20	.62	-1.52	-1.95	.56
0.	86.	3.16	5.35	7.60	16.6	12.17	(4.48	66.	-1.06	-1.47	68.
9	90	2.37	4.68	6.38	9.33	19:11	13.95	60.	-2.51	-2.97	40.
-	1.39	3.75	6.03	8.47	68.01	13.23	(5.63	1.42	-1.19	-1.63	1.31
	80	5.57	10.27	14.96	19.78	24.46	29.27	66.	-4.16	-5.25	69.
7:	00.1	577	10.70	15.69	20.85	25.94	31.17	96	-3.55	-4.32	46.
1	1				1		1	1			1
-	37	5.68	10.97	16.24	21.63	26.89	32.27	04.	-5.33	-6.34	.31
	.55	5.33	10.11	14.92	(9.89.	24.74	29.74	69.	-4.56	-5.55	14.
7	2.25	8.04	13.93	20.04	26.43	32.69	39.15	2.34	-3.54	-4.65	2.21
0.	.93	6.43	13.01	17.62	23.43	29.12	34.98	1.00	-4.60	-5.64	16:
(;	17	5.87	11.52	17.11	22.81	28.37	34.07	42.	-5.66	-6.73	61.
	38	5.18	10.11	15.04	20.11	25.06	30.16	.36	- 4.75	-5.69	.25
1.5	1.50	6.35	11.11	15.92	20.85	25.64	30.54	1.60	-3.76	-4.77	1.28
1.	1.49	6.44	11.46	16.59	21.84	27.05	32.35	1.50	- 3.52	-4.33	1.30
1	1	1	1	1	1	1		1	22.60	11.18	1
7	2.10	7.21	12.35	17.61	23.00	28.29	33.72	2.09	- 2.82	-3.70	1.88
	(107	63	75 71	0000	0. , .	0	000			

Table 44. Strain Gage Results at 499 Flights - AFCG-4 (Continued)

HANGING FREE

STRAIN	3	MEASURED		(KSI)	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	IED AXI	AL LOA	O (KIPS)			
.0v	OBE	0)	20	30	40	50	60	ØBI.	01-	-12	ØB.
25	28	4.77	9.84	15.05	20.46	25.76	31.19	12		-6.77	50
26	.15	5.68	11.23	16.89	22.75	28.47	34.32	81.	-5.78	-6.80	01.1
7	1.42	7.01	13.64	18.42	24.44	30.33	36.36		-4.46	-5.46	1.17
28	1)	1	1			9	81.09	56.73	60.06
	100					1.1					200
T											
T				6-					100	(A)	Ç.
	200	10.11.0				MO THE DATE	10	6			
		2000					18		100		100
								20.7			E
	14	12000	0.00							The Part of the Pa	5.7
	1000							5.00		300	
		18.0				1 - 1		12	120		
							4 5 6				
			- F. S.			I.		080			
						7.3			-		
			40.00				200	6.7			
						18 8 1					
		1 1 1 1 1				1000		\$ 5 S	10)		
4									i i		
						A A TOTAL		CKIBC			
	1211	0.0000		ıl.			100 Jan 100 Jan 1				

103

Strain Gage Results at 631 Flights - AFCG-4 Table 45. H.F. HANGING FREE

B.1. BOLTED IN

TEST CONDITION:	TEST CONDITION: FLIGHT G31 COMPLETE													
*** SAB*** *** SO 40 50 60 68*** -10 -12 *** 37 *** 38 *** 18** *** 104** *** 185** *** 45 -18** -299 *** 16** *** 18** *** 18** *** 18** *** 18** *** 18** -18** -18** *** 18** *** 19** *** 18** <th>*** (ABL**) *** (ACC)** *** (ACC)*** *** (ACC)*** *** (ACC)*** *** (ACC)*** *** (ACC)**** *** (ACC)**** *** (ACC)***** *** (ACC)***** *** (ACC)***** *** (ACC)****** *** (ACC)******** *** (ACC)********* *** (ACC)***********************************</th> <th>STRAIN</th> <th>TEST</th> <th>CONDITION MEASURE</th> <th></th> <th>=</th> <th>ATA</th> <th>LIED AXI</th> <th>MPLET AL LOAI</th> <th>(KIPS)</th> <th></th> <th></th> <th></th> <th></th>	*** (ABL**) *** (ACC)** *** (ACC)*** *** (ACC)*** *** (ACC)*** *** (ACC)*** *** (ACC)**** *** (ACC)**** *** (ACC)***** *** (ACC)***** *** (ACC)***** *** (ACC)****** *** (ACC)******** *** (ACC)********* *** (ACC)***********************************	STRAIN	TEST	CONDITION MEASURE		=	ATA	LIED AXI	MPLET AL LOAI	(KIPS)				
182 4.19 6.72 10.30 13.52 14.52 1.45 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.168 1.121 1.121 1.121 1.121 1.121 1.122 1.120 1.130 1.121 1.121 1.121 1.122 1	.37 — 5.36 1.87 10.41 12.94 15.52 .45 -1.88 -2.99 1/16 — 6.16 6.12 1.12 1.12 -1.21 -1.68 1/16 — 6.16 6.12 1.12 1.12 -1.21 -1.12 1/82 4.19 6.26 9.32 11.92 14.52 15.26 -1.86 -3.85 -4.37 54 1.92 4.50 7.86 11.41 14.10 16.26 -1.86 -3.85 -4.37 .56 2.78 5.29 7.86 11.41 14.10 16.26 -4.86 -3.85 -4.37 .67 3.29 1.20 1.42 -93 -1.12 -1.20 -1.20 -1.20 .87 3.04 5.29 7.54 1.185 14.42 -93 -1.52 -1.20 .87 3.04 3.05 1.185 1.42 -93 -1.12 -1.20 .87 3.06 <th>MO.</th> <th>ØBI</th> <th>17</th> <th>20</th> <th>30</th> <th>40</th> <th>50</th> <th>90</th> <th>ØBI.</th> <th></th> <th>-12</th> <th>ØBI.</th> <th></th>	MO.	ØBI	17	20	30	40	50	90	ØBI.		-12	ØBI.	
1.06	1.02	-	.37	1	5.36	7.87	10.41	12.94	15.52	,45	-1.88	-2.99	.42	
1.82	101	7	1.16	1	6.16	5.72	11.34	3.75	16,60	1.23	-1.21	-1.68	1.12	
1.82	1.82	m	10.1	1	5.73		10.30	13.52	16.21	1.07	48	-1.27	88.	
54 192 4.50 7.16 9.87 12.55 15.26 48 -3.85 -4.37 60 3.27 5.97 8.65 11.41 14.10 16.62 .69 -2.56 -3.44 54 2.24 5.04 7.28 9.57 11.85 14.18 .63 -1.52 -1.96 12 2.24 4.54 6.83 9.15 11.45 13.77 05 -2.56 -3.12 12 2.24 4.54 6.83 9.15 11.45 13.77 05 -2.56 -3.12 12 2.24 4.54 6.83 9.15 11.45 13.77 05 -2.56 -3.12 12 2.24 6.20 6.20 8.25 10.74 13.10 15.47 1.32 -1.28 -1.74 25 5.45 10.07 14.82 19.10 24.57 29.10 .93 -4.21 -5.24 -6.27 26 5.81 10.07 14.82 19.10 24.57 29.10 .93 -4.26 -5.60 27 8.15 14.15 20.43 23.27 40.03 2.44 -3.56 -4.75 28 6.20 17.11 17.33 23.01 24.57 26.57 24.71 -5.57 26 6.20 17.11 17.33 23.01 24.57 26.77 24.57 27 8.15 11.02 15.01 20.05 25.04 30.18 .32 -4.75 28 6.30 11.43 16.55 20.07 25.45 30.38 1.55 -3.12 -4.35 29 12.29 17.52 22.55 28.16 33.27 20.1 25.55 -3.15 20 1.30 12.29 17.52 22.55 23.57 20.1 25.53 -3.55 20 12.29 17.52 22.55 28.16 33.57 20.1 25.55 -3.15 20 22.51 23.61 23.67 23.67 20.1 25.55 -3.15 20 22.51 23.61 26.75 25.75 20.1 25.55 -3.15 20 22.51 22.51 22.51 22.51 22.51 22.51 22.51 20 22.51 22.52 22.51 22.51 22.51 22.51 22.51 20 22.51 22.51 22.51 22.51 22.51 22.51 22.51 20 22.51 2	54 1.92 4.50 7.16 9.87 12.55 15.26 46 -3.85 -4.37 69 3.27 5.97 8.65 11.41 14.10 16.52 .69 -2.36 -3.44 54 2.78 5.04 7.25 9.57 11.85 14.18 .63 -1.52 -1.96 12 2.22 4.54 6.83 9.15 11.85 14.18 .63 -1.12 12 2.22 4.54 6.83 9.15 11.45 13.7 05 -2.36 -3.12 12 2.22 4.54 6.83 9.15 11.45 13.7 05 -2.36 -3.12 13 3.45 10.76 15.74 20.84 2.515 2.910 .93 -4.21 -5.31 25 6.25 12.18 17.84 2.52 2.45 2.910 .93 -4.20 -5.60 25 6.25 12.18 17.84 23.64 23.25 .91 -5.24 -6.27 25 6.05 11.03 15.61 20.67 24.57 .65 -4.45 -5.57 25 6.05 17.11 17.35 23.01 28.64 34.31 .41 -5.44 -5.45 26 6.20 17.11 17.35 23.01 28.64 34.31 .41 -5.44 -5.45 26 6.20 17.11 17.35 23.01 28.64 34.31 .41 -5.44 -5.45 27 8.16 11.03 15.81 20.67 25.64 30.18 .32 -4.15 27 1.38 6.15 11.03 15.82 20.67 25.64 30.18 .32 -4.15 27 1.39 6.30 11.43 16.55 21.77 26.10 32.24 1.51 -2.15 -2.15 27 1.36 6.30 11.45 16.25 21.17 26.10 32.24 21.51 -2.15 -2.15 28 1.39 6.33 11.45 16.25 21.15 26.07 21.8 -2.15 -2.15 -2.15 29 1.36 6.33 11.45 16.25 21.15 26.07 21.8 -2.15 -2.15 -2.15 20 1.30 1.40 1.20 21.15 21.07 21.8 -2.15 -2.15 20 1.30 1.40 1.50 20.07 2	4	1.82	4.19	6.76	9.32	11.92	14.53	17.20	06.1	13	09	9L.1	
.60 3.27 5.97 8.65 11.41 14.10 16.52 .69 -2.56 -3.44 .56 2.78 5.04 7.28 9.57 11.85 14.18 .63 ~1.52 -1.96 .87 3.04 5.29 7.54 9.82 12.10 14.42 .93 -1.12 -1.52 -1.12 </td <td>.60 3.27 5.97 8.65 11.41 14.10 16.62 .69 -2.56 -3.44 .56 2.18 5.04 7.28 9.57 11.85 14.18 .63 -1.52 -1.96 87 3.04 5.29 7.54 9.82 12.10 14.42 .93 -1.12 -1.54 -1.96 -12 2.22 4.54 6.83 9.15 11.45 13.71 -0.5 -2.65 -3.12 1.25 3.45 10.17 14.85 19.58 24.29 29.10 .93 -4.15 -1.14 1.00 5.81 10.17 14.55 20.74 20.15 24.29 29.10 .93 -4.26 -1.13 1.00 5.81 10.07 15.14 20.84 25.15 31.18 1.07 -3.46 -4.26 1.00 5.81 10.07 14.82 19.70 24.58 24.24 25.15 .44 -3.56 -4.26 2.21<td>2</td><td>54</td><td>1.92</td><td>4.50</td><td>7.16</td><td>9.87</td><td>12:55</td><td>15.26</td><td>48</td><td>-3.85</td><td>-4.37</td><td> 93</td><td></td></td>	.60 3.27 5.97 8.65 11.41 14.10 16.62 .69 -2.56 -3.44 .56 2.18 5.04 7.28 9.57 11.85 14.18 .63 -1.52 -1.96 87 3.04 5.29 7.54 9.82 12.10 14.42 .93 -1.12 -1.54 -1.96 -12 2.22 4.54 6.83 9.15 11.45 13.71 -0.5 -2.65 -3.12 1.25 3.45 10.17 14.85 19.58 24.29 29.10 .93 -4.15 -1.14 1.00 5.81 10.17 14.55 20.74 20.15 24.29 29.10 .93 -4.26 -1.13 1.00 5.81 10.07 15.14 20.84 25.15 31.18 1.07 -3.46 -4.26 1.00 5.81 10.07 14.82 19.70 24.58 24.24 25.15 .44 -3.56 -4.26 2.21 <td>2</td> <td>54</td> <td>1.92</td> <td>4.50</td> <td>7.16</td> <td>9.87</td> <td>12:55</td> <td>15.26</td> <td>48</td> <td>-3.85</td> <td>-4.37</td> <td> 93</td> <td></td>	2	54	1.92	4.50	7.16	9.87	12:55	15.26	48	-3.85	-4.37	93	
.56 2.78 5.04 7.57 11.85 14.18 .63 ~1.52 -1.96 .87 3.04 5.29 7.54 9.82 12.10 14.42 .93 -1.12 -1.52 -1.54 12 2.22 4.54 6.83 9.15 11.45 13.10 15.47 -0.55 -2.65 -3.12 1.25 3.60 6.00 8.65 10.74 13.10 15.47 1.32 -1.28 -1.74 .65 5.45 10.14 20.84 25.19 29.10 .93 -4.26 -4.26 .100 5.81 10.76 15.74 20.84 25.19 31.18 1.07 -3.46 -4.26 .37 5.11 11.03 16.28 21.59 26.27 32.25 .51 -5.24 -6.27 .37 6.55 12.18 23.24 24.53 24.55 -5.54 -6.27 .38 6.05 10.07 15.01 20.05 25.64 34.33 41 -5.54 -6.27 .39 6.10 10.0	.56 2.78 5.04 7.28 9.57 11.85 14.18 .63 ~1.52 ~1.96 .87 3.04 5.29 7.54 9.82 12.10 14.42 .93 ~1.52 ~1.54	0	09.	3.27	5.97	8.65	14.11	14.10	16.82	69.	-2.86	-3.44	.36	
.87 3.04 5.29 754 9.82 12.10 14.42 .93 -1.54 <td>.87 3.04 5.29 7.84 9.82 12.10 14.42 .93 -1.54 -1.54 -1.54 -1.54 -1.54 -1.53 -1.54 -1.54 -1.54 -1.52 -1.54 -1.54 -1.53 -1.54 -1.54 -1.53 -1.76 -3.12 -1.54 -1.54 -1.54 -2.12<!--</td--><td>7</td><td>.56</td><td>2.78</td><td>5.04</td><td>7.28</td><td>9.57</td><td>11.85</td><td>14,18</td><td>.63</td><td>-1.52</td><td>96.1-</td><td>. 58</td><td></td></td>	.87 3.04 5.29 7.84 9.82 12.10 14.42 .93 -1.54 -1.54 -1.54 -1.54 -1.54 -1.53 -1.54 -1.54 -1.54 -1.52 -1.54 -1.54 -1.53 -1.54 -1.54 -1.53 -1.76 -3.12 -1.54 -1.54 -1.54 -2.12 </td <td>7</td> <td>.56</td> <td>2.78</td> <td>5.04</td> <td>7.28</td> <td>9.57</td> <td>11.85</td> <td>14,18</td> <td>.63</td> <td>-1.52</td> <td>96.1-</td> <td>. 58</td> <td></td>	7	.56	2.78	5.04	7.28	9.57	11.85	14,18	.63	-1.52	96.1-	. 58	
12 2.22 4.54 683 9.15 11.45 13.7405 -2.65 -3.12 1.25 3.60 6.00 8.25 10.74 13.10 15.41 1.32 -1.28 -1.74 1.00 5.81 10.76 15.74 20.84 25.75 29.10 .93 -4.21 -5.21 1.00 5.81 10.76 15.74 20.84 25.75 31.18 1.07 -3.46 -4.26 1.00 2.81 10.03 16.28 21.59 26.87 32.25 .51 -5.24 -6.27 1.00 -5.60 1.00 24.58 29.57 .65 -4.60 -5.60 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1	12 2.22 4.54 683 9.15 11.45 13.7405 -24.68 -3.12 1.25 3.60 6.00 8.35 10.74 13.10 15.41 1.32 -1.28 -1.74 1.00 5.81 10.76 15.74 26.39 29.1093 -4.21 -5.31 1.00 5.81 10.76 15.74 26.39 29.1093 -4.21 -5.31 1.00 5.81 10.05 16.28 24.29 29.1093 -4.21 -5.21 1.00 1.00 5.81 10.05 16.28 24.29 29.1093 -4.26 -4.26 1.00 1.00 14.82 19.70 24.58 29.57 1.07 -3.46 -4.26 1.00 1.00 14.82 19.70 24.58 29.57 1.07 -5.24 -6.27 1.05 12.8 12.8 12.8 12.8 12.8 12.8 12.8 12.8	000	18.	3.04	5.29	754	9.82	12.10	14.42	.93	21.1-	-1.54	48.	
1.25 3.60 6.00 8.65 10.14 13.10 15.41 -1.78 -1.74 .65 5.45 10.16 14.85 19.58 24.29 29.10 .93 -4.21 -5.31 1.00 5.81 10.76 15.74 20.84 25.95 31.18 1.07 -3.46 -4.26 .37 5.11 16.28 21.59 26.37 32.25 .51 -5.24 -6.27 .44 5.22 10.04 14.82 19.70 24.58 29.57 .65 -4.60 -5.60 2.21 8.15 16.15 20.43 26.37 36.37 .16 -5.54 -6.27 .85 6.05 17.18 23.64 36.43 36.13 .41 -5.54 -6.55 .13 6.05 16.01 20.05 25.04 30.18 .35.4 30.18 .35.4 -3.54 -4.56 .13 6.30 10.07 15.01 26.05 25.04 30.18 .35.24 13.51 -3.54 -3.56 .13 6.30	1.25 3.60 6.00 8.35 10.74 13.10 15.45 1.32 -1.28 -1.74 .65 5.45 10.19 14.85 19.58 24.29 29.10 .93 -4.21 -5.31 1.00 5.81 10.76 15.74 20.84 25.95 31.18 1.07 -3.46 -4.26 .37 5.11 11.03 16.28 21.59 26.87 32.25 .51 -5.24 -6.27 .44 5.22 10.04 14.82 10.70 24.58 29.57 .65 -4.26 -5.60 2.21 8.15 14.15 20.43 26.92 33.33 40.03 2.44 -5.54 -6.27 .75 6.05 17.11 17.33 23.04 23.64 34.33 .41 -5.54 -6.57 .13 6.05 11.03 15.82 20.05 25.04 30.18 .35 -3.54 -3.54 .136 6.13 11.43	0	12	2.22	4.54	6.83	9.15	11.45	13.73		- 2:65	-3.12	07	
.65 5.45 10.19 14.85 19.58 24.29 29.10 .93 -4.21 -5.31 1.00 5.81 10.76 15.74 20.84 25.95 31.15 1.07 -3.46 -4.26 .37 5.71 11.03 16.28 21.59 26.87 32.25 .51 -5.24 -6.27 .44 5.22 10.04 14.82 19.70 24.58 29.57 .65 -4.60 -5.60 2.21 8.15 14.15 20.43 26.72 32.25 .51 -6.27 -6.27 2.21 8.15 14.15 20.43 23.64 23.43 34.45 -3.56 -4.75 .25 6.05 17.11 17.33 23.04 23.64 23.43 .41 -5.54 -6.52 .13 5.09 10.07 15.01 20.05 25.04 30.38 1.55 -3.2 -4.85 .1.36 6.30 11.43 16.55 21.77 26.05 30.38 1.55 -3.2 -4.85 .1.36 1.2.29	.65 5.45 10.19 14.75 19.58 24.29 29.10 .93 -4.21 -5.31 1.00 5.81 10.76 15.74 20.84 25.95 31.18 1.07 -3.46 -4.26 .37 5.71 11.03 16.28 21.59 26.87 32.25 .51 -5.24 -6.27 .44 5.22 10.04 14.82 19.70 24.58 29.57 .65 -4.60 -5.60 2.21 8.15 14.15 20.43 26.92 33.37 40.03 2.44 -3.56 -4.75 .96 6.55 12.18 17.33 23.64 23.43 40.03 2.44 -3.56 -4.75 .13 6.55 12.18 17.33 23.64 23.43 40.03 2.44 -3.56 -4.75 .13 6.05 11.71 13.33 23.57 11.6 -4.50 -5.50 .13 6.15 11.03 15.81 20.05 <t< td=""><td>0</td><td>1.25</td><td>3.60</td><td>8.9</td><td>8.35</td><td>4L.01</td><td>13.10</td><td>(5.4.)</td><td>1.32</td><td>-1.28</td><td>+1.14</td><td>1.24</td><td></td></t<>	0	1.25	3.60	8.9	8.35	4L.01	13.10	(5.4.)	1.32	-1.28	+1.14	1.24	
1.00 5.81 10.76 15.74 20.84 25.95 31.18 1.07 -3.46 -4.26 -4.26 -3.75 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	1.00 5.81 10.76 15.74 20.84 25.95 31.18 1.07 -3.46 -4.26 -4.26 -3.7 5.1 5.1 1.03 16.28 21.59 26.87 32.25 5.1 1.05 1.05 14.82 19.70 24.58 29.57 65 -4.60 -5.60 2.21 8.15 14.15 20.43 26.92 33.37 40.03 2.44 -3.56 -4.75 2.60 2.22 6.00 11.71 17.33 23.01 28.64 34.31 41 -5.64 -6.02 1.33 6.15 11.03 15.81 20.67 25.04 30.18 .32 -4.11 -5.64 -6.02 1.38 6.30 11.43 16.55 21.77 26.39 32.24 1.51 -2.65 -4.38 1.36 6.30 11.43 16.55 22.65 32.37 1.01 1.21 -2.65 1.22 1.22 11.22 12.29 17.52 22.65 31.04 2.18 2.03 1.25 -3.55 1.35 1.35 1.35 1.35 1.35 1.35 1.35	=	89.	5.45	10.13	14.85	19.58	24.29	29.10	.93	-4.21	-5.31	.67	
2.21 8.15 14.18 20.43 26.37 32.25 .51 -5.24 -6.27 3.21 8.15 14.18 20.43 26.32 33.33 40.03 2.44 -3.56 -4.56 -5.59 9.5 6.55 12.18 17.18 23.64 23.64 34.31 41.6 -4.56 -5.59 17.18 23.64 23.64 34.31 41 -5.54 -6.52 17.18 17.33 23.01 28.64 34.31 41 -5.54 -6.52 17.33 6.15 11.03 15.82 20.67 25.64 30.18 .32 -4.71 -5.77 17.18 1.38 6.30 17.43 16.55 22.67 32.24 1.51 -2.55 -4.38 17.5 17.5 22.7 20.7 25.75 22.7 20.7 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 20.75 25.75 25.75 20.75 25.75		12	1.00	5.81	10.76	15.74	20.84	25 35	31.18	1.07		-4.26	90.1	
.37 5.22 10.03 16.28 21.59 26.87 32.25 .51 -5.24 -6.27 .44 5.22 10.04 14.82 19.10 24.58 29.57 .65 -4.60 -5.24 2.21 8.15 14.15 20.43 26.92 33.37 40.03 2.44 -3.56 -4.75 .25 6.55 12.18 17.84 23.64 23.43 34.37 11.6 -4.56 -5.59 .13 5.09 10.07 15.01 20.05 25.04 30.18 .32 -4.15 -5.54 -6.50 1.38 6.30 11.03 15.82 20.67 25.04 30.38 1.55 -3.54 -4.38 1.38 6.30 11.43 16.55 21.77 26.06 25.04 30.38 1.55 -3.55 -4.38 1.39 6.30 11.43 16.55 21.77 26.06 25.04 30.38 1.55 -3.55 -4.38 1.39 6.30 11.43 16.55 22.85 22.85 22.74 22.74<	.37 5.2 11.03 16.28 21.59 26.87 32.25 .51 -5.24 -6.27 .44 5.22 10.04 14.82 19.10 24.58 29.57 .65 -4.60 -5.60 .221 8.15 14.15 20.43 26.92 33.37 40.03 2.44 -3.56 -4.75 .25 6.55 12.18 17.84 23.64 29.43 35.37 1.16 -4.56 -5.59 .13 5.09 10.07 15.01 20.05 25.04 30.18 .32 -4.1 -5.50 1.30 6.15 11.03 15.82 20.67 25.48 30.18 .35 -3.54 -4.35 1.30 6.30 11.43 16.55 21.17 26.30 32.24 1.51 -2.52 -3.54 1.36 5.62 20.75 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.16 38.1	13	1	1			1							
44 5.22 10.04 14.82 19.10 24.58 29.57 .65 -4.60 -5.60 2.21 8.15 14.15 20.43 26.32 33.37 40.03 2.44 -3.56 -4.75 .26 6.55 12.18 17.84 23.64 29.43 2.44 -3.56 -4.75 .25 6.00 17.11 17.33 23.64 29.43 .41 -5.54 -6.59 .13 5.09 10.07 15.01 20.05 25.04 30.18 .32 -4.11 -5.54 -6.59 1.36 6.30 11.03 15.82 20.67 25.48 30.38 1.55 -3.2 -4.85 1.36 6.30 11.43 16.55 21.77 26.39 32.24 1.51 -3.55 -4.35 1.36 7.02 12.29 17.52 22.85 23.57 2.01 25.8 -3.13	.44 5.22 10.04 14.82 19.10 24.58 29.57 .65 -4.60 -5.60 .96 6.55 12.18 17.84 23.64 29.43 35.37 1.16 -4.56 -6.59 .25 6.00 11.11 17.33 23.64 29.43 35.37 1.16 -4.56 -5.59 .13 5.09 10.07 15.01 20.05 25.04 30.18 .32 -4.75 -5.77 1.36 6.30 11.43 16.55 21.77 26.79 32.24 1.51 -3.56 -4.38 1.96 7.02 12.29 17.52 22.85 28.16 33.57 2.07 2.58 -3.54 1.96 6.63 11.45 16.25 21.15 26.04 31.64 2.18 2.13 2.53 1.96 6.63 11.45 16.25 21.15 26.04 31.64 2.18 2.13 2.53	4	.37	11.5	11.03	16.28	21.59	26 37	32.25	.51	5	-6.27	.43	
2.21 8.15 14.15 20.43 26.92 33.37 40.03 2.44 -3.56 -4.75 36 6.55 12.18 17.84 23.64 25.43 35.37 1.16 -4.50 -5.59 2.2 6.00 11.71 17.33 23.01 28.64 34.37 .41 -5.64 -6.65 2.13 5.09 10.07 15.01 20.05 25.04 30.19 .32 -4.11 -5.77 2.13 6.15 11.03 15.82 20.67 25.45 30.38 1.55 -3.41 -5.15 2.36 6.30 11.43 16.55 21.77 26.10 32.24 1.51 -3.15 -4.38 2.19	2.21 8,15 14.15 20.43 26.92 33.37 40.03 2.44 -3.56 -4.75 36 6.55 12.18 17.84 23.64 29.43 35.37 1.16 -4.50 -5.59 2.2 6.00 11.71 17.33 23.01 28.64 34.31 .41 -5.54 -6.6.0 2.13 6.15 11.03 15.81 20.67 25.04 30.18 .32 -4.11 -5.54 -6.6.0 2.136 6.30 11.43 16.55 21.77 26.79 32.24 1.51 -3.45 -4.38 2.96 6.63 11.45 16.25 22.85 28.16 33.57 2.01 22.88 -3.79 2.96 6.63 11.45 16.25 21.15 26.04 31.04 2.18 -2.53 -3.54	(5	44.	5.22	10.04	14.82	19.70	24.58	29.57	.65	-4.60	-5.60	.47	
.15 6.05 12.18 17.34 23.64 29.43 35.37 1.16 -4.50 -5.59 1.1 .25 6.00 11.71 17.33 23.01 28.64 34.31 .41 -5.54 -6.65 1.1 .13 6.00 11.03 15.82 20.67 25.04 30.18 .32 -4.81 -5.77 -1.16 .133 6.30 11.43 16.55 21.77 26.50 32.24 1.51 -3.55 -4.38 1.1 .136 6.30 11.43 16.55 21.77 26.50 32.24 1.51 -3.55 -4.38 1.1 .195 7.02 12.29 17.52 22.85 28.16 33.57 2.01 25.8 -3.79 1.5	.15 6.05 12.18 17.3 23.64 29.43 35.37 1.16 -4.50 -5.59 1.1 .13 6.00 11.71 17.3 23.01 28.64 34.37 .41 -5.54 -6.65 .13 6.30 11.43 16.55 21.77 26.76 30.38 1.55 -3.22 -4.58 1.3	9	2.21	8.15	14.15	20.43	26.92	33.33	40.03	2.44	-3.56	-4.75	2.33	
133 6.15 11.03 23.01 28.64 34.31 .41 -5.54 -6.65	.13 6.00 11.11 17.33 23.01 28.64 34.31 .41 -5.64 -6.65	17	96.	6.55	12.18	17.84	23.64	29.43	35.37	1.16	-4.50	- 5.59	1.08	
1.33 6.30 10.07 15.01 20.05 25.04 30.18 .32 -4×1 -5.77 . 1.36 6.30 11.43 16.55 21.77 26.30 32.24 1.51 -3.35 -4.38 1. 1.36 7.02 12.29 17.52 22.85 28.16 33.57 2.01 22.58 -3.75 1. 1.95 7.02 12.29 17.52 22.85 28.16 33.57 2.01 22.58 -3.75 1.	1.33 6.15 11.03 15.82 20.67 25.04 30.18 .32 -4.81 -5.77	8	.25	6.00	11.71	17.33	23.01	28.64	34.31	14.	-5.54	10.0	٠ عرد	
1.38 6.15 11.03 15.82 20.67 25.4% 30.38 1.55 -3.44.85 1.36 6.30 11.43 16.55 21.7 26.7 32.24 1.51 -3.55 -4.38 1.	1.38 6.15 11.03 15.82 20.67 25.4% 30.38 1.55 -3.44 -4.85 1.38 1.38 6.30 11.43 16.55 21.77 26.79 32.24 1.51 -3.75 -4.38 1. 95 1.02 12.29 17.52 22.85 28.16 33.57 2.01 -2.58 -3.79 1. 1.96 6.63 11.45 16.25 21.15 26.04 31.64 2.18 2.18 -2.59 -3.54 1. Buckling Restrainers Installed	6	.13	5.09	10.01	15.01	40.05	25.04	30.19	.32	124-	15.77	.2%	
1.36 6.30 11.43 16.55 21.77 26.76 32.24 1.51 -3.55 -4.38 1. 	1.36 6.30 11.43 1655 21.77 26.30 32.24 1.51 -3.55 -4.38 1. 1.95 7.02 12.29 17.52 22.85 28.16 33.57 2.07 2.58 -3.79 1. 1.96 6.63 11.45 16.25 21.15 26.04 31.04 2.18 2.18 -3.54 .3.54 1.	20	1.33	6.15	11.03	15.82	20.67	25.48	30.38	1.55	W.	-4.85		
1.95 7.02 12.29 17.52 22.85 28.16 33.57 2.07 2.58 -3.79 1.		21	1.38	6.30	11.43	16.55	71.12	26.00	32.24	1.51	II.	-4.38	1.33	
1.95 1.02 12.29 17.52 22.95 58.16 33.57 2.07 25.58 -3.79 1.	1.96 6.63 11.45 16.25 20.85 28.16 33.57 2.07 2.58 -3.79 1.00 1.96 6.63 11.45 16.25 21.15 26.04 31.04 2.18 -2.59 -3.54 1.00 Buckling Restrainers Installed	22)	1		1	1	1		-	4 7.50	76.60	1	
100 000 11 46 10 26 01 16 20 00 31 00 18 10 13 13 00	1.96 6.63 11.45 16.25 21.15 26.04 31.04 2.18 -2.54 -3.54 Buckling Restrainers Installed	23	1.95	7.03	12.29	17.52	22.85	28.16	33.57	2.07	85.2-	-3.73	1.88	
0.63	CONTROLL COUNTY AND AND THE PROPERTY OF THE STATE OF THE	24	1.96	6.63	11.45		21.15	26.04	31.04	2.18	-7.53	3	(8.	

Table 45. Strain Gage Results at 631 Flights - AFCG-4 (Continued)

STRAIN	TEST	TEST CONDITION:		STRESS (KSI)		COMPLETE	AT APPLIED AXIAL LOAD (KIPS)	(KIPS)			
NO.	ØB.	0)	20	30	40	50	60	ØR.	-10	-12	ØB1
25	34	11.4	9.94	15.17	20.55	25.93	31.42	13	-5.77	-6.81	40
26	.26	5.77	11.48	17.18	23.04	28.86	34.78	.45	-5.50	-6.54	81.
27	1.92	7.48	13.27	19.13	25.18	31.21	37.56	2.13	-3.74	-4.74	1.86
28	1	1	1	1		1)		-	
								A Marie			
											1000
											T WILL ST
				0.		386	N.				
								100			
		SHEETERS				Speke E Elli					
		-									

Table 46. Strain Gage Results at 670 Flights - AFCG-4

	Ū	FILGHT	2027	1 .077	1				
MEASURED	STRES	S (KSI)	AT APP	PLIED AXIV	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	(KIPS	_		
	20	30	40	50	09	ØB.T.	0/-	-12	ØB.
2.92 5.	5.43	7.93	10.48	13.01	15.58	\$.	-1.73	12.2-	.48
3,73 6.	6.27	8.84	11.47	14.09	16.73	1.32	-1.06	-1.56	1.23
3.40 5.	5.87	8.40	1.04	13.67	16.34	1.19	66	-1.12	1.00
4.43 6.	6.9	9.56	12.18	14.80	17.45	2.12	.15	36	1.98
2.14 4.69	69	7.35	10.06	12.74	15.44	30	-3.59	-4.15	73
3.42 6.09	60	8.8	11.54	14.24	16.95	.80	-2.69	-3.31	.48
2.87 5.12	N	7.36	976	11.94	14.26	.67	-1.42	-1.88	.64
3.16 5.40	2	7.64	9.93	12.21	14.51	1.02	96	-1.41	.94
2.39 4.70	0	66.9	9.32	11.62	13.95	8.	-2.46	-2.96	70.
3.75 6.14	4	8.49	10.88	13.24	15.62	1.45	-1.09	-1.57	1.37
5.47 10.21	-	14.87	19.60	24.34	29.10	.85	-4.16	-5.33	.64
5.77 10.71	-	15.68	20.78	25.89	31.08	.98	- 3.43	1-4.27	1.01
1	1	1					1		1
5.63 10.94	4	16.18	21.50	26.79	32.13	35.	-5.27	-6.36	28.
5.29 10.10	0	14.89	19.78	24.67	29.62	79.	-4.51	-5.57	.48
8.07 14.09	0	20.43	56.92	33.52	40.17	2.23	-3.65	-4.92	61.2
6.70 12.31	-	17.97	23.79	19.62	35.54	1.20	-4.32	-5.47	1.18
6.04 11.73	m	17.34	23.03	28.67	34.39	.34	-5.45	-6.63	.36
5.25 10.22	2	15.16	20.20	22.52	30.33	.37	4.5	-5.64	.32
6.21 11.06	9	15.85	50.69	25.50	30.36	1.53	-3.70	-4.80	1.27
6.42 11.52	2	16.62	18.12	27.03	32.28	1.57	-3.34	-4.23	4.
1		1	1	1	1		1		
7.12 12.35	35	17.57	22.90	28.20	33.58	2.11	-2.70	-3.66	1.92
1 15 11 45	1	11 30	7	00 10	20.00		2 -	1	100

Table 46. Strain Gage Results at 670 Flights - AFCG-4 (Continued)

8.1.

H.F. HANGING FREE

GAGE		MEASURED		S (KSI)	AT APPLI	W	D AXIAL LOA	O (KIPS		0 1 to 10	0 8	
	ØB.	0)	20	30	40	50	60	ØB.	-10	-12	ØBT.	
25	16	4.83	10.03	15.27	20.66	26.05		11		-6.72	34	
26	.40	5.84	=	17.23	23,11	28.96	34.85	.43	-5.36	-6.44	2.	
27	1	1	1	1	1	1	82.89	25.30	26.39	12.75	43.22	
28	1	1	1		1	1		1	1	1	1	
9	la V				=			- 12 18	14 15 16		art Af	
	35								Est On		49	
T	20								100	100 PM	0.8	
		ES I		in.			\$10 Mark		901/4	1	150 AT	
	190	65				81		8	70 TO 15 TO 15	10	iav G	
		NA PA						10				
		N. S.					8			100		
3					C-2011				8.00	70.8	689	
											28.7	
			8.4					2011		100 200 1		
	DON								10 P 20 P		30	
		100					100	15.65	2001	100	388	
											200	
100			938					3.6	5			
		107 11 15 18 18 18 18 18 18 18 18 18 18 18 18 18										

Table 47. Strain Gage Results at 802 Flights - AFCG-4 HANGING FREE B.I. BOLTED IN H.F.

CTDATE	TEST	TEST CONDITION	LIGH!	100 110	П	いってとしている	11				
GAGE		MEASUREI	STRESS	S (KSI)	AT APPL	IED AX	AT APPLIED AXIAL LOAD (KIPS)	(KIPS	0		
110.	ØR.	01	20	30	40	50	90	ØBI.	01-	-12	ØBI
_	.51	26.2	5.41	7.95	10.49	13.03	15.58	4.	-1.72	12.2-	4.
7	1.34	3.75	62.9	890	11.53	14.18	16.81	1.32	-1.05	-1.56	1.24
3	1.06	3.28	5.68	8.22	10.80	13.40	16.01	1.05	76	-1.22	.88
4	60.2	4.39	68.9	9.44	12.00	14.57	17.16	5.09	91.	35	1.95
2	48	1.93	4.47	7.14	61.6	12.43	5051	4	-3.77	-4.32	86
O	1.0%	3.66	1.31	20%	69.11	14.34	16.91	1.08	-2.42	-3.04	.78
7	89.	78.2	5.09	7.35	6.63	11.91	/4.20	89.	-1.38	-1.85	.65
œ	.97	309	531	7.57	9.84	12.11	14.39	.96	-1.02	-1.45	.88
6	90.	2.34	4.63	76.9	9.24	11.55	13.84	.06	-2:49	-2.98	.05
0	1.45	3.75	6.10	8.47	10.84	13.20	15.54	1.44	-1.09	-1.57	1.38
	.88	5.54	10.21	14.90	19.57	24.28	28.98	66.	-3.92	-5.10	.80
2	1.06	5.73	10,59	15.59	20.63	25.71	30.80	.97	-3.36	-4.19	1.03
3			1		1				1		1
4	44.	5.63	10.86	16.13	21.38	26.64	31.89	14.	21.5-	12.9-	-42
5	.58	5.25	10.00	14.80	19.63	24.49	28.33	.65	-4.42	-5.49	.53
v	.64	6.61	12.75	19.46	26.16	32.83	39.52	79.	-5.43	-6.78	29.
7	1.48	7.00	27.21	18.44	24.35	30.30	36.28	1.48	-4.11	-5.31	1.48
8	.54	02.9	11.86	17.58	23.29	28.99	28.99 34.69	.49	-5.32	-6.51	.53
6	15.	5.42	10.38	15.43	20.49	25.58	30.69	.55	-4.45	-5.47	.51
20	1.59	6.27	11.04	15.85	20.63	15'52	3019	1.63	-355	-4.64	1.39
21	1.60	6.38	11.40	16.53	21.67	28.72	31.98	1.55	- 3.31	-4.19	1.42
22					1						1
23	21.2	7.04	12.19	17.43	52.69	27.97	33.25	5.05	75.2-	-3.62	1.90
7 7 0	11.0	0//	11 12		70.0		-	-	-	-	

* With Buckling Restrainers Installed

Table 47. Strain Gage Results at 802 Flights - AFCG-4 (Continued) HANGING FREE B.1. BOLTED IN H.F.

STRAIN	1	MEASURED		TRESS (KS1)	I) AT APPL	PLIED AXIA	STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	(KIPS)		
.02	OBI	0)	20	30	40	50	60	Ø8.₹	01-	-12	Øbr.
25	10.	4.99	10.16	15.50	26.02		31.83	10-	-5.56	67.7-	02
26	89.	6.08	11.73	17.58	15.55	K 14 - 11	35.40	·64	-5.08	41.9-	4.
27		1	1	1	1	J	1		1	1	1
28		1	1	1		1				1	1
						34		us -	10	ik Pi	
										a land	
T											
	- 12.00										
						32.83					
			100				12.12	38.4			
		9			5.8.5		50.07				
		100									100
							18.8				
						記録を大き上					
					A STATE OF	302.00					
							19/3				
	7887		L-	9							
			1								

Table 48. Strain Gage Results at 876 Flights - AFCG-4 HANGING FREE B.I. BOLTED IN H.F.

STRAIN	TEST (TEST CONDITION MEASURED		STRESS (KSI)	AT APPI	COMPLETE	876 COMPLETE AT APPLIED AXIAL LOAD (KIPS)	(KIPS)			
10.	#UD	07	20	30	40	50	90	ØBI	01-	-12	ØB.
-	.53	2.97	5.46	8.00	10.54	13.08	15.64	,55	-1.69	-2.16	.52
7	141	3.83	6.38	10.6	11.66	14.30	16.96	1.42	99	- 1.47	1.32
2	1.12	3.32	5.72	8.24	10.81	13.39	15.99	1.14	67	11.1-	96.
4	2.11	4.39	6.87	9.41	11.97	14.52	11.71	2.13	.20	28	1.97
S	33	2.03	4.53	7.19	9.83	12.45	15.07	34	- 3.59	-4-11	P
9	1.28	3.88	6.50	9.19	11.84	14.46	01.71	1.30	-2.14	-2.72	1.06
7	11.	2,89	5.12	7.39	9.66	+6:11	14.24	27.	- 1.36	-1.80	89.
œ	1.04	3.16	5.38	7.64	16.6	12.18	14.47	1.04	46	-1.36	96.
0	.13	2.41	4.69	7.00	9.30	11.59	(3.89	41.	-2.40	-2.87	.13
0	1.51	3.81	6.15	8.52	88.01	13.22	15.58	1.53	-1.00	-1.46	1.46
=	.87	5.53	10.19	14.86	19.54	24.22	28.95	86.	-3.97	-5.06	TT.
7	1.09	5.78	10.64	15.63	19.02	25.73	30.87	1.06	-3.33	-4.13	1.06
13))			<i></i>	1		1			1
4	.46	5.66	10.88	16.13	21.38	26.61	31.89	.48	-5.10	-6.13	.42
15	.59	5.26	86.6	14.78	19.60	24.44	29.34	.67	-4.41	-5.41	,53
9	-1.72	4.41	10.75	17.59	24.27	30.82	37.43	-1.67	-8.06	-9.39	-1.78
-	1.13	7.31	12.95	18.80	24.78	30.78	36.87	1.78	-3.94	-5.11	27.1
8	49.	6.32	11.99	17.71	23.44	29.14	34.89	.64	-5.23	-6.38	.63
6	151	5,49	10.45	15.49	20.58	25.66	30.82	.63	-4.39	- 5.35	.55
20	1.58	6.25	11.01	16.80	20.58	25.33	30.14	1.65	-3.53	-4.55	1.41
21	1.68	6.45	11.46	16.58	17.12	26.84	32.02	1.68	-3.19	-4.03	1.53
22			1				1	-		1	1
23	2.19	7.11	12.26	17.51	22.76	28.01	33.33	2.18	-2.59	-3.50	2.01
24	216	177	45				,				

* With Buckling Restrainers Installed

Table 48. Strain Gage Results at 876 Flights - AFCG-4 (Continued)
HANGING FREE B.1. BOLTED IN

H.F.

6.35 12.03 15.64 21.07 26.54 32.08 1.3 -5.51 -6.60 6.35 12.03 17.93 23.88 29.88 35.92 .99 -4.70 -5.69	.02 00	ØBr*	0	20	30	40	0	00	SRT.	01-	-12	ØBT.
6.35 12.03 17.93 23.68 29.88 35.92 .99 -4.70 -5.69	ó	6	5.07	10.27	15.64	21.07	26.54	32.08	.13		-6.60	
	6'	9	6.35	12.03	17.93	23.88	29.88	35.92	66.	-4.70	-5.69	- 1
		-	1	1			1	1	1		1	81.44
		1	J	1	1		1	1	1		1	
			12									
	1	1										
		+										
	1	+									1000	
	0											
		1	0	5								
				0 0			2 0 7 E 3	8.6	5		700	8
	2		200							9 1		6
			3.50 P	1000								10.00
	g I		1.0.1		ð	c)	0.3		0	4 J		
				21.85.23	18008		TEN SEVE	A CHARLE	CARL ST			
			971511108									

Table 49. Strain Gage Results at Start of Test - AFCG-5

8.1.

HANGING FREE

H.F.

					\prod									
	10,13	.124	421.	619.	-268	. 824	-,36/	/98:	421.	615.	250.			
	37.5	9.610	9.610	10609	9.826	13.568	9,620	4.064	8.570	8.940	8.662			
	35	9.002	4.002	9.140	9,126	9,898	126'8	8.499	9,033	8.374	8,076			
STRESS (KSI) AT APPLIED AXIAL LOAD (KIPS)	30	2.725	7.725	8.631	7,766	8.549	7.674	7.323	6.834	7.210	6,932	10 (8)		
ST IAL LOA	25	6.499	6.468	7.292	6.396	7,210	6,345	6.130	5,717	6.077	5.789			
OF TEST	20	5.253	5.253	5,974	5.057	5.412	5.057	5.057	4.584	4,923	4.656			
AT APP	15	3.976	3.776	4.635	2.719	4.594	3.713	3.832	3.471	3.790	3512		100	
AT STARET S (KSI) AT A	10	2,750	2.740	3,296	2.369	3,296	2,390	2,740	2.328	2.740	2,369			
	5	1.504	1.473	1.978	1.030	2.019	1,030	1.576	1.236	1464	1.236		3 10	
TEST CONDITION:	BI'o"	.208	.206	670	530	.762	-, 330	.412	103	.340	280	MULALIN		
TEST	HF"O"	0	0	0	0	0	0	0	0	0	0			
STRAIN		1	7	6	4	n	9	1	80	Ь	0	3000		

Table 50. Strain Gage Results at Start of Test - AFCG-6

8T OF TEST 3O 35 OBT 3O 35 OBT 7.52 8.8004 7.49 8.73 .02 7.49 8.73 .02 7.49 8.73 .02 7.49 8.73 .02 7.49 8.73 .02 7.49 8.73 .02 7.49 8.73 .02 6.91 8.0345 6.43 7.5959	I	H.F.	HANGING FREE	REE	B.I.		BOLTED IN						
0 H.F. O B.I.* 10 20 30 35 087 002 2.43 4.97 7.52 8.8004 010 2.48 5.00 7.49 8.73 .02 0 -1.24 1.63 4.36 7.13 8.51 -1.24 0 021 2.35 4.87 7.42 8.6937 0 0 .66 2.81 5.03 7.23 8.36 .62 0 0 .67 2.81 5.03 7.23 8.36 .62 0 0 .52 2.65 4.78 6.91 8.0345 0 059 1.78 4.09 6.43 7.5959	MIN	TEST	CONDITION			이뉴	IED AX	IAL LOA	O (KIPS				
7.52 8.8004 7.49 8.73 .02 7.13 8.57 - 1.24 7.73 9.04 .00 7.73 9.04 .00 7.23 8.36 .52 6.91 8.0345 6.43 7.5959	-	H.F.	0 B.I.		20	30	35	OBI	01-	-20	-25	-30	ORI
7.49 8.73 .02 7.13 8.57 -1.24 9.13 10.46 1.07 7.73 9.04 .00 7.73 9.04 .00 6.91 8.0345 6.43 7.5959	1		- ,02		4.97	7.52	8.80	04	-2,58	- 11	£+'9-	- 7.67	16
7.13 8.51 -1.24 9.13 10.46 1.07 7.42 8.6937 7.23 9.04 .00 6.91 8.0345 6.43 7.5959	2	0	11	2,48	5.00	2,49	8.73	70.	-2.47	-5,00	-6.25	-7.50	1.08
7.42 8.6937 7.73 9.04 .00 7.23 8.36 .62 6.91 8.0345 6.43 7.5959	1	0	17	1.63	4.36	7.13	8.51	-1.24	-4.02	- 6.91	-7.98	-456	-1.26
7.42 8.6937 7.73 9.04 .00 7.23 8.36 .62 6.91 8.0345 6.43 7.5959	*	0	1.13	3.75	6.45	9,13	10.46	1,07	-1.47	-4.38	-5.73	-7.08	98.
7.73 9.04 .00 7.23 8.36 .62 6.91 8.0345 6.43 7.5959	16	0	21	2.35	4.87	7.45	8.69	37	-2.90	-5.41	-6.63	-7.88	23
6.91 8.0345 6.43 7.5959	19	0	71.	2.63	5.17	7.73	9.04	00.	-2.52	90'5-	-6.28	-7.57	9
6.91 8.0345	1	0	11	2.91	5.03	7,23	8.36	23.	19.1-	-2.74	-4.77	-6.80	.59
6.43 7.5959	00	0	11	1.78	4.18	6.59	7.79	99.	-3.11	-5.62	-6.94	-8.39	78
6.43 7.5959	+	0	.52	2.65	4.78	6.91	80,03		-1.47	-3.77	-4.78	-6.80	5.65
		0	1 7	1.78		6,43	7.59	53	-2.94	-5.36	-6.59	-7.93	99' -
With Buckling Restrainers Installed	ith Buc	ckling	Restrain	ners Ins	talled								

SECTION IV CRACK PROPAGATION DATA

This section contains tabulated results of crack length versus cycles for each specimen tested. The data is reported herein exactly as recorded. Reading errors which are inevitable, particularly with small flaws such as the corner flaws of holes 1 and 2, have not been corrected. The proper use of this data would be to utilize the best fit curve through an expanded plot. This is the procedure utilized in the analysis of this report presented in Volume I.

The crack propagation results are presented in Tables 51 through 62. Plots of the test data are presented in Figures 33 through 44.

Table 51. Crack Propagation Data From Side 1 - AFCG-1

			CRACK	PROPAGAT	ON DATA				
TOTAL		FLAW LENG		-		ONS 1 THR	U 9		
CICEES	0	2	3	•	(3)	6	7	8	9
EDM	luny (mail	intrase	a loutive	ari era r	.1992	.4959	.1819	.4938	.5398
O		- 9							
3000	.0035	4650.	.0579	.0615	.2300	.5184	.3025	.6283	-788 F
3400	80 90U	ifith c	90 6 W	# £3550	AND 18 (0.3)	.5209	.3667	.6453	
3800	WEST AND	erenerion.	note to be	alieN 5	Les holyes	nee ne i	.3906	.6605	.856
4700			.0695	.0693	.2383	.5246		.6748	.883
4800								דרטה	.9268
5400								.7329	.9846
6000	24 73 -			a power and				.7509	1.034
6600		.0311	.1017	0100.	.2555	. 5344	.5690	ארדר.	1.074
7200	an Algipten	2/21/25	upi trafi	estresch.		30,13747	.6064	.8048	1.1230
7600							.6470		1.149
8000		.0336	.1226	1801.	.2654	. 5414	.6634	-8444	1.185
8400							.6935	.8580	1.225
8800							.7148	-8773	1.765
9200							.7504	.8913	1.238
9600							.7790	.9090	1.3269
10000							.8111	.9261	1.3590
10400			.1594	.1345	.2896	. 5443	.8388		1.407
10800		.0355	0505.			. 5550	.8701	.9608	1.438
11200							.9007	.9764	1.475
11600							.9768	.9933	1.5096
12000			/Ala.				.9585	1.0061	1.5368
12400							1186.	1.0251	1.578
12800							1.0044	1.0414	1.6068
13200				.1706	.3166		1.0332	1.0549	1.6400
13600							1.0693	1.0704	1.6778
14000								1.0984	
14400							1.1369	1.1159	1.768
14900							1.1662	1.1340	1.806
15200							61021	1.1516	1.854
15600			.2479	.2056	.3463	.6107	1.2286		
15800							1.2420	1.1792	1.943
16000							1.2564	1.1828	
16600								1.2043	

Table 51. Crack Propagation Data From Side 1 - AFCG-1 (Continued)

			CRACK	PROPAGAT	ION DATA	YSUL			
TOTAL CYCLES		FLAW LENG				ONS 1 THE	U 9		33.5
CICLES T	①	2	3	•	(5)	6	7	8	9
17000			of Itali				1.3261	1.2216	1001
17600			.2802	.2300	.3699	.5645	1.3766	1.2448	
18200							1.4231		
18800							1.4739	1.3123	
19400								1.3358	asi
00005				.2701	.4087		1-5399	1.3706	salah
20600							1.6300	1.3886	
21200							1.6730	1.4228	1000
21800			2.24				1.7155	1.4463	nees
22200			.3246	.3087	.6540	.5712	1.7161	1.4697	
22800			.3745			. 5767	1.8350	1.4973	
23400			- 4080	.3303	.4798	.5802		1.5326	
24000								1.5507	
24600								1.5896	
75800								1.6473	
26400								1.6734	
27000								1.6991	
27600			.5249	4774	.5950	. 5946		1.7397	
Z8400								1.7707	
29000								1.7878	
30000								1.8267	
31000			.6217	.5125	.7223	.6040		1.8840	
32000			.6575	.5453				1.9388	
33000			.6922	.5790	. 8093	.6125			
34000			סרגר.	.6070	.8615				
35000			.1522	.6434					
36000		10621	.7993	.6772	.9780	.6217			
37000						.6241			
42000						.6414			
48000		.0848				.6599			
53000		.0989				.6746			
54800		5701.				.6817			
57200		.1166				.6869			
59600		.1265				.6974			
62400		-1391				.7039			

Table 51. Crack Propagation Data From Side 1 - AFCG-1 (Concluded)

			CRACK	PROPAGATI	ON DATA	X3480	No.		
TOTAL		FLAW LENGT	H (INCHE	S) AT FLA	W LOCAT	IONS 1 THR	19		23.4%
oroccs	0	2	3	•	(5)	6	7	8	9
64600	1.77.1	.1485				סדור.			DOOF
67000	3448	.1630	1.564	910,00		.7240			Codr
68600	100	.1700				.7309			
71000	75181	.1837				7409			CA R A
73200	east.	.1990				.7511			govi e
74800	0000	.2125		Arw. 1		.7551			ocas.
מספרד	1977	.2285				.7628			0.048
78600	8 13 X 1	.2402				.7669			00.5
79600		.2467				.7689			pa é la
80600		.2569	- 73.			.7727			0.005.55
		Bassa III							
									2003
									necas
	100								And a
			Name 1	Legal I		A COLOR			
	ar be								
	1100								
		+ + +							_
		++							
		+		0.2 (0.4)					
		++				+			000
		++				11			
	-	++				+	V 76 ()	-	2.130.0
-+		++							5-17-18-11 I
-		1	9102			1			
		++					£3634.4		
		++	1200				ENERY		and the
		1	MIG 3				500/		008-
		+							COST
			ALC: I						

Table 52. Crack Propagation Data From Side 2 - AFCG-1

			CRACK	PROPAGAT	ON DATA	STATE OF			
TOTAL		FLAW LEN	GTH (INCHE			ONS 1 THR	U 9		
CYCLES	1	(2)	3	(4)	(5)	6	7	8	9
EDM	3 3 G 1	354214			.2058	.4956	.1834	.4940	.539 5
0	#277.U.I	83014	1452, 3	3 80,8	3 8 5 J	8/85			
3000	BETEV.	08978	.0645	.0168	.7315	.5021	.3115	.5460	. 8145
3400	21711	0755					.3343	.5539	
3800	13.01.7	TARS.					.3625	.5668	
4200	2001	44151	.0785	.0885	.2435	.5024	.3790	. 5840	
4800	OUT IN A	ASAE .							.9769
5400	CEET!	03000							1.0330
6000	ises.	2750							1.0825
4400	\$835	58041	.1065	.1176	.2702	. 5080	.5041	.6710	
7200	21881	1036-1					.5400	.6940	1.1911
7600	9018	5,222	asta.	0.4 (25)		Allert Alle	.5588	-7107	1.2285
8000	Sere!	Clode	.1299	.1301	.7845	. 5088	.5877	.7315	1.2639
8400	5 55 64						.6037	.7434	1.7964
8800	53981	FAS: E	8,620,1			1 47 4	.6353		1.3298
9200	31.533	SAME.					.6527	.7760	1.3702
9600		5,200					-6870	.7930	
10 000		543.9					.7075	.8074	1.432
10400		31363	.1684	-1673	.3081	.5227	.7311	.8249	1.4651
10800	25030						.7544	-8423	1.4964
11200	5402						.7722	.8604	1.5291
11600	od .						.8003	.8745	1.5713
12000	0.80						.8182	-8884	1.6036
12400							.8403	.9071	1.6310
12800							.8594	.9237	1.663
13200	31834		.2056	.1995	.3517	.5281	.8839	.9336	1.6968
13600	05571						5010.	.9480	1.7418
14000			03377	erson	38001	0.238.	.9420	.9610	1.7754
14400			31.83				.9669	.9740	1.8189
14800							.9945	.9930	1.8640
15200							1.0187	1.0071	1.9131
15600			.2570	.2335	.3714	.5312	1.0461	1.0199	66,000
15800							1.0645	1.0275	Longy
16000							1.0708	1.0372	CONTRACT
14600			Det.				1.1030	1.0538	100033

Table 52. Crack Propagation Data From Side 2 - AFCG-1 (Continued)

			CRACK	PROPAGAT	ON DATA				
TOTAL CYCLES		FLAW LEN	GTH (INCHE	S) AT FLA	W LOCATI	ONS 1 THR	NU 9		1711
TICLES I	0	2	3	•	⑤	6	7	8	9
17000				Addi			1.1246	1.0690	
17600			.2810	.2525	.4085	.5331	1.1638	1.0944	
18200			100000	2127			1.1950	1.1155	i nine
18800							1.2270	1.1375	
19400		3 5 3 7					1.2847	1.1641	Z mie
20000		4.87	.3332	.2980	.4495	-5376	1.3144	1.1872	
20600								1.2120	ers.
21200							1.4030	1.2337	
21800							1.4356	1.2520	
22200			.4760	.3518	.4988	.5501	1.4683		
22800	6383	OZOS.					1.5161		
23400		9000	.4096	.3629	.5140	.5550	1.5555	1.3148	
24000	2 5 5		46.862	3465	1,041,	.ee.s		1.3332	
Z4600		th Kenah						1.3592	
25200			.4543	.4005	-5651	-5548	1.6947		
75 800		TO REEL					1.7468		
26400							1.7994		
27000							1.8603		
27600			T T T A			1431	2.0275		ace
00485								1.5055	
29000								1.5242	Z.A.
30000		1000						1.5550	
31000								1.5849	
32000								1.6173	
33000								1.6500	
34000	LAR LAT			Li al				1.6874	603
35000	A 23 6							1.7220	
36000	6		.8020	.7002	1.0239	.5850			
37000		Sala S				. 5816			CO.
38000	118000								1018
39000									105
40000	20 Lo 1	all vale							
41000	3 -5 - 1	Z LZA							
41600	erea.	Leaf III							
42000		Lo ZoL				.5994			41.13

Table 52. Crack Propagation Data From Side 2 - AFCG-1 (Concluded)

			CRACK	PROPAGATI	ON DATA				
TOTAL CYCLES		LAW LENG	TH (INCHE	S) AT FLA	W LOCATI	ONS 1 THRU	J 9		
T	①	2	3	4	(5)	6	7	8	9
48000				MATERIAL DE		.6124			
53000						.6220	C 1 (7)	Carre	
54800		32032				Coro			
57200	a so di	DO NE				3413.0		3	0.15
59600						.6421			0.00
62400		1100							
64600	2571	Calle	264			.6573			
67000	1813	1285				.6656			15360
68600		I CORT	V (191			-6689			
71000	Michael		BUCK.			.6742			0.54
74800		119				.6821			000
78600		8327	2.00		BITTE	.6896			
79600	M) FE	0000				.6916			dag
80600	0.000	5138				.6950			0.0
1254	P/B	Physics.							29, 10
1074									500
29.5		Sens V				2466			
(3.03)	0.183	40.403							
	NY PA	PARSA							
1.3197	1.110	15May							1000
te die	arer.								1000
463.	202F	100							
	V Salar	3,300							
337	e centre	SECTION				E CO E I			5,00
1005	0.00	The same of							1001
		Ray							958
sede l									0.113
	5 7 2 9	nije kie i							Date
12,33	hars.	THE STATE OF							
									conc
Ses		7 5 5 3 1		100		10.5			0003
	931								002
									Tares.

Table 53. Crack Propagation Data From Side 1 - AFCG-2

		CRACK PROPAGATION DATA											
TOTAL CYCLES	F	LAW LENGT	H (INCHE	S) AT FLA	W LOCATIO	INS 1 THR	U 9		1316				
CICLES	0	0	3	4	⑤	6	7	.8	9				
EDM					.1974								
0	. 2760	.3/12	.0360	.0355	.2041	.4873	.5487	.4201	.183				
600			.0402	.0411	.2037	.4941	.5626	.4230					
1600			.0446	.04.46		4940	.6006	.4442	.210				
2200			.0456	.0472		4942	.6281	.4711	,220				
2800			.0543	.0553		4950	.6615	.4824	.242				
3400			.0554	.0576		,4957	.6850	4982	.263				
4000			.0594	.0613		4960	.7085	.5145	.278				
4600			.0600	.0581		.4909	.7501	.5286	.2966				
5200			.0651	.0637		.4978	.7832	.5408	.3203				
5800			.0706	.0684		.4984	.8140	.5579	.3415				
6400			.0752	.0719		.4972	.8403	.5738	.361				
7000							.8772	.5904	.384				
7600							.9073	.6092	.4017				
8200							,9449	.6292	.4353				
8800							.9795	.6440	.459				
9400			.0943	.0914		. 4961	1.0058	.6632	.485				
10,000							1.0404	.6840	.508				
10600							1.0719	.6989	1.5404				
11200							1.1121	.7153	.576				
11800							1.1440	.7276	597.				
12400							1.1714	.7524	.632				
13000							1.1980	.7665	.672				
13600			.1303	1230		.4983	1.2250	.7907	.708				
14200							1.2487	.8039	.729				
14800							1.2793	.8194	.7666				
15400							1.3130	.8380	.787				
16000							1.3536	.8509	.84.5				
16600							1.4078	.8708	.868				
17200							1.4354	.8900	.905				
17800			.1604	.1586	.2152	. 5056	1.4687	.9067	.929				
18400								9198	.9674				
19000								.9421	1.002				
19600								9511	1.038				
20000								.9754	1.077				

Table 53. Crack Propagation Data From Side 1 - AFCG-2 (Continued)

	CRACK PROPAGATION DATA											
CYCLES		FLAW LENG	TH (INCHES	The same of the same of		ONS 1 THRU	9		7,07187			
CICCES	0	0	3	①	⑤	6	7	8	9			
20800							1	.9896	1-1095			
21400			.2039	.1875	.2152	.5066		1.0094	1. 1364			
22000						18.3		1.0201	1.1795			
22600						065		1.0401	1.2072			
23200				Van IV	348 -10			1.0521	1.246			
23800					35.0			1.0656	1.2797			
34400					200	80.9		1.0781	1.3244			
25000			.2407	. 2234	171	.5055		1.1019	1.356			
25600			30.5			74		1.1181	1.3964			
26200				AA e				1.1322	1.4467			
26800								1.1492	1.4820			
27400								1.1702	1.5248			
28000				may I				1.1818	1.5754			
28600			.2848	.2595	.2192	.5089		1.2019	1.6222			
29200			Sees Hills					1.2268	1.6609			
29800								1.2399	1.7097			
30400				1000				1.2577	1.7523			
31000				23.0				1.2787	1.8086			
31600			4.53					1.3036	1.864			
32200								1.3165	1.9483			
33800			,3332	.3124		.5094		1.3353	5339 11			
33400								1.3598	arra es			
34000								1.3810				
35200			.3735	.3436	.2290	.5129		1.4168				
36400								1.4571				
376m			.4120	.3800	.2300	.5157		1.4946				
38200			.4235	.3824	.2309	.5161		1.5115				
38800								1.5316				
39400			.4416	.4008				1.5495				
40600	- 1		.4577	.4239	,2372	.5168		1.5959				
42000			.4915	,4443	.2400	.5168		1.6427				
43200			.5126	.4488				1.6866				
44400			.5373	.4814				1.7251				
45600			.5590	.5046				1.7835				
46800			.5893	.5262			ı	1.7965	1.			

Table 53. Crack Propagation Data From Side 1 - AFCG-2 (Concluded)

		FLAW LENGTH (INCHES) AT FLAW LOCATIONS 1 THRU 9												
TOTAL		-	The same of the sa	the same of the same of the same of										
	0	0	3	0	⑤	6	7	.8	9					
47800			.6168	.5399	.2497	.5226		1.8512	010					
49000			.6381	.5724	.2516	.5201			3.34					
50200			.6685	.5990					-395					
51400			.6995	.6243					003					
52600	101		.7272	.6469	.2575	.5235								
53800			.7645	.6769					000 8,7					
55000	are is I		.8034	.7059	.2620	.5258			0 6 4					
63800	nial L.				.2842	.5326			200					
71800					.3355	5395								
78000					.3764	.5452			40.0					
83400					.4386	.5522								
88000					.5159	.5565			006					
90600					.5616									
92400					.6054	.5606			9					
98800					.7875	5639								
101400					.8858									
102600					.9351	.5667								
103400					.9732	.5686								
108800						.5696			00					
124600			0			.5747								
143000						.5933								
161200						.6075								
									1,234					
			D049		Election	87E, 1			inst.					
				1. 1					1					
			7 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Man and a	008	15 A			1347					
	2102.4		130001			554			0000					
	115 11								COST /					
	513				383	3128. 1			0.00					
	1.62		2012 1	15.5	884									
	1000				111 111	0.03			0.536					
					911 3				BALL B					
	3371				194. 1	100			0314					
					100 /	Day			COME					

Table 54. Crack Propagation Data From Side 2 - AFCG-2

			CRACK	PROPAGAT I	ON DATA	A AME I			
TOTAL		FLAW LENG	TH (INCHE	S) AT FLA		INS 1 THR	10 9		33.01
CICCES	0	0	3	(4)	(3)	6	7	. 8	9
EDM	ALC: SIL								
0			.0354	.0496	.2070	.5095	.5419	.5043	.1956
600			.0401	.0570	.2072	.5100	.5612	.5101	. 2039
1600		10.75.0	.0438	.05.63	.2064	.5103	.5873	.5270	.2183
2200	(2,8,6.)	E012	.0464	.0598	.2075	.5105	.6082	.5405	. 234
2800			.0518	.0633	.2105	-5145	.6325	.5545	.249
3400	Amelia		.0538	.0660	.2122	.5162	.6542	,5703	.266
4000			.0583	.0708	.2125	.5170	.6695	.5846	.288.
4600			.0612	.0731	.1324	1	.7060	.5920	.298.
5200			.0643	.0763		.5165	.7318	.6106	.319.
5800			.0674	.0810	.2160	.5172	.7627	.6245	.336
6400			.0708	.0833		.5176	.7933	.6389	.352
7000							.8165	.6506	. 372
7600				Est Sal	1601		.8467	.6636	.392
8200	10.5						.8832	.6813	.412
8800							.9050	.6997	.439.
9400			.0918	.1066	.2204	.5231	.9396	.7145	.463.
10,000							.9673	.7265	. 4838
10600	LAE ELL						9966	.744.5	.509
11200							1.0253	.7643	.530
11800							1.0500	.7768	.55
12400							1.0734	.8113	.570
13000							1.1086	.8080	.600
13600			.1231	.1399	.2255	.5259		.8237	.623
14200			1		1	1	1.1667	.8402	.648
14800					Electronia	1.12	1.1922	.8549	.672.
15400			12.	VE CL		CAR		.8728	.697
16000							1.2594	.8896	.723
16600							1.2931	.9034	.749
17200			101	384 54		Qui	1.3128	.9224	.776
17800			.1642	.1733	.2288	.5340	1.3287	.9384	.799
18400	440		1			1	1.3303	.9538	828
19000					1277	321	1.3970	.9728	.854
19600	E TE				130		1.4393	9864	.880
20000	and the			-			1.4735	.9960	.9000

Table 54. Crack Propagation Data From Side 2 - AFCG-2 (Continued)

	CRACK PROPAGATION DATA FLAW LENGTH (INCHES) AT FLAW LOCATIONS 1 THRU 9											
CYCLES				the same of the confession of					HATGI			
	0	0	3	(1)	(3)	6	7	8	9			
20800							1.5073	1.0147	.9323			
21400			.1979	3,2028	.2328	.5424	1.54.30	1.0283	.9555			
22000							1.5748	1.0438	.9813			
22600							1.6122	1.0584	1.0091			
23200	-6-1						1.6509	1.0725	1.0373			
23800	Alexander November		245014	190			1.6855	1.0870	1.0620			
24400							1.7218	1.1017	1.0950			
25000			.237	3 .2385	.2336	.5390	1.7535	1.1145	1.1247			
25600							1.7970	1.1330	1.1575			
26200							1.8391	1.1485	1.1829			
26800							1.8905	1.1685	1.2125			
27400							1.9213	1.1879	1.2407			
28000								1.2001	1.269			
22600		LV 51 6 -	.275	1 .2768	. 2403	.5399		1.2169	1.2969			
29200								1.2331	1.334			
29800								1.2533	1.370			
30400								1.2675	1.3995			
31000								1.2845	1.4374			
31600	Cattle Balle II							1.3039	1.4780			
32200	dania jan m							1.3212	1.5112			
33800			.331	9 .3740	2422	.5428		1.3351	1.534			
33400								1.3532	1.560			
34000								1.3683	1.5717			
35200		-36.5	.367	0 .3553	2460	.5450		1.3973	1.682			
36400	and the second							1.4311				
37600		D D V	.405	9 .3836	.2466	.5480		1.4788	1.7567			
38200			.420	1 .3984	.2490	.5481		1.4900				
38800								1.5074				
39400			.4400	4075				1.5259	1532			
40600			.460	2 .4280	2536	.5493		1.5644				
42000			.487.	5 .4540	.2539	.5509		1.6074				
43200			.506	9 .4687				1.6298				
44400			.530	8 .4895				1.6712				
15600		-	.557	8 .5107				1.7083				
46800			.583	8 .5342				1.7 346				

Table 54. Crack Propagation Data From Side 2 - AFCG-2 (Concluded)

			CRACK P	ROPAGATI	ON DATA				
CYCLES		FLAW LENG	TH (INCHES) AT FLA	W LOCATIO	NS 1 THRU	J 9		
CICLES	0	0	3	•	⑤	6	7	8	9
47800			.6043	.5517	.2591	.5562	(5)	1.7821	
49000	9.0	3 14 V	.6306	.5748		216	261	SVR-10	
50200		Lossel Bar	.6632	.6000	TIA DIL	08.0	eerb.	62.16	
51400	17-2	30 22	.6892	.6273	15 A 15 L	680	0.00	1882G	1 45
52600	6	TA101	.7248	.6533	.2723	.5601	8 F / (2 -	54.60	20
53800	5048.	2013	.7563	.6561	AR L	17 A D.	9/100	0.610	. 6.1
55000	1714	Eller	.79.33	.7134	.2785	.5619		3.8.8.	40.5
63800	Este	1414		5.0	.3115	.5720			
71800	A FORE	7 10	188	5.118	.3717	.5904		MA 513	106
75000	2184	Section 1		C2 (1)	.4291	.5890	4.9	Marine .	
83400	4314	4			.4988	.5967			
82000	184-		844		.5756	.6021	S.E.E.		
90600	I/I 2.	30 5	5.2	S. P. Branco	.6216	35 a Cal.	25 2		18
92400	NE COM		45.8		.6627	.6089	200	122	
98602	8048	5.147		4.3	.8375	.6179		Maria Land	
101400	15.42			Fo Carl	.9402	.6220		10354 X	
102600	6445	0 t 9.			.9848	.6230	10		
103400	\$8155	5.5.4	235		1.0266	.6237	£ 8 2	1623	
108800	1012	At least	10 F E			.6287			DC 5
124600	& COLL	9440				. 6423			
143000	22.	12 / E				.6656	Salar D	10.00	
161200	2015		<u> 1</u>	10 to 10		.6860	<u> </u>	0521	
		(O.E.)		4.1 S. W				1-2/4	
	1351	AASE			1583	P. P.S. Land	later.		
EFS (L)	e dale Non			asset L			WELL.		Ed. S.
58,840	ALLEL	W.C. & O.L.	E STANKE	114.		beck I	1855	00-00	OC.
2/ CS, 1/				M 46 1		1021	LSEQ	1829	<u>L</u> EUE
1.5.2.2		P.C.C.	Salar Bridge	Section Services	1000	err.	S. E. Say	0320	304
	J. F. F. Law	270	20023-20		3-5-67	LEGI.	EAROL	ASSES	ELF
			Laca.	100	£9.F4	enal.	EA HOLL	14.69	_ 112
		8.5 C L		1.93	16.2	5911			911
		QLL L	ALC: CANO	SILL	C. T. E. Laure		16.50	100	100
	2019.1	n - = -m		B 2 Lane	SKELL	ėlgi,	eako.	BRADIL	431
	1-5-2-1				2446	S. S. Salaman			
	1 1 1 1 1	S BEAL			16.64	MIA	MATERIA.	STATE AND	

Table 55. Crack Propagation Data From Side 1 - AFCG-3

		4 g	CRACK	PROPAGAT	ION DATA	id selle an	DV) J WAJ		
TOTAL		LAW LENG	TH (INCHE	S) AT FLA	W LOCATIO	ONS 1 THE	U 10	1	To deed
FLTS.	0	2	3	4	(5)	6	8	9	10
0	.0150	.0132	DELE	.0360	.2289	.2046	.5295	. 2168	.2179
41	.0159	.0133	.0363	.0417	.2291	.2093	.5460	.2472	.2685
72	.0206	.0144	.0394	-0436	.2398	.3121	.5696	.2691	.2853
152	.0240	.0175	.0430	.0684	.2456	.2126	.6147	.3023	.349
233	.0199	.0219	.0456	.0567	.2347	.2246	.6466	.3403	. 396
290	.0243	.0220	-0472	.0613	.2376	.2182	.6713	.3781	.440
350	.0245	.0222	.0528	.0645	.2434	.2195	.6826	.3969	485
380	.0246	.0222	.0549	.069.5	.2434	.2223	.6998	.4094	.505
410	.0246	.0241	.0569	.0696	.2474	_2233	.7103	.4312	
450	.0240	.0230	.0639	.0613	.2453	.1237		.4464	The second second
484	.0245	.0233	.0643	.0678	.2515	.2248	.7355		.574
525	.0248	.0235	.0678	.0695	.2523	.2263	.7502	.4817	.6046
565	.0270	.0248	.0180	.0750	.2533	.2292	.7742	.5034	
635	.0309	.0263	.0823	.0868	. 2598	.2315	.7977	.5408	
721	.0319	.0248	.0825	.0900	.2699	.2331	.8215	.5651	.7630
847	.0333	.0294	.0860	.0359	.2738	.2356	.8579	.6244	
932	.0354	.0312	.1027	.1092	.2815	.2357	.8975	.6582	249
1000	.0389	.0339	.1110	.1158	. 2879	.2394	.9175	.6904	
1070	.0390	.0341	1181	.1192	.2946	.239.5		.7072	1.105
1095	.0396	.0265	.1325	.1213	.2970	.2399	.9556	.7385	1.139
1115	.0400	.0262	.1238	.1247	.2996	.2430	.9662	.7500	1. 1730
1155	.0430	.0307	1256	.1345	.3010	.2444	.9809	.7727	1.230
1195	.04-53	.0365	.1299	.1398	.3036	.2491	.9934	.7951	1.282
1253	.0465	.0392	.1380	.1451	.3081	.2500	1.0278	.8254	1.3593
1306	.0466	.0397	.1434	-1467	.3178	.2609	1.0404	.8536	1.453
1373	.0467	.0391	.1501	.1574	.3216	.2569	1.0719	.8739	1.571
1405	.0520	.0400	.1559	1606	.3252	.2551	1.0904	9060	1.674
1453	.0525	.0423	1620	.1640	.32 85	.2565	1.1093	.9397	
1491	.0531	.0429	.1654	.1704	.3342	.2569	1.1242	.9724	
1516			.1703	.1835	.3348		1.1423	.9929	
1602	.0609	.0438	.1774	1875	.4103	.2608	1.1790	1.0475	
1724	.0608	.0484	.1914	.1987	.3664		1.2323		
1821			.2075	.2130	.3729		1.2517	1.1657	
1921	.0678	.0545	.2167	.3212	.3825		1.2850	1.1847	
2024	.0726	.0577	.2281	.2395	.3956	.2694	1.3129	1.2258	

Table 55. Crack Propagation Data From Side 1 - AFCG-3 (Continued)

			CRACK	PROPAGAT	ON DATA	i.i.en			
TOTAL		FLAW LENG	TH (INCHE	S) AT FLA	W LOCATIO	ONS 1 THR	U 10		
FLTS.	0	@	3	4	(5)	6	8	9	10
2124	.0765	.0596	2439	2513	.4066	.2729	1.3535	1.2700	
2225	.0795	.0648	.2480	.2670	.4239	.2764	1.3789	1.3333	5.4.2
2328	.0816	.0661	.2649	.2780	.4383	.2762	1.4027	1.3756	
2458	.0870	.0693	.2868	.2954	-4617	.2828	1.4510	1.4308	
2520			.2940	.3072	.4699		1.4763		
2595	.0930	.0710	.3047	.3169	.4862	.2831	1.4964		
2648			.3153	.3257	.4950		1.5258		
2700	.0971	.0731	.3266	.3360	.5080	2882	1.5390		
2757			.3304	.3576	.5223		1.5591		
2857	.1093	.0783	.3546	.3661	.5389	.2962	1.6103		
2945			.3733	.3843	.5763		1.6637		
3057	.1164	.0844	.3879	.4089	.5820	.3062	1.7231		
3104			.3992	.4222	.5992		1.7659		
3200	.1312	.0993	.4164	.4410	.6525	.3032	1.8004		
3260			.4265		.6472		1.8411		
3320			.4379		.6830	.3048	1.8762		
3380	.1342	.1037	.4511	.4822	.7059		1.9316		
3440	.1374	.1103	.4670	.5006	.7342	.3088			
3552	.1427	.1108	.4884	.5341	.7836	.3122			
3640	.1452	.1152	.5166	.5573	.8230	.3123			
3720	.1546	.1180	.5342	.5829	.8717	.3147			
3799			.5644	.6052	.9234				
3854	.1655	.1269	.5780	.6245	.9572	,3203			
3923	.1705	.1292	.5957	.6487					
3965	.1765	.1323	.6025	.6767		.3228			
4038	.1775	.1351	.6330	.6877					
4075	.1809	.1366	.6478	.7040					
4148	.1835	.14.09	.6718	.7426		.3283			
4200	1878	.1480	סדס ד.	.7680					
4240	1985	.1457	.7080	.7854					
4291	1948	.1520	.7260	.8119		.3278			
4344	.2046	.1539	.7376			.3388			
4640	.2305	.1661				.3385			
4786	.2435	.1744				.3420			
4886	.2537	1826				.3466			

Table 55. Crack Propagation Data From Side 1 - AFCG-3 (Concluded)

			CRACK	PROPAGATI	ON DATA				
TOTAL FLTS.	F	LAW LENGT	H (INCHE	S) AT FLA	W LOCATI	ONS 1 THRU	110		-741
FLIS.	0	2	3	4	(5)	6	8	9	10
4996	.2655	.1920	artes b			.3502		2 3 0 -	
5150		.2009				.3488	a 3		
	SERFI	1.502.	355 4	824. I	1275	1432			8118
	11,48,61	STEASIE	222.1	1333					
		e a racil		920.1	tens.	300			1111
		100	225.4	084 L	0.815		neco.		
				tera, l					6-12
			199	ace. I	1200	10.00	STY	2.55	Col
		0.00			17 2 2	0.83			
			307				OF BUILD	3501	1250
					1.532	3.00			
			308			3.87	tao.	4500	172-431
		in second				E 12. 1			47.1
		538.4	608		1000	200	ego.	2 (OG.C
		38.1							0,
			And I		C Tal.				0566
			ray l			1.23	ung i	205	ONE I
			ren	AST I					04.3
			216 1	25,62		0.0			11.387
			218 1					0.151	0.458
			2/5	Harte I	Parties	1000		SADI.	OSPI
					12.76				POTE
			0.07	(×)		terre.		Angl.	119
						7893	0.0	est.	828
			232		BES.	100		Carl	2.86
					- F8-31	10000	28	2.55	1.803
					4571	TAS.	atio 1	FO.7.1.	3.000
			865		10000	SUDA .	041.1	DEPT.	BAL
					BAT I	ties at .	1141 1	artu	Cr. S.
				-	285.1	OPE -	200	3 9 61	
			0.5%		2/19 }	200	1001	0.697	100
			5.5			F7 F		1100	- 60-
-			202						0.5
			238				السالية	ZEAC !	ART

Table 56. Crack Propagation Data From Side 2 - AFCG-3

TOTAL			CRACK	PROPAGAT	ON DATA	8 10111			
TOTAL FLTS.		FLAW LENG	TH (INCHE				U 10		4/1
FLI3.	0	(2)	3	4	(5)	6	8	9	10
0		12 15	.0356	.0422	.2210	.2040	.5020	. 2 222	. 2223
41			.0375	.0436	.2220	.2060	.5502	.2561	.2652
72		1	.0463	.0483	.2249	.2065	.5749		.3394
152		12 188	.0492	.0597	.2302	,2139	.6083	.3012	.3536
233		leini	.0538	.0640	.2354	.2124	,6331	.3441	.377
290		7-14-8	.0532	.0652	2351	.2123	,6507	.3631	.4146
350			.0586	.0701	.2366	,2125	.6739	.3920	.4509
380			.0638	.0719	.3406	,2158	.6830	.4032	.+760
410		101 3	.0668	.0747	.2462	.2168	.6916	.4202	.5060
450			.0688	.0786	.2467	.2168	.7048	.4380	
484		Jan Har	.0700	.0794	.2496	.2169	.7161	4490	.558
525			.0703	.0799	. 2527	.2165	,7221	.4587	.5803
565			.0765	.0800	.2529	.2207	.7379	.4599	602
635			.1251	.0921	.2477	.2170	.7358		.664
721		12162	.0927	.0944	.2650	.22.53	.7675	.5469	.7188
847			.0997	.0992	.2754		.8259	.6108	.8:119
932			.1061	.1215	.2827	.2309	.8576	.6509	.865
1000			.1128	.1253	.2838	.2312	.8879	.6736	.9370
1070			.1192	.1336	.2893	.2319	.9115	.7052	.986
1095			.1230	.1361	.2920	.2319	.9145	7 292	
1115			.1267	.1393	.2963	.2339	.9216		
1155			.1285	.1454	.3019	.2363	.9412	.7603	
1195			.1386	.1540	.3068	.2366	.9620		
1253			.1432	.1546	.3084	.2421	.9734		
1306			.1490	.1603	.3160				1.260
1373			.1545	.1653	.3222		1.0155		1.306
1405			.1609	.1682	.3249	.2422	1.0287		
1453			.1616	.1772	.3280		1.0624		
1491			.1679	.1813	.3411	.2468	1.0771	9528	1.457
1516			.2216	.1919	.3425		1.0840		
1602			.1810	.2006			1.1066		The second second
1724			.1996	.2093			1.1378		the second second second
1821			.2209	.2232	.3830			1.2818	Contract and a contract of the last
1921			.2213		.3830	.2561	1.2024		
2024			.2310		.3979				

Table 56. Crack Propagation Data From Side 2 - AFCG-3 (Continued)

TOTAL				PROPAGAT		V 32/67			
FLTS.			TH (INCHE						
1213.	0	2	3	4	(5)	6	8	9	10
2124	Keeka	10,002	.2439	.2545	4114	.2622	1. 2775	1.4618	
2225		15-12	.2556	.2709	.4273	.2662	1.3122	1.5972	
2328	lag ca	10000	.2701	.2866	.4437	.2698	1.3462	1.6268	li
2458	1000	les sa	.2834	.3048	.4570	.2705	1.3863		
2520	1400	11243	.2940	.3146	.4820		1.4070		-
2595	lu es	1	.2034	.3258	.5001	.2758	1.4447		
2648	[C.] 1-8		.30 46	.3355	.5063		1.4676		
2700	L. Fore		.3245	.3458	.5211	.2788	1.4983		
2757			.3300	.3568	.5334		1.5198		
2857	10 10		.3481	.3764	.5609	.2839	1.5666		1
2945	Tarle A		.3654	.3962	.5771		1.6086		
3057			.3848	.4192	.6148	.2843	1.6667		
3104			.3947	.4295	.6224		1.7025		
3200			.4153	.45 68	.6651	.2851	1.7272		-
3260			.4308	.4672	.6817		1.7393		
3320		1 62 6	.4434	.4791	.7019	.2916	1.7763		
3380		TATES,	4578	.4948	.7298	.2932	1.8052		
3440		1144	.4708	.5077	.7538	.2939	1.8386		
3552		7 - 2 - 1	4)68	.5382	.8162	.2968	1.9452		
3640			.5224	.5597	.8630	.2968			
3720		100	.5430	.5878	.9037	. 2998			
3799		1.0	.5633	.6004	.9562				1
3854			.5787	.6294	.9947	.3015			
3923	15 E8.	The state of	.5970	.6485					
3965			.6145	.6626		.3058			
4038			.6369	.7094					
4075	trade.	100	.6527	.7190					
4148		les bo.	.6689	.7481		.3081			
4200	1842	Lie to	7174	.7730		.3135			
4240	STEE.	la A la	7115	.7943		.3092			
4291	15 3 8 3		.7391	.8164		.3106			
4344	23 00		.7544			.3136			
4640					The state of the state of	.3198			
4786	E De					.3232			
4886					1	.3240			

Table 56. Crack Propagation Data From Side 2 - AFCG-3 (Concluded)

			CRACK	PROPAGATI	ON DATA				
TOTAL		FLAW LENG	TH (INCHE	S) AT FLA		ONS 1 THRU	10		
FLTS.	0	2	3	4	(5)	6	8	9	10
1996			70			.3268			
5150						.3340			
							(Internal		
		10:11	ETC.	10 10 10 10 10 10 10 10 10 10 10 10 10 1		7.08.00	A Line		
	4773		Para E	1124			116		
	2.022	1 (5 % (7 %)						4.45	
			15215	2.71.71.71	13385				
	1000	334	ETALL.	88.83	18904		18 4 6 1		
A	0084	1338	2000	53.00					
	13261	10000	8555	3.5931	3333	JAPA !		la nasa.	
	120.50	8188				10000		1 2 2 2 2	
	Set 1	Crev.		TAR STORY					
				200					
R 0 19						ROENEK I.			
		Date					SOFT		
	lana a						10.2.35	hasel	
								I BANKS	
		Erest.			1,1		23.00	Lt.a-e.o.i	
								lanao.	16.
			100					15000	2.2
			Lanca Control						
		100 600							
E CHELL				255			Control Control	le see	1 437
NAME OF	Table 1		Le car	erby				Lawrence .	
	Leans		ISPAC	2022	A COL				
	Lange 1	Caren	To be a little	La 8 (58)					
Range S.	le es		D. Wall					Tax-eal	
EFFS	APER.	10101	75.9.20				32.45		
				21216					
2235	ires.		17825				1 20		
1320		In ceal	10000		CANA				1 00

Table 57. Crack Propagation Data From Side 1 - AFCG-4

			CRÁCK	PROPAGAT	ION DATA				
TOTAL FLTS		FLAW LENG	TH (INCHE	S) AT FLA	W LOCATIO	ONS 1 THR	U 10	3	
. 2.13.	0	2	3	4	(5)	6	7	9	10
EDM	.0150	.0156	.0386	.0270	.2030	.2073	5051	.2186	.5008
2	.0182		.0431	.0322	.2072		.5173	.2357	.519
4	.0166	.0154	.0465	.0333	.2102	.2564	.5294	.2457	.538
13	1710.	.0163	.0501	.0330	.2142	.2075		.2601	.558
30	.0189	1710.	.0555	.0384	.2217	.2076		.2834	.581
74	.0240	.0210	.0674		.2344	.2139	.5987	.3265	.634
150	.0228	.0281	.1052	.0818	.2709	,2142	.6626	.3470	.651
212	.0209	.0237	.1339	.1088	.2938	.2173	.6482	.3648	.667
253	.0277	.0266	.1594	.1292	.3200	.2224		.3800	.636
305	.0293	.0300	.1921	.1684	.3674	.2278		.3994	.716
359	.0335	.0389	. 2 399	.2069	.4044	.2285		4245	.743
386	.0325	.0423	.2587	.2261	.4349	.2259	.7070	.4360	.739
397	.0357	.0433	.2711	.2340	.+499	.2275	.7137	.4302	300
413	.0421	.0446	.2836	.2551	.4692	.2266	.7205	.4317	.764
443	.0406	.0461	.3030	.2685	.5162	.2266	.8157	.4656	.792
459	.0347	.0493	.3219	.2787	.5284	,2319	.7133	.4 499	
479	.04.00	.0702	.3389	.2861	.5563	.2327	.7195	.4585	.799
499	.0361	.0501	.3610	.3079	.5883	.2338	.7241	.4606	.750
507	.0450	.0595	.3689	.3236		.2355	.7436	4696	.815
521	.0423	.0585	.3846	.3346	.6261	.2369	.7439	.4635	.834.
534	.0475	.0659	.3993	.3518	.6511	.2416	.7447	4762	.830
545	.0424	.0651	.4126	.3601	.6725	.24.15	.7422	.4780	.832
555	.0524	.0661	.4219	.3693	.6888	.2446	.7496	.4808	.837
565	.0503	.0675	.4381	.3831	.7121	.2450	.7427	.4850	.851
578	.0485	.0699	.4512	.3945	.7428	,2430	.7457	.4895	.851
601	.0583	.0776	4779	.4167	.7749	.2519	.7478	.5021	.856
608	.0567	.0747	.4704	.4317	.7889	2 475		.5090	
621	.0564	.0718	.4952	.4479	8372	2472	סררד.	.5090	
631	.0577	.0757	.5590	.4575	.8644	.2473	.7780	.5089	.869
641	.0617	.0729	.5294	.4696		.3467	.7570	.5206	
649	.0628	.0804	.5387	4778		.2483		.5242	
656	.0651	.0759	.5516	.4891		.2480	.7812	.5276	
664					.9695			_	
670	.0757	.0818	.5781	.5124	.9970	.2438	.7938	.5397	.902
702	.0699						1.0710	100	

Table 57. Crack Propagation Data From Side 1 - AFCG-4 (Continued)

TATA:		th (CRACK	PROPAGATI	ON DATA				1 212
TOTAL FLTS			TH (INCHE			IONS 1 THR	y 10		
80.4	0	2	3	4	(5)	6	7	9	10
722	.0767	.0940	. 6476	.5713	84 52	.2546	.7873	.5415	.9376
744	.0768	.0986	.6866	.6071		.2550	.7870	.5476	
762	.0764	.1055	.7061	.6395	3.5 (5.	.2551	.7884	.5475	
779	.1063	.1125	.7474	.6754	200	,2598	.7938	.5543	
793	.0830	.1044	.7648	.6823		.2551	.7968	.5633	
802	.0840	.1187	.7834	.7041		.2583	.8385	.5604	.987
821	.0903	.1234	4 1 5	7192		.2544	.7920	.5628	.974
841	1000	.1272		.7384	Z) el-	.2559	.7928	.5718	.992
859	1001	.1321	54 5.	. זררה	Quir.s.	.2604	.8062	.5697	1.021
876	.0992	.0933	8118	.8230	EX L	.2636	.8067	.5816	1.033
898	.1012	.1511		23 3	21	.2689	.8134	.5888	1.025
920	.1013	.1659	200	20 14		.2699	.8251	.6064	1.050
947	.1093	.1098			98	.3216	.8212	.6169	1.113
	10312. 15-61. 1582	18,075 18,37 18,43		6 00			8		

Table 58. Crack Propagation Data From Side 2 - AFCG-4

			CRACK	PROPAGAT	ION DATA				
TOTAL FLTS.		FLAW LEN	STH (INCHE	S) AT FL	W LOCATI	ONS 1 THR	U 10		
TEIS.	0	2	3	4	5	6	7	9	10
EDM			.0328	.0364	.2006	. 2034	.5068	.1141	.506
2			.0340	.0369	.2380	.2066	.5196	.2315	
4			.0315	.0360	.2379	.1999	.5185	.2418	.532
13			.0330	.0375	.2399	.2025	.5363	.2540	.551
30			.0385	.0460	.2425	.1990	.5565	.2757	
74			.0505	.0575	.2560	.2079	.5825	.3069	.606
150			.0962	.0806	.2798	.2263	.6547	.3342	.652
212			.1257	.1197	.3052	.2224	.6386	.3620	.666
253			.1597	.1413	.3264	.2277	.6465	.3739	.680
305			1890	.1710	.3527	.2269	.6549	.3888	.6710
359			. 2255	,2083	.3963	.2316	.6686	.4030	.674
386			. 2452	.2219	.4248	.2346	.6750	.4245	.675
397			.2571	. 2357	.4359	.2339	.6788	.4265	724
413			.2771	.2596	. 4577	.2371	.6888	.4360	.742
443			.2992	.2687	4780	.2382	.6957	.4408	.744
459			.3118.	. 2976	.4961	.2400	.7041	.4522	.758
479			.3367	.3046	.5262	.2449	.7041	.4572	.772
499			.3521	.3168	.5546	. 2455	.7162	.4640	.774
507			.3622	.3224	.5690	.2427	.7179	,4653	ררר.
521			.3713	.3375	.5920	.2430	.7200	.4705	.780
534			.3880	.3486	.6113	.2436	.7231	.4760	.783
545			.3517	.3578	.6330	.2446	.7275	4792	.7810
5.5.5			4160	.3669	.6503	.2443	.7269	.4811	.796
565			.4275	.3776	.6770	.2454	.7302	.4825	.795
578			.4475	.3912	.7035	.2970	.7375	.4929	.803
601			.4801	4136	.7596	.2510	.7521	.5163	.8123
608			.4907	.4220	.7672	, 2595	.8147	.5016	.816
621			.4988	.4306	.8000	.2530	.7612	.5077	.826
631			.5114	.4465	.8284	.2531	.7665	.5087	.826
641					.8536		.8130		
649			.5365	.4743	.8794	Control of the Contro			
655				4811	9022			.5215	A STATE OF THE PARTY OF THE PAR
664			.5676	4942			.7795		
670			,5711	.5008	.9972		.7782		
702				.5444			.7865		

Table 58. Crack Propagation Data From Side 2 - AFCG-4 (Continued)

			CRACK	PROPAGATI	ON DATA	Yaleya			
TOTAL		FLAW LEN	STH (INCHE	S) AT FLA	W LOCATI	ONS 1 THR	y 10		23.137
FLTS.	0	2	3	4	(5)	6	7	9	10
722			.6484	.5726		.2582	.7951	.5479	.8717
744			.6797	.6010		.2606		.5541	.875
762			.7033	.6291			.8117	.5644	
779			.7365	.6548		.2589		.5682	
793			.7646	.6786		.2588	.8262	1000	
802				:6896		.2593	The second secon		
821				.7166		.2634		.5814	- Contract Contract
841				.7590		2766	.8462	.6359	
859				.7822		,2598	.8407		Total State of the Control of the Co
876				.8196		.2749	.8504		
898						.2744	.8647	.6060	
920							.8849		
948							.9096		
									Ú8
								3	

Table 59. Crack Propagation Data From Side 1 - AFCG-5

TOTAL			CRACK	PROPAGAT	ON DATA	3.50			
TOTAL CYCLES		FLAW LENG	TH (INCHE	S) AT FL	W LOCATIO	ONS 1 THR	U 9		100
10.1	0	2	3	(4)	(5)	6	7	8	9
0	.0198	.0172	.0388	.0407	.2096	.1063	.2163	.3063	,2212
600	.0220	.0192	.0907	.0465		.2006	. 20012	.6237	. 2; 50
1400	.0226		.0452	11110		.2070	. 2902	.5557	,2760
2200	.02201	.0233	.0463	.0010		.2120	.3220	.5870	.3020
3200	.0230	.0170	.0537	2000:		.7121	.3808	istail)	3110
3600	.2773	.0202	.0022	1000		.1107	.3960	2332	3010
1000	0213	.0227	.0644	:0732		.2128	. 4102	4833	133.50
4600	1220	.0210	10034	0733	.1104	.2157	.710	.6729	+
L100	.0110	.0259	.0715	10127	.2152	.2199	· 474:	.6773	.17
5322	. 2237	.0255	.0791		.2172	.2221	.471-	שרייםן.	.; 37
6200	.0233	.0227	1/311.	1 750	.2192	2201	.6112	11200	.; 337
6377	0209	.0238	.0072	4011	:2290	2730	.640	.743-7	
1200			.0879	11:30		.4215	. 15 Jahr.	.7:271	.6.120
7600			.0942	: 175		.2241	.07~	.7757	2600
3000			.0984	1009		.22957	1, 190	.794=2	.5825
3400			.1030	1030	1771	.2260	.6313	.305	.: 093
3300			.1018	.1111		.2200		.3740	.6307
0.200	1200	.0296	.1132	1305	.2310	:439	.7524	.3762	.7074
11,000			.1290	.1346	.2420	.2343	.3003	.27252	-000
11400			. 193	.1400	.27:5	.2326	.878	.9316	7900
800	.0258	.2210	. 578	. 1.33	.2111	.2320	. 8639	17430	
2200			.1411	.1537	.4.30	2178	.89062	1.37	.8374
2600			.180,00	.15,73	.11732	.2123	.9221	.9820	.3857
3000			1178	.1701	25,78	.2431	.7512	.7872	.9079
3400	.0259	.2162	.1:193	.1740	17733	.21 -5	9880	1.0083	.9358
13800			.1627	.777	11:001	.2164	THE RESIDENCE OF THE PERSON NAMED IN	1.0230	.9674
19200	0198	0264	·1652	. 343	17737	.2440	1.0398	1.0383	.9950
14400			. 2011	875	.2627		1.0935	1.0440	10114
19800			.1667	. 752	.2654	.2431	1.0710	1.0613	1.0367
15600			1307	.10:20	.2726	.2018	1.1385	1.0868	1.1012
16000	.0307	0288	.1363	2089	.2748	.254:	1.1598		1.1267
16400			.1900	2151	.2800	25100	-		1.1520
16800			.1970	.2189	.2859	110,00			1.136
17200			1990	1201	.2391		1.2660		1.220
17600		ezerbituare per al	.2029	.2270	.2941		1.2929		1.7610

Table 59. Crack Propagation Data From Side 1 - AFCG-5 (Continued)

			CRACK	PROPAGAT	ION DATA	MOARC			
0400 0000 19200 19600 20400 21200 21400 21400 21300 21300		FLAW LENG	TH (INCHE	S) AT FL	AW LOCATIO	ONS 1 THR	RU 9		
CICLES -	0	2	3	4	(5)	6	7	8	9
18000	.0322	.0195	2110	.2339	.7970	2003	1.3276	1.1750	1.2750
18400			.2157	.2917	.3035	.2632	13636	1.1983	1.3044
18800	R. Stell		.2229	.2488	.3084	1691	1,3893	1.2090	1.3320
19200	.0312	.0313	.2302	.2551	3146	1650	1.4169	1.2220	1.3586
19000	.0318	.0390	.2311	.7420	.3340	.2708	1.9022	1.1509	1.3841
20000	8-47		.2393	2710	.3080	.2728	1.4760	1.7901	1.4260
20400	DATE		.2226	.2798	.3300	.2739	1.5078	1.2649	1.4517
20800	.0371	.0317	.2376	.2762	.3371	.2087	1.6957	1.2871	1.4811
21200	.0389	.0366	.2055	.2917	.3363	.2017	1.5901	1.3025	1.5309
21400	.03750	.0378	2576	.2829	.3963	.2728	1.6022	1.3123	1.5463
21600	PER A		.2000	.2932	.3475	.2781	1.6280	1.3320	1.5062
21800	.0385	.0416	.2694	.2942	.31072	1310	1.6350	1.3359	1.5782
22000	ing to g		.2717	,3035	.3/37	.2861	1.6478	1.3921	1.5978
22400	5755		.2768	3120	3010	.1308	1.7017	1.3616	1.6304
11800	3 (6 t)		. 2800	.3198	3112		1.7217	1.3787	
23200			.2913	.3280	31.30	7	1.7574		1.6995
13600	.0389	.0429	.2981	.3372	3751	.1907	1.8027		1.7291
14000			3060	3444	.3818	.1919	1.8508		1.7798
14420			.3118	3643		. 2931	1.8853	1.4642	1.3112
24800			.3187	.3639	. 3923	. 2988	1.9517	1.4633	1.3579
251200			.3259	.3717	.4032	.2989		1.4769	1.3388
(1000)			.3298	.3774	.4173	.2989		1.4946	1.9128
2600	2420	.0100	3408	.3332	.1.73	.2999		1.4797	353(8)
26400			.3137	39=10	. \$220	3000		1.0170	
26800			3503	.3730	.4387	.3012		1.6300	
27000	.0430	.0437	3539	7080	.9321	.3039	OBAN.	1.5358	.0
27200			.3632	3657	.4331	.3034		1.5614	100,000
27400			3668	4.234	.4396	.3087		1.5062	
1:1600			.3087	.42300	.4513	3074		1.5678	7.57.19
27300			.3690	.; 196	1447	.4090		1.5838	
73000			.3710	.4329	. 15,33	.3124	-3/3/3/II	1.5850	
	.0492	.7470	.3771	.1182	4:33	.3/20		1.5987	
18600			.3835	.1C167	.+712	.3/30	19 113	1.6176	
19000			13922	.4656	.4837	.3127		1.6307	
199.20			3980	1697	.4373	.3128	1	1.6470	135505

Table 59. Crack Propagation Data From Side 1 - AFCG-5 (Continued)

			CRACK PROPAGATION DATA										
TOTAL		FLAW LENG	TH (INCHE	S) AT FL	AW LOCATI	ONS 1 THR	U 9						
CICLES	0	2	3	4	(3)	6	7	8	9				
19800	.0452	0034	.4081	.4861	.4995	.3183	BP YS	1.6084	Model				
20200	REAL.	EARLY I	.4162	.4875	.5021	3200		1.6739	COLE				
30600	0.00030	2101	.4797	4997	,5201	.3236		1.6363					
31000	- 111	P214 1	.4351	.5156	.5268	.3213	6180	1.700	Cas				
31400	1000	33598	.4448	.5290	.5393	.3292	SPES	1.7130					
32000		day ii l	.4603	.5487	, 5,573	.3282		1.7473	TO CO				
32000	52.5		.4708	.5077	1.5794	.3303		1.7730					
33200	.0488	.0627	.4342	.5879	.6940	.33350	United S	1.8031					
33800	1333		.5006	.6152	.6160	.3350	Grant 1985	1.3246	17.5				
39400			.5130	.6321	.6380	.3376	5000	1.3400					
35,000	Contraction of		.5341	.6576	.6626	.3380		1.8796					
35400			5417	.6720	.6810	3905	100	1.9004					
45 800	.0923	.0662	.5522	.6850	.7046	3192		1.9155	de de				
36200			.5696	.1091	.7172	.3982		1.9424.					
30000			.5804	.7185	.7337	3512		1.9072					
37000			.5902	.7461	,7523	.36722							
37400		17 SIG 11	.6016	.7577	7093	. 3623	10.30	08.					
37800				17742	.7918	.3501							
38200			. 6255	.7991	.3109	.3007							
38600			.6337	.8120	.8342	.3529			100				
39000	.0097	.0821	.6443		.8191	.3010							
39200	18.4		.6519		.3712	. 3522			No.				
39800			. 6713		.9010	.3512							
\$0,200			. 6837		.9190	.3631							
10600			.6933	130 ()	.9010	. 3698							
91000	.0047	.0886	.7079	177	. 9760	.3689	1/5 25	2836					
11400			.7173		10093	.3710			COST				
92000			.7847	MELE.		. 3783							
\$2400	Provide a		.7592	E NOTE	13 T S V	.3788			1000				
42800	35200		. 7760		1000	.3827			381				
43200	.0702	.1024	. 7958	83.0	89.83	. 3827							
	.0816	1222	Mark	A 1 1	Eland	.4019							
	.0913			1111	7.1-3.5.1	.4221							
52400		.1720	TARR	2.5	with L	. 4436							
545200	:13/7	.1986	Received			. 4658			11-11-1				

Table 59. Crack Propagation Data From Side 1 - AFCG-5 (Concluded)

	CRACK PROPAGATION DATA												
TOTAL		FLAW LENGT	H (INCHE	S) AT FLA	W LOCAT	IONS 1 THR	U 9		1 244				
CICLES	0	2	3	①	(5)	6	7	8	9				
57200	.1473	.2178	4.00		research	.+307							
5880		.2211	2000			1933			100				
59300		.2486	y lots to		Link row	1.57.52			2525				
6082		.2673	Jane			,4999			E SAN TA				
61300		.2700	D.O.S.		RENT	.5062							
62300		.2839	Park		91.612	.5069							
	.20000		5393		610	.6186							
3 17.4	Liena.	Ersa	4.515		Life its	10.65							
- 5 4 5	Contract No.	I zyna i	4.4.5.3						Contract of				
	To a Page	121.4											
	mxs/		178.0						19/2 3				
		Te de la constitución de la cons											
						2000							
	Let'Latte		2724	30.77 (6.0		10000							
						24.00		1					
						1 No. 1							
						 							
			E v I L										
e e													
	1 10 5 100					2000							
				y 3. 8 s									
								 					
									1				
				43 1 . 3 %									
9-1-20-0	The No. On the	CONTROL OF		3.64.8									
						1							
	200					No.							
					1 PS 1	-							
	San un	25 17 15		333		200							
-						-							

Table 60. Crack Propagation Data From Side 2 - AFCG-5

			CRACK	PROPAGAT	ION DATA	ADAF)			
TOTAL CYCLES		FLAW LEN	GTH (INCHE	S) AT FLA	W LOCATI	ONS 1 THR	U 9		
CICLES T	0	2	3	4	(5)	6	7	8	9
0			.0200	0000	.2077	.2145	.1724	.5037	.2177
600			1 1 1 5 3	.0085		.2093	.2428	.5220	.2412
1400			.0385	.0084		.2092	. 2682	.5483	,2728
2200			.0527	.0610		.2084	. 2740	.5773	,3125
3200			.0580	.0098		.2034	.3320	.6150	.3474
3600			0614	0100		. 2199	.3474	.6239	.3620
4000			0652	.0148		.2222	.4026	.6390	.3764
4600			.0688	.0196		.2244	3393	.6590	.4012
1200			.0799	0235		.2261	.4073	.0870	.4227
5800			.0730	.0278	.2000	.1265	.4332	.6953	.45,27
6200			.0753	.0286	.2081	.2311	.4477	.7035	.4673
4300			.0784	.0359	.2085	. 2327	.4659	.7197	.49150
7200			.0823	.0371	.2138	.2290	.4855	.7343	.5113
7600			0870	.0430	,2173	.2313		.7515	
8000			.1000	.0433	.2185	.2335		7650	
8400			.1042			. 2330		.7820	
8300			.1063			.2335		.8010	Committee of the Commit
10000			1183		.2209	THE RESERVE THE PROPERTY OF TH		.8532	
10800			.1215	.0893	.2233	. 2473		.8800	
11200			.1200	.0801	.2391	. 24.42		.9037	
11600			.1298	.0963	.2903	. 2440	.7120	.9157	.7730
12000			1.1378	.0973	.2923	.2957	.7311	.9328	.7928
12400			.1397	.1083	.2403	.2479	.7528	.9408	.8144
12800			1379	1064	.2969	.2968	.7800	.9608	.8435
13200			1765	1120	.2434	2522	.8008	,9747	.8750
13800			1.1547	.1261	.1480	.2520	.8251	.9910	.9023
14200			1600	.1341	.2530	.2510	.8516	1.0007	.9289
19900			1663	.1393	.2530	.2514	.8444	1.0135	.9364
14800			1669	.1386	.2545	.2515	.8730	1.0273	.9602
15000			.1099	.1108	.2578	.2514	.9089	1.0438	.9823
15600			.1760	.1460		2016		1.0017	
16000				.1578	.2620	.2601	and the same of the same of	1.0793	THE RESERVE TO A PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TWO IS NAMED IN COLUMN TWO IS NAMED IN THE PERSON NAMED IN TRANSPORT NAMED IN THE PERSON NAMED IN
16200			.1863	.1673	.2695	.2630	.9715	1.0971	1.0580
16900			.1914	.1715	.2769	.2017	9968	1.089	1.0838
17200			.1909	.1790		.2696			

Table 60. Crack Propagation Data From Side 2 - AFCG-5 (Continued)

			CRACK	PROPAGAT	ION DATA				
TOTAL CYCLES		FLAW LEN	GTH (INCH	S) AT FL	AW LOCATI	ONS 1 THE	RU 9		a later
UTCEES	0	(2)	(3)	4	(5)	6	7	. 8	9
17600			1981	.1785	.2801	.2064	1.0503	1.1955	1.1335
18000			.2023	.1890	2829		1.0700	1.1580	
18400			.2005	1963	.2810	.2683	1.1010	1.1780	1.1840
13800			1.2110	.2020	.1950	.2690		1.1910	1000
19200			.2173	2082	.3052	.2738		1.2093	
19600			.2212.	.2200	.3100		1.1856		12057
10000			. 23250	.2321	.3189	.2732		S. Landau and C. Carriero	1.2851
20400			.2344	.2340	.3166	.1785	1.2399	1.2021	13038
20300			.2916	.2468	.3213		1.2678		1.3370
21200			.2503	.2001	3336.		1.2912	1.2723	
21400	C. T. Viss		.2187	.3040	.3338		1.3012	1.2989	1.3796
21600			.2533	.2621	3300	The second second	1.3183	1.3109	1.4000
11800			.2611	.2863	. 5367			1.3190	
22000			.2616	.2655	.3379				1.2190
224.00			.2667	.2793	3952			1.3900	
11300			1.2744	.2859	.3507		1.3987		
23200			.2811	.2983	3546		1.4278		
23600			. 2886	.4030	3618	.2319	1.4535		1.5470
29000			1.2994	.3168	.3678	1394		1.4075	
24400			.3003	3138	.3711	.2876		1.4180	
29800			.3076	.3298	.3769	.2894		1.9327	1.6285
20000			.3125	.3370	.3827	.2902	1.5460		1.6609
15600		0	.5190	.3418	.38400	.2892	1.5701	1.4700	
26000			.3252	.3563	.3980	.2931		1.4860	
26400			.3313	.3684	.4070	.2919	1.6229		1.7539
16800			.3379	.3768	.4164	.2973		1.5207	1.7847
27000					.4200	.3019			
27200			.3418		.4292		1.6893		
27400			.3450		.4304		1.6977		
27600			.5950	3960	.4310		1.7163		
27800			.3516	.3999			1.7308		
18000				.4064		.3009		15693	
18400			.3608		.4409	.3020		1.9916	
28600			.3681	.4227	4420			1.0038	Compose o
19000				.4347			1.8365		South Residence

Table 60. Crack Propagation Data From Side 2 - AFCG-5 (Concluded)

			CRACK	PROPAGAT	ION DATA	Nation J.			
31400		FLAW LEN	GTH (INCHE	S) AT FLA	AW LOCATI	ONS 1 THR	U 9		643
CICCES	0	2	3	4	⑤	6	7	8	9
31000			9238	.4970	.500	-31100		1.6960	
31400		MARKET	.4300	.5130	.519	.3148		1.7133	
32000			.4401	.5270	.5191	.3167		1.7423	
32600			1.2627	.5438	5516	.3192		1.7071	
33200			. 9729	:5689	5,670	,3209		1.7737	
33300			. 4865	.5966	.5862	3240		1.8.79	
34400			.6017	.6133	. 2107	3275		1.3030	
35000			. 5112	.6373	.6329	.3277		1.3320	
30,400		C Total	. 5273	.65,70	.6108	.3329		1.9077	
35300		3.12	. 52/3	10691	رعادي.	.33++		1.72+	
36200			.5498	.6857	.6701	3300		1.71 2	
36600			.5600	.7095	:676	.3370			
37000		μ	.5755	.7207	7112	7,747			
37400		Coet.	.5860	.7431	. 1392	. 4. 5£			
37800	SAME	WITE.	. 5978	.7663	170300	3,42			
38200			.6200	.7768		.3:02			V
38600			.6177	.7971	. 1856	. 3411			
39000			. 332	100 to 100 to	.8050	.3 + 24			
39900			.6813		.8276	-			
39300		316	.6556		.3512	3508			
40200	5.5		.6460		.3738	3527			
40000			.6785		.8770	.3531			
41000			.6738		.1:84	.3589			
41400			.7080		.9574	3572			
42000	No.	433 0).	.7255			.3615			
92900	1703-00	No. of the last	1.7416		No and the	.36 \$1			
42800	Pera.	A Section	.7690	38131	P-94	.3627			
43200	teres.	e John	.7710	8000		.3631			
46200	to Pari	TIPE				3825			1299
49200	THE SE	241		C 10		.3967			11.
52400	Vibral I	13.7			To late la	.4083			
555:00		ELWT.			P VS.D.	.4186			
57200					20713	.1160			4373
58800	SE SEC.	STITE	18675		7 13 4	.4361			Diseis.
59800	PAGE	CLASS.	10191	REAL	4487	.1378			

Table 61. Crack Propagation Data From Side 1 - AFCG-6

TOTAL			CRA	CK PROPA	GATION D	ATA	05			
FLIGHTS		FLAW LEN	GTH (INC	HES) AT	FLAW LOC	ATIONS 1	THRU 10)		
LEIGHI2	0	@	3	4	⑤	6	7	8	9	10
0				and the			.1994	.4990	.1971	-
20	.0200	.0047	.0348	.0362	. 2126	.3040	.2210	.5030	.2028	.322
38	.0175	.0050	.0330	.0361	.2232	.1959	,2212	.5186		.229
50	.0186	.0055	.0325	.0387	.2203	.2007	,2289	.5252		.233
70	.0163	.0038	.0351	.0363	.2230	.2047	. 2335	.5250	.2277	
85	.0202	.0048	.0383	.0334	,2271	. 2079	.2432	.5313	.2279	
100	.0192	.0064	.0407	.0362	.2216	2102	,2432	.5392	.2354	
120	.0198	.0061	.0390	.0376	.2152	.2053	.2466	.5424		
169		.0065	.0416	.0346		.2083	.2631	.5527	.2583	The state of the s
221			1				.2774	.5658	.2620	
278							.2916	.5815	.2769	.313
339	.0264	.0075	.0508	.0422	. 2220	.2084	.3088	.5898	.2904	.332
400							.3264	.6076	,30 48	.354
451							.3345	.6165	.3153	.370
500							.3527			. 383
550	.0266	.0053	.0570	.0469	. 2335	. 2125	.3682	.6292	.3394	.401
601	.0293	.0069	.0593		.2259	.2087	.3732	.6429		
651	.0301	.0056	.0665	.0485	. 2294	.2122	.3904	6515	.3673	
700	.0268		.0649	.0531	-2303	-2146	.4048	.6581	.3806	.46
750							4197	.6772	.3952	.477
800							.4361	,6866	.4072	.498
855							.4515	.6968	.4186	.512
905	.0280	.0075	.0780	.0570	.2413	.2195	. 4665	.7051	.4354	.530
962	1						.4830	.7135	.4484	.547
999							.4928	.7209	.4581	.561
1040							.5013	.7267	.4704	.575
1074	.0285	.0077	.0865	.0629	.2461	. 2225	.5125	.7339	4789	.591
1104					-		.5198	7369	.4920	.601
1136							.5271	.7446	.4938	.609
1179							.5361	.7505	.5112	.630
1215	.0316	.0069	.0925	-0676	.2486	.2231	.5490	.7585	.5151	.640
1245		11					.5608	.7623	.5240	.64
1276							.6184	7696	5300	.663
1305	.0340	.0084	.0977	.0723	2480	.2229	.5776	7755	and the second second	

Table 61. Crack Propagation Data From Side 1 - AFCG-6 (Continued)

TOTAL			CRA	CK PROPA	GATION D	ATA				BAKOT
TOTAL		FLAW LEN	GTH (INC	HES) AT	FLAW LOC	ATIONS	THRU 1	0		2771.07
FLIGHTS	0	2	3	4	(5)	6	7	8	9	10
1335							.5617	.7525	.5265	.6900
1370			3 3 3		18.0		.6002	.7957	.5641	.7051
1402			.0992	9779		.2247	.6065	.7962	.5724	.7037
1432					.2617		.6193	.8043	.5737	.7235
1461	.0357	.0056					.6292	.8094	.5807	.7253
1510			.1095	.0812	.2637	.2312	.6468	.8215	.5982	.7436
1553		200			.2660		.6584	.8262		
1584	33.5	TO A COLO					-6669	.8302		.7745
1624							.6818	.8375		
1655			ACT III				.6921	.8443	SALES MALE AND AND AND AND AND AND AND AND AND AND	.7972
1685							.7011	.8484		.8078
1709	.0424	.0070	.1251	.0822	. 2675	.2367	.7063	. 8530		.3176
1737							.7238			
1757							.7392			.8382
דררו							.7304			
1797						02-40-2	.7334		.6848	
1817	.0426	.0072	.1285	.0915	. 2743	. 2386			.6783	.8530
1837					P. C. P	11400	.7491	.8803	.6792	.8584
1857					SLE LA	14.4	.7499			
1877	0.01						7561	.8814		.8814
1905	ESS P.L.						.7642	.8834		
1925	.0455	.0076	.1341	.0992	.2807	.2415		.8876		
1946							.7799	.8868		
1981			711 9				.7842	.8929		.9185
2021			.1385	.1050		.2432	.7986	.9023	.7254	
2070		DA S	1	1			.8188	.9106		
2120	-0482	.0064			. 2962	Back Class		.9156		
2174			33 4					.9235		
2224								.9288		
2265							The second secon	.9889		
2307								.9452		
2352	.0512	.0074	.1507	.1160	.3017	.2530	.8970	A CONTRACTOR OF THE	and the same of the same of	
2405		1		1				.9613		
2453	217 25, 3	581 07	85 F	12.3	- to 3	12.1		.9660		

Table 61. Crack Propagation Data From Side 1 - AFCG-6 (Continued)

TOTAL			CRA	CK PROPA	GATION D	ATA				
TOTAL		FLAW LEN	GTH (INC	HES) AT	FLAW LOC	ATIONS	THRU 1	0		
FLIGHTS	0	2	3	④	(5)	6	7	8	9	10
2503							.9456	.9731	.8493	1.1016
2563	.0561	.0133	.1583	.1259	.3112	. 2554	.9668	.9809	.8593	1.118
2607							.9807	.9939	.8761	1.137
2651							.9946	1.0021	.8985	1.157
2690							1.0081	1.0091	.8953	1.172
2720	.0579	.0135	.1636	.1325	.3140	.2555	1.0121	1.0154	.9036	1.185
2770			1672	.1407			1.0425	1.0193	.9186	1.207
2820							1.0419	1.0369	.9289	1.230
2862	.0635	0170	.1720	.1456	.3270	. 2623	1.0552	1.0350	.9398	
2911								1.0413	.9594	
2961	Ta t	B						1.050	.9702	
3010								1.0374		
3058	.0693	.0192	.1833	.1550	.3281	.2625	1.083	1.0687	.996.3	
3105								1.0735	1.0055	1 332
3139							1.1302	1.0771		
3174							1.1405	1.0854		
3226	.0708	.0216	.1951	.1660	.3435	.2672	1.1584		1.0362	
3276					7.		1.1753	1.1046	1.0500	1.385
3330							1.1902		1.0623	
3381							1.2023	1.1189	1.0680	1.419
3436	.0772	.0201	.2078	.1730	.3535	.2765	1.2213	1.1263	1.0806	1.437
3490							1.2358	1.1382	1.0938	1.457
3545							1.2509	1.1516	1.1039	1.472
3605							1.2740	1.1584	1.1197	1.503
3655							1.2870	1.1651	1.1361	1.464
3706	.0831	.0245	.2268	.1887	.3716	.2791	1.3096	1.1652	11440	1.540
3757							1.3185	1.1874	1.1603	1.556
3807							Annual Control of the	1.2002		
3859							1.3553			
3907	.0878	.0247	,2435	.2047	. 3745	.2842	1.3784			
3957							1.3930			
4011							1.4139			
4061							1.4286			
4111	.0821	.0255	.2673	. 2203	.3891	.2920	1.4570	1.2595	1.2636	1.706

Table 61. Crack Propagation Data From Side 1 - AFCG-6 (Continued)

TOTAL			CRA	CK PROPA	GATION D	ATA				4.0
		FLAW LEN	GTH (INC	HES) AT	FLAW LOC	ATIONS	THRU 1	0		
FLIGHTS	0	2	3	4	(5)	6	7	8	9	10
4161							1.4801	1.2610	1.2823	1.7391
4211							1.4991	1.2737	1.2968	1.7535
4262								1.2823		
4311	.1028	.0368	.3364	.2334	.4042	.3435				
4365							1.5467			
4413								1.3051		
4466								1.3082		
4518	.1086	.0283	.3028	.2368	4181	.2991	1.6060			
4573								1.2810		14 8 6 6
4625								1.3336		
4675	.1132	.0326	.3117	.2560	.4337	.3018				
4727								1.3537		781 5
4830	W-1		8 8 4 5 5 5					1.3707		
4890								1.3813		
4943	.1263	.0332	.3359	2758	.4607	.3070			Charles and the second and the secon	Annual Control of the last of
5043		.0360			.4676		1		1.5396	
5143	1	10360	.3431	2010	-+010	1			1.5684	
5245									1.6047	
5345	.1400	.0377	.3692	.3011	.4980				1.5819	
5447	1		1						1.6762	
5548									1.7212	
5645	.1510	0303	3086	.3252	.5471	.3238			1.7450	
5732	.1559		4011		.5364				1.7592	
5833	.1617	The second	.4124		.5439			1.5349		
5933	.1663		.4189		.5542					100
6057	1681	.0428	.4312	.3633		.3319		1.5506		
6175		.0436						1.6120		V 300
6325	.1851				.6149			1.6470	 - - - - - - - - - 	
6475	1918		.4675							
6676	.1967			.4263				1.6787		
67.50	.2048			.4365				1.7196		12
6867		.0533								
6997	.2184		.5197		.7221			1.7694		
7150		.0611		.4899				1.8369		

Table 61. Crack Propagation Data From Side 1 - AFCG-6 (Concluded)

TOTAL			CRA	CK PROPA	GATION D	ATA				
		FLAW LEN	GTH (INC	HES) AT	FLAW LOC	ATIONS 1	THRU '	10		
FLIGHTS	0	2	3	4	⑤	6	7	8	9	10
7302	.2324	.0628	.5616	.5128	.7754	.3656		1.8857		
7425	.2401	.0658	.5797	.5270	.8062	.3689		1.9544		
7675	.2437	.0663	.7034	.5514	.8337	.3512	Ball N.	1-1-1		
רצרר	.2763	.0703	.6252	.5727	.8766	.3723				
7876	.2616	.0767	.6523	.5921	.9030	.3711				
7981	.2690	.0734	.6740	.6074	.9310	.3740				
8083	.2761	.0783	.6980	.6228	.9639	.3740		+		
8213	.2869	.0807	.7198	.6446	1.0074	.3845				
8363	.2949	.0804	.7446	.6704		.3858				
8503	.3043	.0805	.7748	.6966		.3906				
8604	.3107	.0884	.7932	.7 135		.3937		+		134
8757	.3250	.0861		.7320		.3962				
8862	.3284	.0946		,7548		.3904				
8963	.3003	.0960		.7702		.4054			1	
9059	.3436	.0962		.7983		.4007				
9075	.3368	.0997		.8035						
9111	.3399			.8093						
9243	.3462	.1020		.8201		.4087				
9383	.3637	.1099				.4156	-		\dashv	
9608	.3826				_			1-1-1		
9839		1253				.4078				
10039	.4020	.1283			_	.4104				
10243	.4411	.1411	34.			.4338				1
10316	.4451	.1375				.4338		1		
		531.46.2								
								-		
										2 4
		dente						-		
								-		

Table 62. Crack Propagation Data From Side 2 - AFCG-6

			CRA	CK PROPA	GATION D	ATA	NO.			
TOTAL FLIGHTS		FLAW LE	NGTH (INC	HES) AT	FLAW LOC	ATIONS	THRU 1			
Lidins	0	@	3	4	(5)	6	7	8	9	10
0					.2049				_	
20	1		.0289	.0240		.2107	.2467	.5912	.2140	.236!
38			00300	.0225		.2193	.2615	.5536	.2244	.2450
50			.0184	0215		.2135	.2694	.560%	.2304	.2550
70			.0231	.0226		.2176	.2802	.5685	.2339	.2645
85			.0222	.0214		.2185	.2903	.570!	-2406	.2690
100			.0241	.0254		,2189	.2971	.5766		.2788
120			.0235	.0227		220	.3071	.5860	.2472	.7823
169			.0244	.0227		.2219	.3252	.5970	.2557	.3111
221						.2175	.3451	.6125	.2678	.3183
278					.2085	.2251	.3671	.6258	.2813	0725.
339		1	.0327	.0268	.2075	. 2278	.3875	.6406	.3004	.3523
400							.4125	.6538	3166	.37146
451							.4378	.6644	.3338	3509
500							.45 04	.6745	-3410	.4032
550			.0328	.0305	.2142	.2317	. 4756	.6853	.3527	.4241
601			2244	.2324	.2140	:2577	.500E	.6973	.3643	.4435
651			1.7:48	.72p!	-2167	.222.1	.5229	1001.	.3723	.4.E11
700			.7:53	.0355	.218;	.232.	.5401	.7203	.3804	.4660
750			1			1	.5719	.7317	.3966	.4830
800							.5977	.7127	.4122	.5032
855							.6238	.7549	4287	.5224
905			.0412	.0411	.2252	.7403	.6496	.7644	4449	.5427
962				1			.6860	.775!	.4522	.5689
999							2079	.7824	.4568	.5783
1040							.7292	.7977	4668	.5938
1074			.0448	.0494	.2292	.2417	-7573	.8105	.4759	.6022
1104			111				.7833	.8212	.4894	-6147
1135							.7968	.8199	-5015	.6254
1179							.8247	.8385	.5105	.6454
1215			.0485	.0516	.2394	.2492	.8511	.8505	.5160	.6580
1245		-	1		-		.8762	-8601	.5276	-6673
1276		1					-8967	.8676		
1305							.9202		.5347	.6949

Table 62. Crack Propagation Data From Side 2 - AFCG-6 (Continued)

	CRACK PROPAGATION DATA											
TOTAL FLIGHTS		FLAW LE	NGTH (INC	(INCHES) AT FLAW LOCA			CATIONS 1 THRU 10					
	0	2	3	4	(5)	6	7	8	9	10		
1335			.0510	.0518	.2394	.2450	.9445	.8815	.5439	.7039		
1370		0.0				10	.9683	.8925	.5527	.7181		
1402							.9930	.9049	.5623	.7310		
1432		58.48					1.0190	.9129	.5708	.745		
1461			.0549	.0606	.2454	.2460	1.0423	.9230	.5800			
1510					333 55	200	1.0818	.9385	.5938	יררר.		
1553					.2513		1.1160	.9573	.6011	.7974		
1584							1.1479	.9727	.6107			
1624			.0593	.0727		. 2484	1.1839	.9832				
1655		18					1.2141	.9904				
1685					S. H. L.	Sara a	1.2477	1.0010				
פסרו		- 1 1	.0665	.0768	.2570	.2487	1.2736	1.0095		.8734		
1737		24 3					1.2961	1.0194	.6524	.885		
1757		1 10 1					1.3181	1.0512	.6593	.895		
רררו								1.0317				
1797							1.3559	1.0399	.6665			
1817		91 -	.0768	.0824	.2610	-2528		1.0406				
1837								1.0408				
1857		3.8						1.0566				
1877							1.4606	1.0655	.6930	.967		
1905					100		1.4605	1.0738	.6980	.973		
1925			7770	.0815	. 2652	.2552	1.4829	1.0832	.6999	.9829		
1946							1.5025	1.0894	.6996	.986		
1981							1.5404	1.1029	.7070	1.008		
2021		33.5						1.1167		1.027		
2070	3 2 1 2 3			Will be				1.1315	7279	1.056		
2120		100	.0825	.1405	.2728	. 2559		1.1486				
2174					-+-				.7574			
2324								1.1920	.7668	1.142		
2265		3 46.5			88	98 81			.7775			
2307								1.2229	.7882	1.190		
2351			.0931	.1050	.2810	-2612			.8004			
2405							7		.8133			
2453					1	CELS	1	1.2868	.8244	1.277		

Table 62. Crack Propagation Data From Side 2 - AFCG-6 (Continued)

TOTAL	CRACK PROPAGATION DATA											
LIGHTS		7				TIONS 1 THRU 10						
	0	0	3	4	(5)	6	7	8	9	10		
2505	1		100					1.3058	.8337	1.3102		
2563			.1065	.1167	.2919	.2632		1.3279	.8537	1.3517		
2607			5,000 00					1.3451	8612	1.3722		
2651			0.00					1.3633	.8744	1.407		
2690				- N - S					.8868			
2720			.1125	.1245	.2977	.2646			.8944	The same of the same		
2770									.8996			
2820									.9110			
2862			6 = 8 , 7	0.74				1.4354				
2911								1.4568				
2961			.1201	.1296	.3040	.2667		1.4761		1.6435		
3010				= 90				1.4945	-96.59			
30.58			.1265	.1400	.3113	. 2693		1.5199		A THEOREM STREET		
3105								1.5416				
3139									1.0163			
3174									1.0299			
3226			.1363	.1490	.3160	.2716		1.5918		1		
3276								1.6138				
3330									1.0999	1 2 2		
3381							7 1		1.1323			
3436			.1528	.1578	.3337	. 2757			1.1694	l abc		
3490			1014						1.1945			
3545			. best 1						1.2228			
3605									1.2666	la dec		
3655								1.7640				
3706			.1639	.1707	. 3396	.2770			1.3104			
3757						200	5.0		1.3394	61 -11		
3807								1.8182	1.3749			
38.59									1.4127			
3907			.1808	.1858	. 3533	. 2834			1.4472			
3957									1.4921			
4011						250	38 74		1.5354			
4061									1.5942			
4111			.1973	2050	.3672	2836		1	I			

Table 62. Crack Propagation Data From Side 2 - AFCG-6 (Continued)

7074	CRACK PROPAGATION DATA											
TOTAL FLIGHTS		FLAW LE	NGTH (INC	THRU 10								
	0	2	3	4	⑤	6	7	8	9	10		
4161		1		318 (31)		23				34		
4311			.2132	.2062	.3812	.3049						
4363					.3825	.3001						
4518			.2285	.2225	.4172	.2990						
4675			1.2429	.2315	.4084	.2983						
4830			.2625	.2394	.4257	.3003						
4943			.2734	.2527	4347	.2962						
5043			.2795	.2574	.4417	.3020						
5143			.2904	.2638	.4505	.3000						
5245			.2997	.2733	.4578							
5345			.3101	.2754	.4705	.3063						
5645			3421		.5493				Early.			
5732			.3622		.5076							
5833					.5205	,3095				00 5		
5933					.5293	.3124						
6067					.5483	.3138						
6175					.5641							
6325			4117		.5830	.3164						
6475			4247		.6069							
6668			4426	.4008								
6750			.4521	.4120		.3205						
6867			4658	.4249		.3200						
6997			.4832	.4405	.6938							
7150			.5014	.4625	.7250							
7302			.5200	.4858	.7537			11				
7425			.5359			. 3303						
7575						.3329						
7736			.5764			.3358						
7876			.5988		.8932							
7881					.9200							
8083					.9498							
8213					.9816							
8363			.6831			.3474				IT		
8503	8			.6646		-3490		11	1	1		

Table 62. Crack Propagation Data From Side 2 - AFCG-6 (Concluded)

	CRACK PROPAGATION DATA											
TOTAL FLIGHTS	F	The second second	GTH (INC	The second named in column 2 is not a se		THE RESERVE TO A PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	THRU 1	0				
	0	3	3	4	(5)	6	7	8	9	10		
8604	.1790		.7375	.6846		.3510		1				
87.57	.1942			.7084		.3545						
8862	.2027			.7299		.3565						
8963	.2156			7490		.3639				711		
9059	.2270			.7721		.3607						
9075	.2250			.7737						dg a		
9111	.2289			.7844								
9243	.2322			.7896						200		
9383	.2708					.3690						
9608	.2859					.3714						
9839	.3117					.3766						
10039	.3320					.3787						
10243	.3531											
10316	.3668					.3825		1				
									 			
										-		
								-		-		
										-		
										-		
								-	-	-		
										-		
								-	+	-		
					-				+			
									-	-		
										1		
				9 (C. C. S. S. S.								
								1		1		

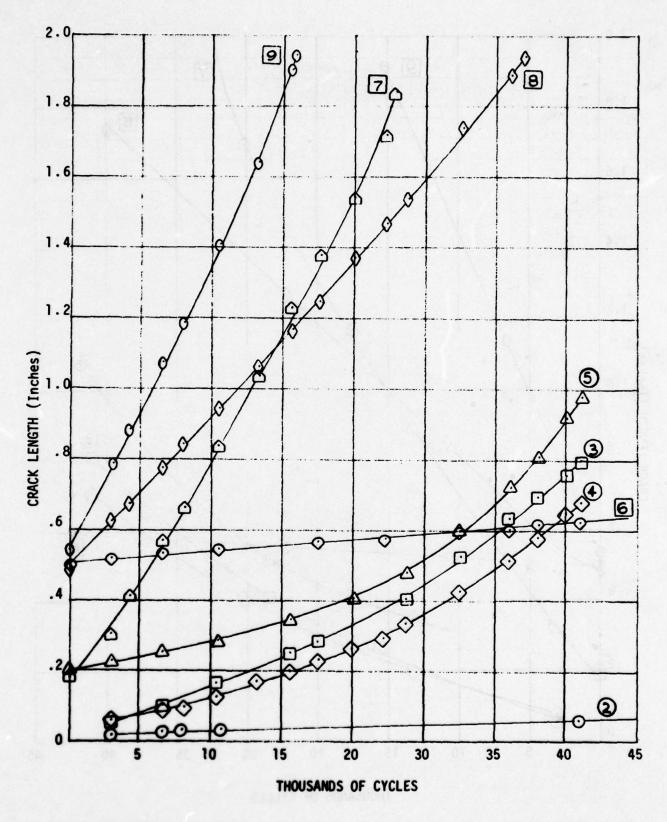


Figure 33. Crack Propagation Plot of Crack Length Vs Cycles - AFCG-1 Side 1

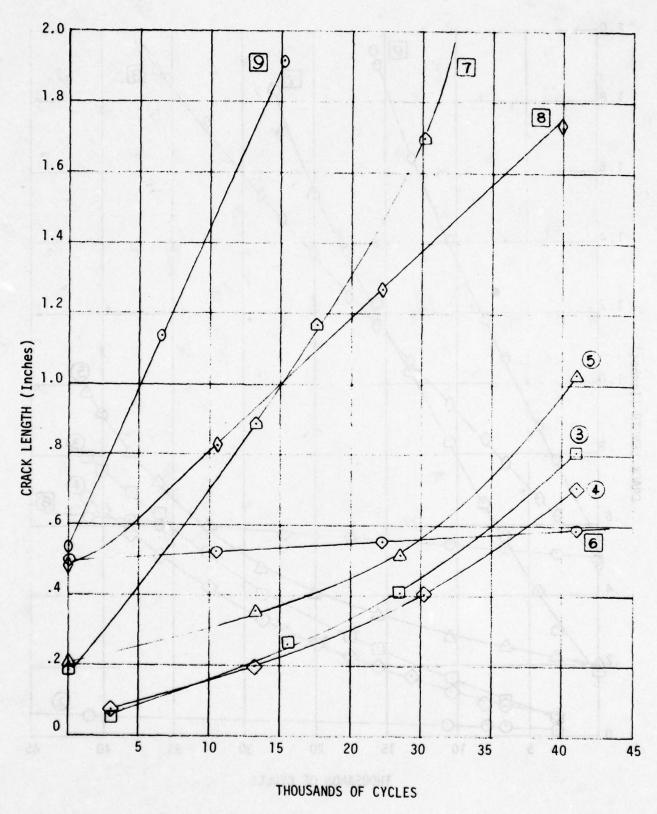


Figure 34. Crack Propagation Plot of Crack Length Vs Cycles - AFCG-1 Side 2

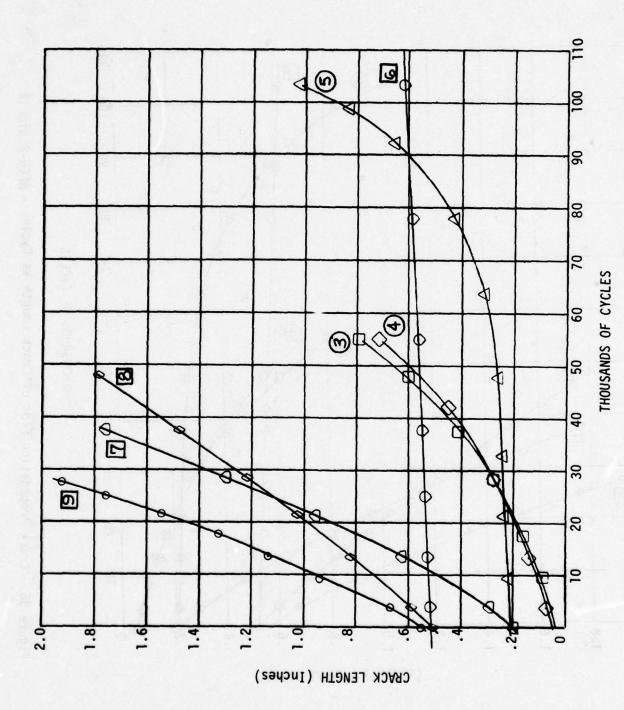


Figure 35. Crack Propagation Plot of Crack Length Vs Cycles - AFCG-2 Side 1

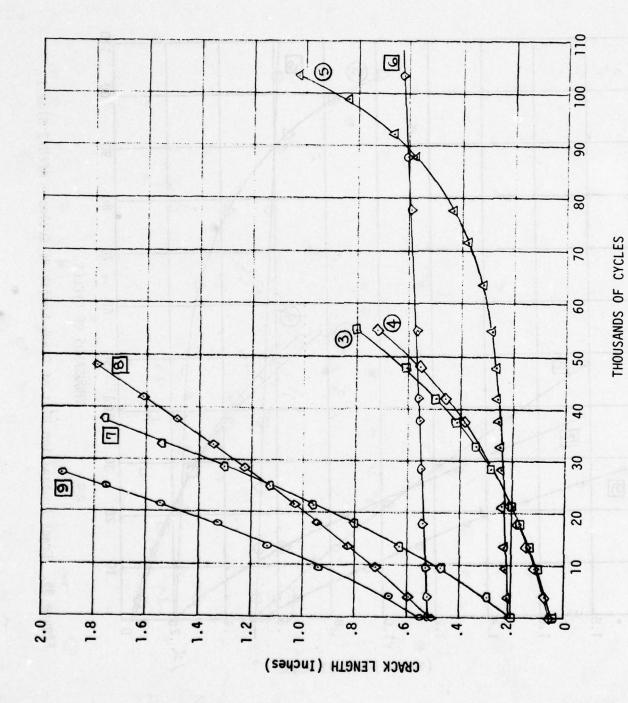


Figure 36. Crack Propagation Plot of Crack Length Vs Cycles - AFCG-2 Side 2

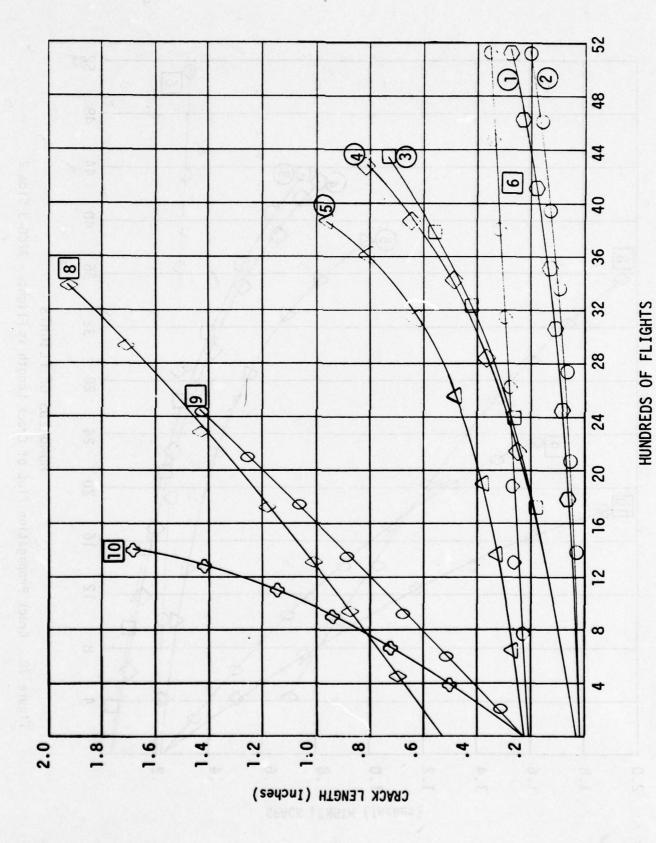


Figure 37. Crack Propagation Plot of Crack Length Vs Flights - AFCG-3 Side 1

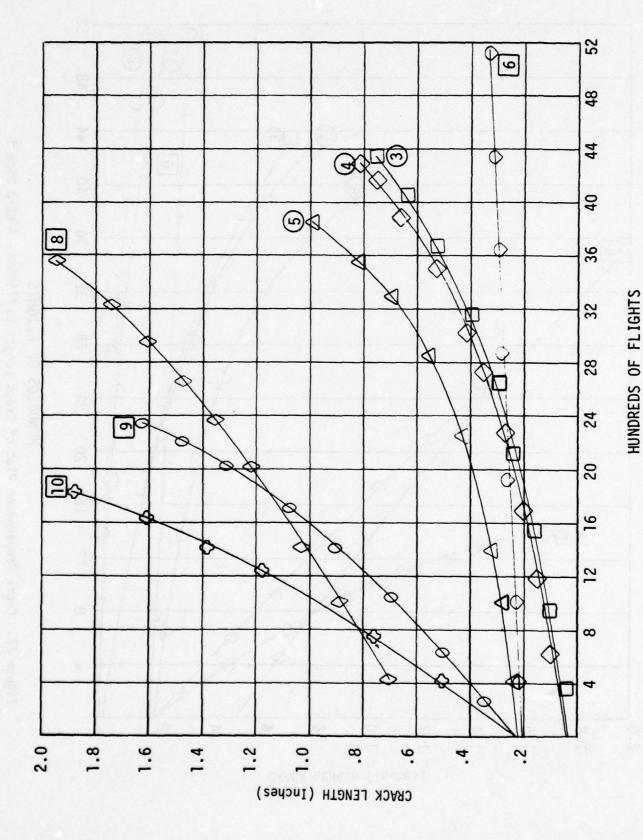
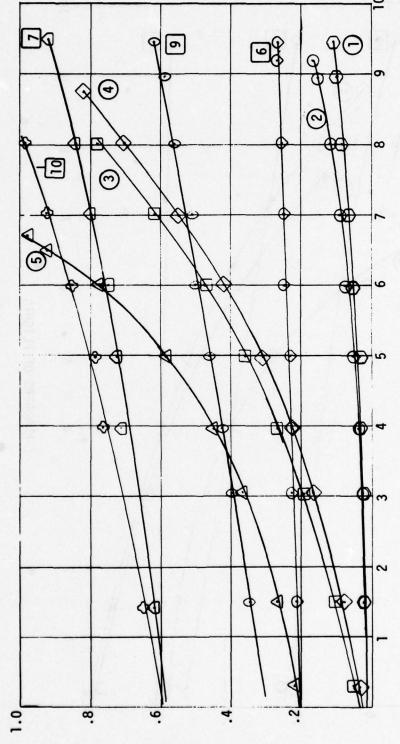


Figure 38. Crack Propagation Plot of Crack Length Vs Flights - AFCG-3 Side 2

HUNDREDS OF FLIGHTS



CRACK LENGTH (Inches)

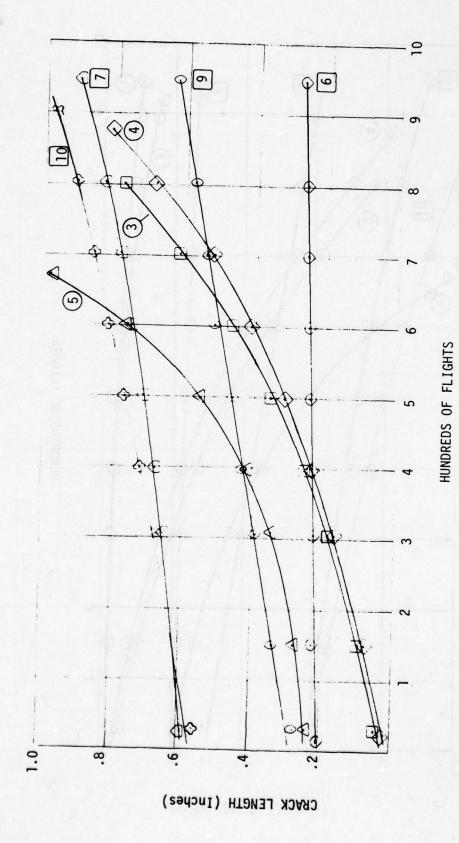


Figure 40. Crack Propagation Plot of Crack Length Vs Flights - AFCG-4 Side 2

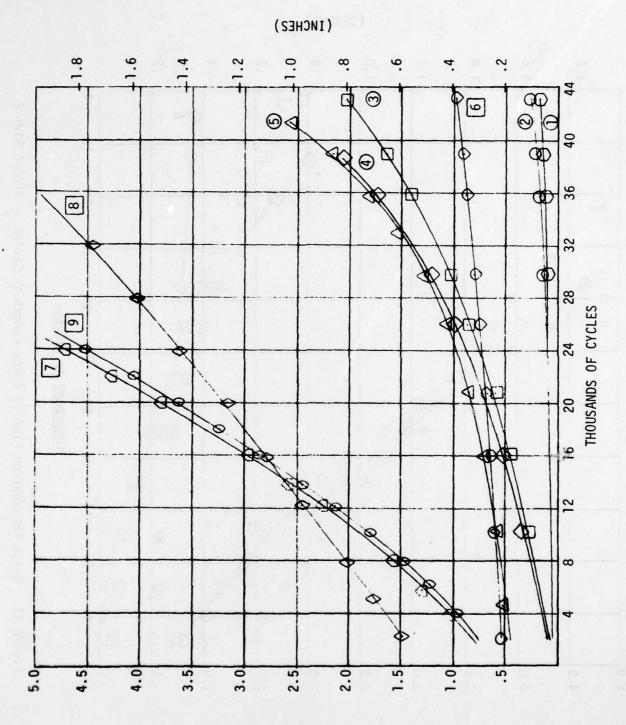


Figure 41. Crack Propagation Plot of Crack Length Vs Cycles - AFCG-5 Side 1

CRACK LENGTH (cm)

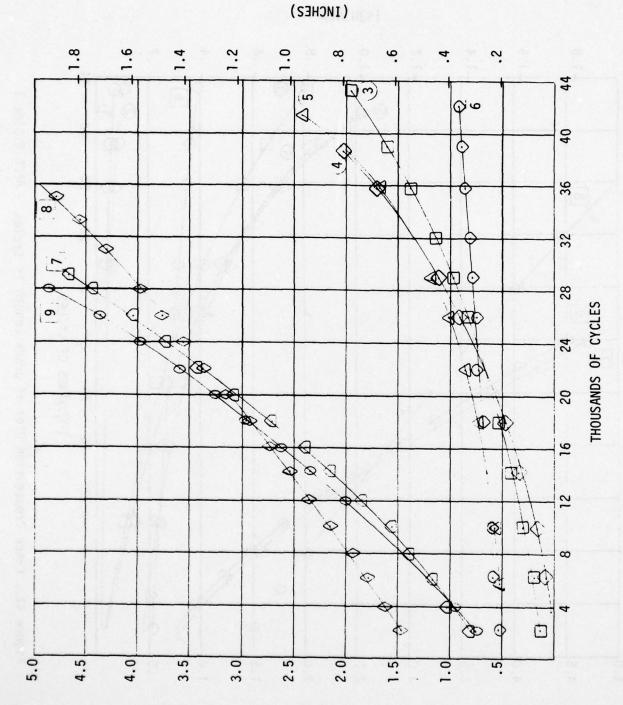


Figure 42. Crack Propagation Plot of Crack Length Vs Cycles - AFCG-5 Side 2

CRACK LENGTH (cm)

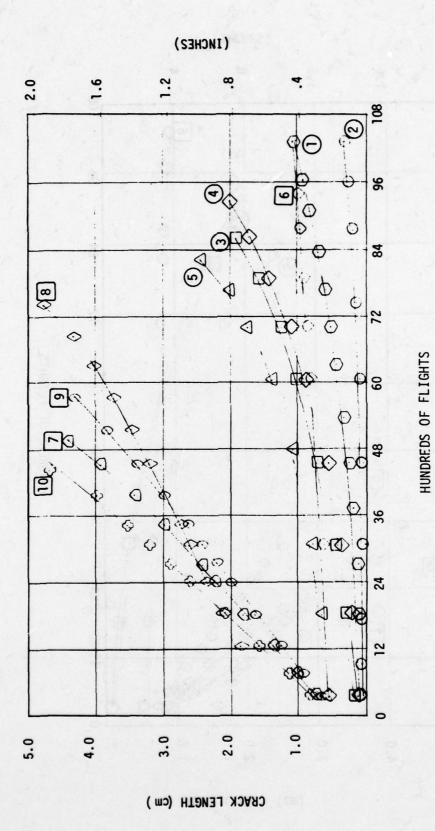


Figure 43. Crack Propagation Plot of Crack Length Vs Flights - AFCG-6 Side 1

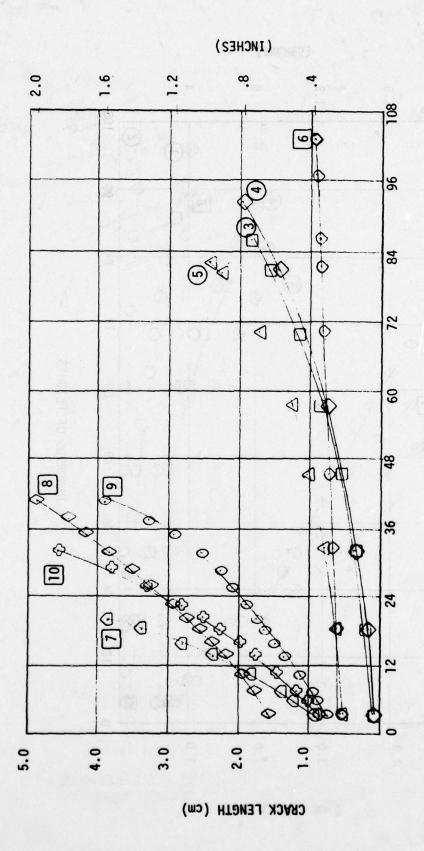


Figure 44. Crack Propagation Plot of Crack Length Vs Flights - AFCG-6 Side 2

HUNDREDS OF FLIGHTS

SECTION V

KMAX VS da/dn CALCULATIONS AND PLOTS

Printout from the computer programs which calculated and plotted $K_{\mbox{MAX}}$ vs da/dn relationships are presented in this section.

Results of K_{MAX} vs da/dn calculations for each specimen flaw are presented in Tables 63 through 89 for Specimens AFCG-1 through AFCG-6, respectively.

Log-log plots of K_{MAX} vs da/dn for the structure flaws of the six test specimens are presented in Figures 45 through 71.

REFERENCES:

Newman, J.C., Jr.; Predicting Failure of Specimens with Either Surface Cracks or Corner Cracks at Holes. NASA TN D-8244. 1976.

Boeing Document D180-22966-1; Stress Intensity Factors for Through and Part Through Cracks at Neat Filled Holes. Feb. 1978.

AFFDL-TR-74-47, Volume 1; <u>Fracture and Fatigue Crack Growth Behavior of Surface Flaws and Flaws Originating at Fastener Holes</u>. Figure 92. May 1974.

01		(3)	-		
Table 63. K _{MAX} Vs dc/dn Calculations - AFCG-1 Flaw 2		10.	989	3747	
ш.	11	1 11	N	120	
6-1	11	001	3	11	
AFC	4	ES.	#	000	
1	Ξ	5	E	異	
ions	dey	REH	AMET	HICK	
at	-	Œ	H	-	
5	Č	98	щ	ᇦ	
Cal	å	36	Ē	Ē	999
두					Ġ
dc/					11
ls (ċ
×	10	,			1
¥	ON O	í	9		å
	-1	8	9	900	ď
63.	500	S W	Ġ	90.	=
a	生品	12	11	4	Ž
ab	1 5	3	9.0	11	3
-	2	ພິ	OHI	÷	10
	w !	38	_	DI	9
	(F)	RA-	ER	=	93
	00	00	Z	-	3

	wa Ch. nankistia da 📦 w	
7,3-80	TES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(D2C/DN) B=1,SINGLE CRACK MITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)T DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2	
HOLE DIAMETER,D= 0.2630 PANEL THICKNESS,T= 0.3747 00	DIES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(D2C/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)T DIRECCHALF LENGTH OF CORNER CRACK OR LENGTH OF CORNER CFILLED HOLE CORRECTIONS APPLIED ONLY IF E=2	
த்_ட்	5 222	
8.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	HREE CONTRACTOR CONTRA	
ETE ICKN	CRACE CRACE CRACE CRACE	
H H		
OLE PAREL B	CONTRACTOR OF THE CONTRACTOR O	
¥ 2 0	SH. THE CRACK CRAC	
11	88.00 8.00 8.00 8.00 8.00 8.00 8.00 8.0	
10,	ACK AND CONT TIND CONT TO CONT	
B RH.	A PACA SERVICE OF THE	
86.68 86.68 ULAS	A C C C C C C C C C C C C C C C C C C C	
# 4.0 ₩		
HD. F	TES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA E=3,FOR CORNER CRACK(S),FHSTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION— B=1,SINGLE CRACK NITHIN THE FASTENER HOLE— B=2,TWO CRACKS WITHIN THE FASTENER HOLE— A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S) C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2	
R_LOAD,P= 0.000 IDTH,W= 4.0000 R/PLATE MODULAS RATIO,R= 0.000		

DC/DH	7.2222E-07	7.1429E-87 8.9286E-87	6.7308E-07	8.06456-07	9.09096-07	1.5000E-06	1.9167E-06	3.1800E-06	3.6667E-06	4.0417E-06	4.2917E-06	4.6429E-06	4.7727E-06	5.3333E-06	6.0625E-06	6.4583E-06	6.3636E-06	7.1875E-86	7.2727E-06	7.3125E-06	8.8000E-06	7.0000E-06
AVG KMAX	4.823	4.4. 00.0. 00.00.	5.009	5,189	314	5.396	5.592	5.824	5.938	6.011	6.096	6.185	6.269	6.346	6.415	6.488	6.579	6.638	6.712	6.789	6.850	6.90c
KMAX 4.782	4.865	4.4 0.0 0.00 0.00	5.053	5,164 5,000	0.00 0.00 0.00	5.444	5.741	5.907	5.969	6.054	6.137	6.233	6.305	6.386	6.444	6.532	6.608	6.669	6.756	6.823	6.878	6.935
DC	2.6000E-03	1.8000E-03	3.5000E-03	5.0000E-03	4.0000E-03	6.0000E-03	2.3000E-02	1.5900E-02	6.6000E-03	9.7000E-03	1.0300E-02	1.3000E-02	1.0500E-02	1.2800E-02	9.7000E-03	1.5500E-02	1.4000E-02	1.1500E-02	1.6000E-02	1.1700E-02	8.8000E-03	7.0000E-03
ດ 0.0 294	B.8328	6.6355	0.6396	6.6446 6566	6.6546	0.0600	0.0830	6860.0	6.1055	0.1152	0.1255	0.1385	0.1490								0.2490	
ВВ	2.6999E-93	1.8888E-83 2.5888E-83	3.5000E-03	5.0000E-03	4.0000E-03	6.0000E-03	2.3000E-02	1.5900E-02	6.6000E-03	9.7000E-03	1.0300E-02	1.3000E-02	1.0500E-02	1.2800E-02	9.7000E-03	1.5500E-02	1.4000E-02	1.1500E-02	1.6000E-02	1.1700E-02	8.8000E-03	7.9000E-03
я 6.6294	6.6326	6.6355	0.0390	0.0 0.0 440 0.00	6.6546	0.0600	0.0830	6860.0	0.1055	0.1152	0.1255	0.1385	0.1490	.1618	.1715	.1870	.2010	.2125	.2285	.2402	0.2490	.2569
Ä	3688	2800	5200	6200 5400	4400	4666	12000	5666	1866	2400	2400	2800	2200	2400	1600	2400	2200	1600	2200	1600	1666	1000
CYCLES	6699	10800	16999	22200	32000	36000	48000	53666	54800	57200	59600	62400	64600	62000	68699	71999	73200	74800	27866	78600	29699	80600

Table 64. KMAX Vs dc/dn Calculations - AFCG-1 Flaw 3

	10.018		r~	
~J		3570	0.374	
JDE , E=	TRESS:	3 = D + S	11 4391	
TYPE C	AREA S	IAMETE	"ANEL THICKNESS, T= 0.3747	
CRACK	GROSS AREA STRESS, S=	HOLE DIAMETER, D= 8 3578	PANEL	999
				⊕
<u>т.</u>	-	9		FASTENER/PLATE MODULAS RATIO, R= 0.000
IES, M=	HOLE, B=	FASTENER LOAD, P= 0.000	4.6666	MODULAS
ENTR	NI S	LOHD, F	HM *HLO	PLATE
F	Ť		14	-3
# OF CYCLE ENTRIES,M= 13	OF CRACK	RETENER	HAEL MII	ASTENER.

MIDTH,W= 4.0000 WIDTH,W= 4.0000 WIDTH,W= 4.0000 PRNEL THICKNESS,T= 0.3747 NOTES: NOTES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(D2C/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(D2C/DN) B=2,TNO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) R=2,TNO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) R=26-THO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CHACK S)

		0	.3167E-0	.3333E-0	.4286E-0	.4542E-0	.6187E-8	.7083E-0	.8000E-0	.9667E-0	.0818E-0	.4833E-0	.6778E	.8292E-0	.9147E-0	.3500E-0	. 4000E-0	45BBE-B	7000E-0	100E-0
AVG	KMAX		(0)	5	88.	0.18	0.5E	96.B	1.16	1.40	1.69	1.91	12.133	N. 46	10.0V	0.00	3.61	3.85	4.17	4.40
KMAX		0	9	.77	0.00	0.36	0.75	1.05	1.28	1.56	1.83	1.99	12.269	2.66	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.00 0	0.00	3.98	4. NOI	प्रतास च
	DC		.5800E-0	. 2000E-0	. BOBBE-B	. 4900E-0	. 5180E-B	. 1000E-0	, 6000E-0	.7200E-0	. 5800E-0	. 9800E-B	4.8200E-02	. 7900E-0	. 9100E-0	. 3500E-0	. 4666E-B	450BE-B	. 7000F-0	.770BE-0
0		.06	· 67	. 10	12	.16	. 20	. NO	. NO	000	0	40	0.4570	00.	.60	(O)	69.	CI F-	92.	. S
	当		. ២២២២E+២	. быбыЕ+ы	. BBBBE+B	. BBBBE+B	. ២២២២E+២	. өөөөөЕ+ө	. OBBOBE+B	. BBBBE+B	. BEBBE+B	. មាមមាមE+មា	0. ២២២២E+២២	. GBBBE+B		. BBBBBE+B	. BBBBE+B	. ติติติติตE+ติ	. ӨӨӨӨЕ+Ө	. BBBBE+B
Œ		0	0	60	60	8	6	8	6	8	8	0	0.3750	00	0	9	37	8	32	33
	H		OUL	-	7	77	100	4	150	77	17.1	N	1800	7	7	150	150	120	1666	1666
CYCLES		3666	4200	6600	8666		00	117	1-	1		10	25200	1-	++	CA	177	4	117	T
#			ou.	0	7	n	o	r-	00	gr:	0	+-1	ou	00	4	47	10	1-	00	(T)

Table 65. K_{MAX} Vs dc/dn Calculations - AFCG-1 Flaw 4

	CRACK TYPE CODE, E= 2	GROSS AREA STRESS, = 10.018	HOLE DIAMETER, D= 0.3570	PANEL THICKNESS, T= 0.3750	: MODULAS RATIO,R= 0.000
TEST CASE ID AFCG-1 F4	# OF CYCLE ENTRIES, M= 19	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P = 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS R

E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION--(D2C/DN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE--(DC/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE--(D2C/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)--T DIRECTION
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

	9	.9167E-0	1.0583E-05	.1214E-0	.1667E-0	.3250E-0	.4375E-0	.5200E-0	.5833E-0	.7273E-0	.7167E-0	.8556E-0	.9750E-0	.5029E-0	.9500E-0	.2000E-0	.3000E-0	000E-0	.1000E-0
A NO		φ.	7.497	47	66.	98.	0.04	0.38	69.	96.0	. 18	1.35	1.60	1.98	2.31	2.49	1.69	90	3.18
KMAX	8	.75	8.242	. 70	80	40.	4	0.53	0.84	.12	1.25	1.46	1.74	2.23	. 40	2.59	6.	89	. 28
20		.1900E-0	2.5400E-02	.5700E-0	. 8000E-0	.7100E-0	.4500E-0	.0460E-0	.8000E-0	. 8000E-0	. 0600E-0	.3400E-0	.7400E-0	.5100E-0	.9500E-0	.2000E-0	.3000E-0	.7888E-8	.2000E-0
ပ	.008	. 020	0.0455	.061	.089	.126	.160	191	.229	.267	.287	.321	.368	.453	.483	.515	.548	.585	.627
H	•	. BBBBE+B	0.0000E+00	. BBBBE+B	. 0000E+0	. BBBBE+B	. 0000E+0	. BBBBE+B	. BBBBE+B	. BBBBE+B	. 0000E+0	. 0000E+0	. 0000E+0	. BBBBE+B	. BBBBE+B	. BBBBE+B	. 0000E+0	. BBBBE+B	.0000E+0
σ	37	37	0.3750	.37	34	.37	.37	33	37	.37	.37	37	37	37	.37	33	.37	.37	.37
Z		1200	2400	1400	2400	2800	2400	2000	2400	2200	1200	1800	2400	3400	1999	1999	1000	1000	1666
CYCLES	3888	4266	6699	8000	16466	13200	15699	17600	20000	22200	23400	25200	27699	31000	32000	33666	34000	35868	36999
									_	_				-	1			-	-

-თი4ობ<u>ითან-თი4ობ</u>ნა

Table 66. K_{MAX} Vs d2c/dn Calculations - AFCG-1 Flaw 5

			D2C/DN .4167E-0	.7917E-0	.0417E-0	.2568E-8	.5005E-0.	.9773E-0 .1167E-0	2833E-7500E-	.4794E-8	.9700E-0	8-300£8.
818	TION RACK(S)	PV C	6.221	94	014	1 7 0	000	4 r-	აბ მი 0 4	(V (S	900	400
= 1 5 = 10. 6.3000 = 9.3747	STRESS (D2C/BN) DC/BN) C/BN) -T DIREC CORNER C	КМЯХ	6.159	900	0.0	400 C	000	₩₩ ₩₩	200	(0 M	700	— ტ დ 4
TYPE CODE,E RREA STRESS DIAMETER,D= THICKNESS,T	KNESS CRACK R GROSS AREA ND E=3 NFIGURATION TENER HOLEC NER CRACK(S)- OR LENGTH OF ONLY IF E=2	Jou	.0100E-0	.1100E-0	.5000E-0	. 00000. 70000T-0	.8800E-0	.3500E-0 .5400E-0	4.1100E-02 6.6000E-02	.1830E-0	.9700E-0	700E-0 300E-0
CRACK GROSS HOLE PANEL	TREEDER TRE	0	6.1154 6.1265	131	150	1001	214	ი ი ი	.382	.361		44 700 200
-1 1= FS BB BB 900	FACE OR THROUNER CRACK(S), D LOAD CASE O OR THROUGH C CRACK WITHIN CKS WITHIN SURFACE CRACK TH OF SURFACE	Ē	0.0000E+0	0.0000E+0	6.8888E+8	6.0000E+0	9.8888E+8	0.8999E+9	ଡ.ଡଡଡେଟ+ଡଡ ଡ.ଡଡଡେଟ+ଡଡ	0.0000E+0	0.0000E+0	6.8888E+6
NTRIES,M IN HOLE, D,P= 0.99	FOR FOR FOR FOR CORN SURPRICE SURPRICE FTH OFF FOR FOR FOR FOR FOR FOR FOR FOR FOR	Œ	6.3759 6.3759	375	375	3750	.375	.375	375	.375	375	.375
CASE ID- CYCLE EN CRACKS I NER LORI WIDTH, N	N E E E E E E E E E E E E E E E E E E E	Z	20	24	200	$\frac{4}{2}$	94	0 0 0 0	1899 2499	200	000	2 2
F##T PASTEN		CYCLES	3888 4288	99	949	766 766 766	999	228 348	88	166	400	200 600

-0040000000000400000

Table 67. K_{MAX} Vs dc/dn Calculations - AFCG-2 Flaw 3

TEST CASE ID AFCG-2 F3	
# OF CYCLE ENTRIES,M= 20	CRACK TYPE CODE, E= 2
# OF CRACKS IN HOLE, B= 1	GROSS AREA STRESS,S≠ 10.018
FASTENER LOAD, P = 0.000	HOLE DIAMETER, D= 0.3312
PANEL WIDTH, W= 4.0000	PANEL THICKNESS, T= 0.3747
FASTENER/PLATE MODULAS RATIO, R= 0.000	0.000

E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION--(D2C/DN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE--(D2C/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)--T DIRECTION
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

		(2)	(2)	0	(2)	90	\odot	(2)	O	(2)	\odot	\odot	\odot	(2)	(2)	(2)	(2)	50	50	50
	3	8	10	CU	8	-3660	00	10	10	(0)	CU	8	1-	10	10	8	8	3	8	1
	4	(3)	10	9	00	8.86	<u>ت</u>	1.05	1.16	1.00	4	6	r-	Ø,	00	***	-	4	N	1.97
×		- N	io N	SS	90	90	98	CM CM	(O)	OJ OD	90	40	on m	च च	CU LO	00	r- m	ø,	15	43
KMNX		00	(<u>S</u>)	-	J.	ф. Ф	(J	(D)	. J	₩.	 	m.	0.	(J	()	01	(-)	3.0	3.4	è
	010	Ø	寸	-	(3)	070	00	IO.	OJ	O	10	-	W.	Oil	O.	-	U)	寸	P-	-
		ď				10.	ø	·	S		-			oj		oi	oi		0	
		(2)	9	1	9	E-02	9	9	5	9	9	9	9	9	9	9	9	1	9	(2)
DC		8	99	150	96	7000	0	88	8	8	8	20	9	58	56	99	4	9	10	(3)
	(2)	-				න ශ														
	.041	. 658	. 068	. 693	.126	.163	.200	.238	.280	.336	.370	.418	.461	.489	.535	.586	.608	.665	.727	. 798
	3	(2)	(2)	(2)	(Z)	ଜ ଜନ	(E)	(Z)	(Z)	(Z)	(2)	(Z)	(Z)	(2)	(Z)	(Z)	(Z)	(2)	(Z)	(Z)
Œ		+	+	+	+	BBBE+6	+	+	+3	+ 1	+3	+	+ 3	+	+	+	+	+	+	+
DA		(Z)	<u>.</u>	७.	9	0.00	७.	⊕.	ø.	9	9	<u>a</u>	·	3	₾.	Ø	0	<u>.</u>	0	2
	3	2	2	2	23	8228	2	2	2	2	23	3	23	2	2	2	23	23	13	13
						6.9														
DE		3400	1866	3600	4200	4200	3600	3600	3600	4200	2400	3000	2400	1400	2400	2400	1888	2400	2400	2400
	500	999	୍ ପର	400	9999	.800	400	996	999	800	500	500	999	999	400	800	800	500	999	999
	•	4	Š	ď	136	178	21.	250	286	328	325	380	400	426	44	468	478	505	526	556

-0048067800010048047800

Œ

CYCLES

Table 68. K_{MAX} Vs dc/dn Calculations - AFCG-2 Flaw 4

	CRACK TYPE CODE,E= 2	GROSS AREA STRESS, 3= 10.018	HOLE DIAMETER, D= 0.3312	PANEL THICKNESS,T= 0.3747	0.600
1531 CH3E 11 HTCG-2 F4	# OF CYCLE ENTRIES, M= 20	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P = 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO, R= 0.000

RACKS IN HOLE,B= 1 LER LOAD,P= 0.000 MIDTH,W= 4.0000 ER/PLATE MODULAS RATIO,R= 0.000	DIES: E=1.FOR SURFACE OR THROUGH THICKNESS CRACK E=2.FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3.FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=4.COMBINED LOAD CASE OF E=2 AND E=3 B=0.SURFACE OR THROUGH CRACK CONFIGURATION(D2C/DN) B=1.SINGLE CRACK WITHIN THE FASTENER HOLE(D2C/DN) B=2.TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)T DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CURNER CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2
RACKS IN ER LOAD,P WIDTH,W= ER/PLATE	NOTES: E=1.70 E=2.70 E=4.00 B=1.51 B=1.51 C=HBLEPTH FILLED

	1	. BBBBE-B	.5000E-0	.6667E-0		.2143E-0	.6111E-0	.4444E-0	.0333E-0	.1738E-0	.3333E-0	3633E-0	4833E-0	.6571E-0	.5333E-0	.8417E-0	.7800E-0	.0625E-0	917E-8	.4833E-8	
A A C G		64.	. B.	00	0000°	00.	0.23	0.48	0. J	BB.	1.24	1.44	1.66	0	S 60	SN . S	4	63	96	34	
KMAX	8	40.	.11	04.	9.764	0.10	98.	0.61	0.85	1.15	1.33	1.56	1.76	1.00	2.10	2.36	N. 47	₩.√3	3.13	4	
DC		. 7000E-0	. SØØØE-Ø	. 4000E-0	3.1500E-02	.4500E-0	. 1000E-0	. 4000E-0	.7200E-0	.9300E-0	. 2000E-0	. МЭВВЕ-В	.5600E-0	,3200E-0	.6800E-0	.4200E-0	.7800E-0	. 9500E-0	. 2600E-0	.9600E-0	
o .	040	. 066	.076	.168	0.1315	.166	.197	. 231	.268	.317	m + 0 .	900.	.426	044.	.486	. 53B	. U40	.597	.65B	.709	
DA		. ติดิติติธิ+ติ	. BBBBE+B	. BBBBE+B	0. មិចិចិចិE+ចិចិ	. GBBBE+B	. BBBBE+E	. BBBBBE+B	. BBBBE+B	. GBBBE+B	. BBBBE+B	. BBBBE+B	. BBBBE+B	. BBBBE+B	. ӨӨӨӨЕ+Ө	. OBBBE+B	. BBBBE+B	. BBBBE+B	. BBBBE+B	. ӨӨӨӨЕ+Ө	
Œ	375	.375	.375	.370	0.3750	.375	.375	.375	.375	.375	.375	.375	.375	.375	.375	.375	.375	.375	.375	.375	
3		9	00	99	4200	0	99	99	99	8	4	0	日	4	S T	94	00	4	4	40	
CYCLES	699	(3)	00	4	13600	00	7	56	9	8	80	8	90	20	4	68	200	8	0	50	
#	-	e4	m	4	ريا ريا	w	1-	00	g,		11										

				2/2	.9412E-6	.8889E-0	.5238E-0	.5556E-0	.6667E-0	. ପ୍ରସ୍ତ୍ର - ଜ କ୍ଷ୍ୟର	. 3238E-8 . 2508E-0	.3333E-0	.6667E-0 4286E-0	.7241E-0	.2917E-0	.5795E-0	.7500E-0	.2074E-0	.6087E-0	.9077E-0	. 1007E-0 . 8359E-0	.711 SE-0	4.3333E.05 4.8625E-05
. 5	.018	CTION	AUG		99	00	© 0 ⊘ 0) (Z)) 4	20	4	0 (Z) - (Z) (-	전 ((V) (n e N e	4	$^{N}_{0}$	8	40	- d	(A)	in α	70	72	12.226
AFCG-2 Flaw	E= 1 S.S= 10 0.0000 T= 0.374	- CDSC/DN CDC/DN) CDC/IN) COC/IN) T DIRE	КМЯХ	9	<u>.</u>	00	<u>ක</u> ශ්ර	96	9.	ლ. ლ.		200	И 4	46	ი ს ი ს	19	യോഗ	960	98.	 	ეტ შ	8	12.399 12.652
Calculations - AF	K TYPE CODE, S AREA STRES DIAMETER,D= L THICKNESS,	CKNESS CRACK RM GROSS AREA AND E=3 CONFIGURATION- ISTENER HOLE ENER HOLE ENER CRACK(S) CON LENGTH OF	D 2C		. ପ୍ରତ୍ରତ୍ତମ - ପ୍ରତ୍ରତ୍ତମ + ପ	.4000E-0	. ପ୍ରସ୍ଥମନ୍ତ . ଜନ୍ମନ୍ତନ୍ତ	.0000E-0	.4000E-0	.6000E-0	. 0000E-0	. GOODE - O	. 88888E-8	.0000E-0	. 1888E-8	.1500E-0	.6000E-0	.5200E-0	. 4000E-0	.9600E-0 9400E-0	.8150E-0	.6500E-0	5.2000E-02 3.8900E-02
d2c/dn Calc	CRAC GROS HOLE PANE	CRACK CRACK	٥	.109	169	.110	110	1111	.112	4114	.118	.120	122	128	138	.152	.175	234	.271	. 290 0.00 0.00	. 486	454	മ. 48 മ. 58 ഉള്ള ഉള്ള
. KMAX VS	7.2 7.8 7.8 9.0 9.0 9.0 9.0 9.0 9.0 9.0 9.0	R CRACKS R CRACKS LOAD CASE THROUGH BCK WITHIN S WITHIN OF SURFA	Æ		. 8888E+8	. 9999E+9	. 00000E+0	. 0000E+0	.0000E+0	. 8888E+8	.0000E+0	. 0000E+0	. BUBBE + B	. 0000E+0	. BBBBE+B	. 0000E+0	. ଉପସେପ୍ୟ-ପ ଜନ୍ମନ	. 0000E+0	. 0000E+0	. 0000E+0	. 0000E+0	. 0000E+0	6.6666E+66
Table 69	ATRIES, NTRIES, IN HOLE 0,P= 0	FOR CORP SOURTHONNER SOURTHONNER FOR CORRE SOURTHONNER FOR CRACK FOR CR	Œ	.375	.375	.375	.375	375	.375	375	375	.375	375	375	375	375	.375	375	.375	.375	375	.375	6.3756 6.3756
	CYCLE ENCRECKS CRACKS ENER LOH		Ä		(Z) (Z	3 (2)	00 C	30	69	90	34	00	4 4 2 2	80	20 4 20 2	80	900	14	69	20 0	04	69	1200 800
	1 # # 1 ES T		CYCLES	(3)	ପ୍ର ପ୍ର	040	36 0	- 	500	800 800 800 800 800 800 800 800 800 800	200 100 100 100 100 100 100 100 100 100	828	0 0 0 0 0 0	789	200 200 300	388	186	0 0 0 4 0 0	899	969	900 000 000	0140	102600 103400
			#	-	c) c	9 4	יי מו	01	00														282

-
Flaw
AFCG-3
Calculations
5
Ca
dc/dn
dc/
٧s
K _{MA}
70.
Table

MAA	FCG-3 F1	~	OLE,B= 1 GROSS AREA STRESS,S:	E DIAMETER, D=	PANEL WIDTH,W= 4.0000 PANEL THICKNESS,T= 0.3750	
	CASE ID A	# OF CYCLE ENTRIES,M= 28	CRACKS IN H	ENER LOAD, P=	PANEL WIDTH, W=	MA THOUGH OFFICE

E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION——(D2C/DN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE——(DC/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE——(DC/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)——T DIRECTION
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(C)
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

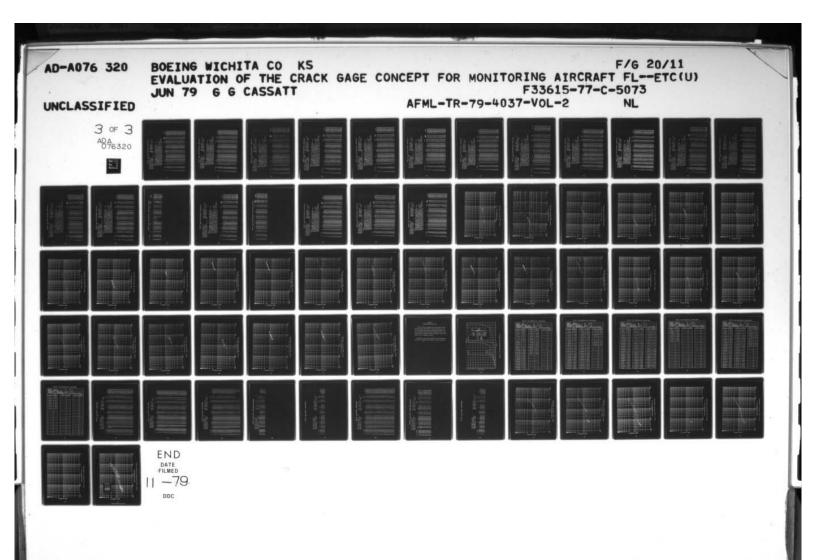
ng/Ju	14596-	1.8433E-05	9151E-	-3060G	6154E-	8571E-	5381E-	4483E-	3842E-	0552E-	5802E-	1000E-	3147E-	-92999	-3826 9	-BBBBB	0149E-	4054E-	1818E-	0400E-	0110E-	4340E-	1216E-	0616E-			
Aug		7.617																			-		-				
E .	7.429																										
DC	. BBBBE-	4.0000E-03	-30006.	. BBBBE-	.1000E-	. 0000E-	.0000E-	.1000E-	.9000E-	.9100E-	.2000E-	.0400E-	- GOOGE-	.0200E-	.4800E-	-6000E-	.4000E-	. 0000E-	.0000E-	.8000E-	.2000E-	. 99996 -	.7000E-	.5500E-		.1800E-	.5500E-
	0.0200																										
ΡŪ	. BBBBE-B	4.0000E-03	.9000E-0	. 0000E-0	. 1000E-0	. 0000E-0	. 0000E-0	. 1000E-0	.9000E-0	.9100E-0	.2000E-0	.0400E-0	Ģ	.0200E-0	.4800E-0	.6000E-0	. 4000E-0	.0000E-0	.0000E-0	.8888E-8	.2000E-0	. 0000E-0	.7888E-8	.5500E-0	Ġ.	.1800E-0	$\overline{\Omega}$
	0.0200																				•						
Ä	233	217	271	279	195	210	197	319	203	471	262	200	143	180	260	000	134	111	119	125	91	က္	296	146	100	110	154
CYCLES	233	450	721	1666	1195	1405	1662	1921	2124	2595	2857	3857	3266	3380	3640	3720	3854	3962	4075	4200	4291	4344	4640	4786	4886	4996	5150

Flaw	
AFCG-3 Flaw	
1	
Vs dc/dn Calculations	
dc/dn	
Vs	
K _{MAX}	64 6
rable 71.	AFCC-
Table	CASE IN AFPER-3 FO
	PASE

	CRACK TYPE CODE,E= 2	GROSS AREA STRESS, S= 16.230	E DIAMETER, D= 0.297	PANEL THICKNESS, T= 0.37	ମ.୭= ଜ ଜନ୍ନ
TEST CASE ID AFCG-3 F2	# OF CYCLE ENTRIES,M= 26	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P = 0.000 HOL	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MOTILI DS PATI

IR LOAD,P = 0.000 HOLE DIAMETER,D = 0.2970
IDTH,W = 4.0000 PANEL THICKNESS,T = 0.3750
IRZPLATE MODULAS RATIO,R = 0.000 PANEL THICKNESS,T = 0.3750
OTES:
E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), FASTENER LOAD ONLY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION - (D2C/DN)
B=1,SINGLE CRACK MITHIN THE FASTENER HOLE - (D2C/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE - (D2C/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE - (D2C/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S) + T DIRECTION
C=HRLF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

	DC/DN	.0616E-	.0204E-	.0753E-	2.0513E-05	.5238E-	.0305E-	.5078E-	.6316E-	.8627E-	.3471E-	.3949E-	.5000E-	.8951E-	.2778E-	.1279E-	.2857E-	.6418E~	.8649E-	.6995E-	.6643E-	.7736E-	.0811E-	.0976E-	45456	.8779E
A A A	· · · · · · · · · · · · · · · · · · ·	Ψ.	00	0	8.171	0	4	Φ.	σ.	O.	4	w.	1-	ω.	σ.	-:	(V)	ල ල	7.	n.	10	vo.	٢-	σ.	0	11.142
КМЯХ	4	73	.87	. 96	8.289	. 37	.55	8.	.00	3	1989	.64	8.	ee.	.06	0.17	0.27	0.39	0.46	.57	9.66	69.6	88.0	1.03	9.	.19
ji L		. 1000E-0	. OBBOBE-B	. BBBBE-B	4.0000E-03	. BBBBBE-B	. OBBOBE-B	. BBBBE-B	. OBBBE-B	. 0000E-0	. 1000E-0	. 9000E-0	. 0000E-0	. OBGOBE-0	.7000E-0	. 1000E-0	.2000E-0	. 9000E-0	.4000E-0	.6000E-0	. 1000E-0	. OBBBE-B	.8000E-0	.5000E-0	. BBBBE-B	.0900E-0
Ú	. 82	68.	. 02	. 83	0.0340	B3	40.	40.	B	90.	. 67	9.	89.	9	.10	. 11	.11	.12	.13	4.1.	4.	.15	.16	. 100	.19	. 20
Œ	.0219	.0250 3.1000E-0	.0270 2.0000E-0	. 0300 3.0000E-0	0.0340 4.0000E-03	.0360 2.0000E-0	. ଓ4ଓଡ 4. ଓଡ଼ଜଣ=-ଜ	.0480 8.0000E-0	.0560 8.0000E-0	.0650 9.0000E-0	.0731 8.1000E-U	.0800 6.9000E-0	.0890 9.0000E-0	.0960 7.0000E-0	.1037 7.7000E-0	.1108 7.1000E-0	.1180 7.2000E-0	.1269 8.9000E-0	.1323 5.4000E-0	.1409 8.6000E-0	.1490 8.1000E-0	.1510 2.0000E-0	.1690 1.8000E-0	.1840 1.5000E-0	.1900 6.0000E-0	.2009 1.0900E-0
N		O.	$\sigma_{\rm i}$	r-	195	7-4	σ_{γ}	-	\odot	00	4	n.	∇	v.	∞	r-	ø	134	111	183	143	က္က	Œ,	246	-	100
CYCLES	(1)	OI	W	0	1195	9	99	3	Q.	4 0	20	8	8	20	8	2	2	88	96	4	8	46	49	88	8	5
*	-	N	ო	4	n	ø	۲-	σ	σ	10	11	12	13	14	15	16	17	18	19	20	21	22	53	24	25	56



Flaw
AFCG-3 F
1
Calculations
dc/dn
٧s
K MAX
72.
Table

	CRACK TYPE CODE, E= ∃	GROSS AREA STRESS, = 16.230	HOLE DIAMETER, D= 0.3218	PANEL THICKNESS, T= 0.3750	ତ. ଉପ୍ତ
LEST CHSE ILT HFCG-8 FG	# OF CYCLE ENTRIES,M= 27	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P= 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO,R= 0.000

NOTES:
E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION—(L2C/DN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE—(DC/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE—(D2C/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)—T DIRECTION
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

DC/DN	Water State of the		7.9096E-05	8.444E-05	8.4906E-05	9.1503E-05	9.1282E-05	1.0095E-04	1.0660E-04	1.1416E-04	1.2808E-04	1.2935E-04	1.4163E-04	1.5328E-04	1.6412E-04	1.8200E-04	2.0629E-04	2,1444E-04	2.4128E-04	2.5000E-04	2.3750E-04	3.0896E-04	2.8406E-04	3.2174E-04	3.3636E-04	3.8043E-04	3.7255E-04	3.96235-04
Ave	XWXX		13,465	14.052	14.587	14.981	15,320	15.687	16.039	16.376	16.709	17.015	17,332	17.607	17.914	18.287	18.593	18.910	19.289	19.594	19.796	20,099	20.411	20,709	21.110	21.514	21.815	22.062
XMMX		13,180	13,750	14.353	14.822	15,140	15.500	15,875	16.203	16.549	16.869	17.161	17.584	17.710	18,118	18,456	18.730	19.091	19,487	19.702	19.889	20,369	20.512	20.986	21.314	21.713	21.936	32,187
	BC		-		1.8000E-02	_	1.7800E-02	2.1200E-02	2.1000E-02	2.5000E-02	2.6000E-02	2.6000E-02	3.3000E-02	2.1000E-02	4.3000E-02	3.6406E-02	2.9500E-02	3.8600E-02	4.1500E-02	2.2000E-02	1.9000E-02			3.7000E-02				2.1000E-02
٥		0.0510	0.0650	0.0840	0.1020	0.1160	0.1338	0.1550	0.1760	0.2010	0.2270	0.2530	0.2860	0.3070	0.3500	0.3864	0.4159	0.4545	0.4960	0.5180	0.5370	0.5784	0.5980	0.6350	0.6720	0.7070	0.7260	0.7470
	DA		Ø	Ø	0.0000E+00	Ø	Ø	Ø	Ø	Ø	Ø	3	Ø	Ø	Ø	Ø	ø	Ø	Ø	Ø	Ø	ø	(2)	Ø	ø	Ø	ø	Ò
Œ		0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750
	M		177	225	212	153	195	210	197	219	203	291	233	137	262	200	143	180	172	88	80	134	69	115	110	92	51	53
CYCLES		233	410	635	847	1000	1195	1405	1602	1821	2024	2225	2458	2595	2857	3057	3200	3380	3552	3640	3720	3854	3923	4038	4148	4240	4291	4344

2
AFCG-3 Flaw
_
L
3
1
G
C
щ.
4
2
5
.=
٠
Œ
_
3
Ü
_
D
Calculations
dc/dn
P
`
2
0
Vs.
KMAX
3
3
Y
3
73
-
Table
_
-
.0
_

	CRACK TYPE CODE,E= 3	GROSS AREA STRESS,S= 16.230	HOLE DIAMETER, D= 0.2962	PANEL THICKNESS, T= 0.3750	ଜ.ଜଜଜ
LEST CHSE IU HFUG-3 F4	# OF CYCLE ENTRIES,M= 26	# OF CRACKS IN HOLE, B= 1	FASTENER LOHD, P= 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO,R= 0.000

MIDTH,W= 4.0000 WIDTH,W= 4.0000 PANEL THICKNESS,T= 6.3750 NOTES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 AND E=3 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=2 E=4,COMBINED LOAD CASE OF E=3 E=4,COMBINED	DEBETH OF SURFHUE CRHOS OR CORNER CRHCKSSTT DIRECT CHHRIF LENGTH OF SURFHUE CRHCK OR LENGTH OF CORNER OF THE CHILD NOT TO CORNET THE OWN OF THE	
---	---	--

DC/DN	4.6328E-05	.3556	.4906	.15036	.7436E	1.0667E-04	1.1472E-04	1.1872E-04	1.2808E-04	.4428	.50216	.6788	83218	. 00506	.23086	4444	.6860	.93186	2.6250E-04	.6567	.62328	.8261	4.1818E-04	-8630E-	4.7647E-04
AVG KMAX	13,457	13.857																							
KMAX	13,593	14.122	14.548	14.838	15.187	15.546	15.864	16.189	16.482	16.785	17.128	17.347	17.795	18.170	18.472	18.897	19,358	o	19.841	Ġ	ö	-	-:	oi	oi.
2	8.2000E-03	1.8800E-02	1.8000E-02	4000E	9000E	2400E	2600E	GOODE	6000E	30006	SOODE	SOODE	SOOBE	0100E	1900E	4000E	6200E	5800E	2.1000E-02	3000E	SOOGE	4000E	6000E	2900E	4300E
	0.0722				•																				
ВЭ	0.0000E+00	0. ଉଉଉଉE+ଉଉ																							
A 9.3758	0.3750																								
Z	177	225	212	153	190	210	197	219	203	201	233	137	262	200	143	180	172	88	88	134	69	115	110	92	51
CYCLES 233	410	633 1	847	1999	1195	1405	1602	1821	2024	2225	2458	2595	2857	3057	3200	3380	3552	3640	3720	3854	3923	4638	4148	4246	4291

2
Flaw
AFCG-3
Calculations
d2c/dn
Vs.
KMAY
74.
Table

AND THE PROPERTY OF THE PROPER	TEST CASE ID AFCG-3 FS # OF CYCLE ENTRIES,M= 21	NOTES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION-+(ULC/DN) B=1,SINGLE CRACK MITHIN THE FASTENER HOLE(U2C/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(U2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)T DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF (CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

, , , , ,	DECON		.9096E-0	. 4444E-B	.4906E-0	8.4314E-05	.8974E-0	.4762E-0	.0102E-0	.0959E-0	.3695E-	.3532E-	.7167E-	-38788.	.3664E-	-80008.	.2867E-	-9667E-	8725-	-37788.	.7500E-	0
Pec	KNAX		00	0.08	0,40	10.757	1.06	1.40	1.30		(T)	4 G	30.00	00	4.78	in in	6.20	6.0	(T.	Ū,	0	50 F-
KMHX		00.	00	0.27	0.63	10.882	1.24	1.60	1.90	00.N	01 00 01	9.00	0,00	(C) : 寸	5.14	0.00 0.00	6.50	01 00 r-	00	10°	07	GJ.
			130	BBBE-B	BOBE-B	1.2900E-02	.9300E-0	900E-0	9-30066.	. 4000E-0	.7800E-0	.7200E-0	BOODE-0	. GBBBE-B	. 2000E-0	. GOORE - B	. ZOBBE-B	. COUGE-0	8900E-0	. 3160E-0	. SBBBBE-B	. 5000E-0
0		1111	.118	127	.136	G. 1430	.152	. 162	.172	400.	.198	212.	SSN.	0.40	.276	. 3B4	VOO.	.360	. 400	4.	044	00 00 1
	山		· BODDE+	. GOODE+	. OBOBE+	Ø. छछछछE+छछ	· BBBBE+	. BBBBE+	. OBOBE +	. BBBBBE+	. GBBBE+	. GBBBE+	. BBBBE +	· BBBBE+	. BBBBE+	, BBBBE+	. GBBBE+	. BBBBE+	· BBBBE+	· BBBBE+	. BBBBE+B	GGGGE+0
Œ		.37	0	.37	0.	0.3750	P. 0.	.37	00	. 3d	.33	.04	.37	.37	6.0	33	.37	.37	60	.07	.37	.37
	NO		^ <u>- </u>	NO 01	212	100	1.45	210	197	21.0 0.17	N 100	201	233	137	262	200	143	186	172	80	6 00	134
CYCLES		(0)	-	(0)	T	1866	(T)	9	99	္ ထ	80	OJ OJ	5	50	00	5	30	80	5	64	N	50
#		-	e4	00	4	(i)	ø	۲-	00	(T)	9	-	O.	0	4	5	9	-	00	5	80	77

		DC.ZBN	0 10000	.2727E-0	. BBBBE-B	.7573E-0	.7778E-0	6.57898-05	.9286E-0	.9286E-0	.1321E-0	.6792E-0	.3810E-0	.0256E-0	.7544 1999	9688E-6
910	TION RACK(S)	KMHX X	Ü	9.0	81	S.C.	50.		1.45	1.68	201	2.33	75	9	0.	3.5
Flaw 1	STRESS (DZC/DN) DC/DN) C/DN) - DIREC	MAX ,	4.0	900	40	50	00.	11.104	96	6.0	200	4		8.		42
- AFCG CODE, E STRESS ER, D=	ESS CRACK GROSS AREA LOAD ONLY IGURATION NER HOLE(DZ R CRACK(S)- LENGTH OF NLY IF E=2 NLY IF E=2	DC	00000	. ପ୍ରସମ୍ପର୍ଥ - ସମ୍ପର୍ଥ - ସ	. 8000E-0	. 9000E-0	.2000E-0	2.5000E-03	. ଉପ୍ରତ୍ୟକ୍ତ	. 8888E-8	. ଅଷ୍ଟର୍ଜନ୍ୟ - ସ . ଉଷ୍ଟର୍ଜନ୍ୟ - ର	. 9000E-0	. 1000E-0	. 0000E-0	. ପ୍ରସମ୍ପର୍ଥ - ପ୍ର ସ୍ତର୍ଜ୍ୟ - ଜ	. 0000E-0
Vs dc/dn Calculations CRACK TYPE GROSS AREA HOLE DIAMETE PANEL THICK!	CRACK CORNE CRACK CONTENT FROM THE FROM THE FROM CORNE CRACK CRACK CORNE CRACK CRACK CORNE CRACK CORNE CRACK CORNE CRACK CORNE CRACK CORNE	0 8	010	00.00	. 022	. 627 000	. 633	9.8368 9.888	. 645	.050	.850	.069	. 488 488	. 688	20.0 00.0	1691
75. Kwax 14 F1 15 20 18 1 1800 1800 1800 1800	SURFACE OR THROUS CORNER CRACK(S), SINED LOAD CASE OR THROUGH CITE CRACK WITHIN THE CORRECTIONS OLD CORRECTIONS	. (002 001 000 000 000 000 000 000	୦୬ /.ଅପ୍ରପ୍ରମ ହଣ 1.ଉଷ୍ଣ୍ରମ-ଡ	28 3.8888E-8	77 4.9000E-0 00 1 /aaac.a	35 4.2000E-0	68 88 84	50 5.0000E-0	98 5.9998E-9	58 5.88885-8 18 5.88885-8	99 8.9888E-8	30 3.1000E-0 40 1.1000E-0	80 4.0000E-0	80 1.0000E-0	10 0.0000E-0
ID A ENTRI S IN H OBD, P= LATE M	TES: E=1,50R SU E=2,50R CO E=4,00MBIN B=0,SURFAC B=1,SINGLE B=2,TWO CR C=HALF LEN FILLED HOL		න න	04 90 90	6 6.6	ധ മ മ	4 9 9 9	38 0.0 3	6.00 6.00	9.00	2 . 2 . 2 .	3 6.9	00 20 20	9.0	~ o 2 c 2 -	7 6.1
TEST CASE # OF CYCLE # OF CRACK FASTENER L PANEL WIDT	2	CYCLES			471	O	OW	397 443	TO.	10 c	2 4	0	4 5	1 77	0 0	40
		# .	(vσ	41	ın v	۰، ۵	ωσ			70					

Table 76. KMAX Vs dc/dn Calculations - AFCG-4 Flaw 2	CRACK TYPE CODE,E= 2	GROSS AREA STRESS, S= 21.	OIR	PANEL THICKNESS, T= 0.3750	96
's dc/dn C		_	-	-	AS RATIO,R= 0.000
K WAX	F2		90	_	RATIO
Table 76.	CASE ID- CYCLE EN	CRACKS IN	ENER LOAD, P	PANEL WIDTH, W= 4.8888	ENER/PLATE MODUL

NOTES:
E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S),FASTENER LOAD GALY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION—(D2C/DN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE—(D2C/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE—(D2C/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)—T DIRECTION
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2 .918 Ø

	DC/DN	-	.3077E-0	.2727E-0	.9474E-0	.9677E-0	.0732E-0	.!.	.1111E-0	9	.!.	٨.	.!.	.9565E-	1.6667E-04	.2642E-	.7500E-	.3750E-	.1282E-	.7778E-	.1176E-	.5909E-	4.04556-04
RUG	KMAX		9.294	9.437	9.755	10.217	10.601	10.905	11.279	11.621	-	12,152	O	12.779	13,645	13,320	13.667	13.954	14.168	14,345	4	14.605	7
KMAX						ø		-	-	-	oi		oi					4				14.687	
	DC DC		. 0000E-0	. 0000E-0	. BBBBE-B	. 7000E-0	. 9000E-0	.4000E-0	. 6666E-6	. BBBBE-B	. 1000E-0	. BBBBE-B	. 9000E-0	. BBBBE-B	. BOBBE-B	. 2000E-0	.6500E-0	. 5000E-0	.2200E-0	.8000E-0	. BOBBE-B	1.0100E-02	.9000E-0
ပ																						0.1506	
	DH.		. 0000E-0	. 0000E-0	. OBBBE-B	.7000E-0	.9000E-0	. 4888E-8	. BBBBE-B	. 0000E-0	.1000E-0	. 0000E-0	.9000E-0	. 0000E-0	. 0000E-0	.2000E-0	.6500E-0	.5000E-0	.2200E-0	.8808E-8	. 0000E-0	1.0100E-02	. 9000E-0
Œ		9	9	9	Θ.	9	Θ.	9	9	9	3	0	Θ.	0	Θ.	<u>.</u>	-:	-:	-:	-:	-:	0.1511	-:
	K		56	44	92	62	41	525	94	38	46	26	26	46	4 0	23	69	40	39	130	17	22	22
YCLES		4	30	74	150	212	253	305	359	397	443	499	555	601	649	762	762	802	841	859	928	898	950

ن

	10/20	.4643E-(.5484E-(. 5879E-	. 00000E-0	2250E-(1.4844E-03 1.6873E-03 1.7856E-03	. 9353E-
918	RHCK(S)	24.28	4.04.0 1.04.0	30.00	44400 86000 800000		04046	9.0
Flaw 21.	CD2C/DN) DC/DN) C/DN) C/DN) T DIREC CORNER C	99.76	 		4.4.0.0.0 0.00.0.0 0.00.0.0	7.15.25 5.25.25 5.25.25	28.188 29.188 29.651	9.89 8.89
- AFCC CODE: STRESS RESS: RESS: RECK RECK	E 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	.7888E-8 .6288E-8	 4.4.4 0.4.4.0 2.2.2.2.2 2.2.2.2.2 2.2.2.2.2 2.2.2.2.	. 10000. . 90000. . 90000. . 90000.		. 99996 - 45696 - 96966 - 95966 - 95966 - 95966 - 95966		.1200E-0
Cal CR CR CR CR CR CR CR CR CR CR CR CR CR	5m5mr8x8	0.00 0.440 0.440	21.1. 2000 2017	2000	0000.44 0000.44 0000.44	44.00 7.00 7.00 7.00 7.00 7.00	6.613 6.6813 7.126 7.126	.782
KMAX Vs de 1	TO SECTIONS DATE TO SURFICE . 9999E+9	 2000 2000 2000 2000 +++ 2000	20000 20000 20000 20000 20000 20000 20000	000000.0000000000000000000000000000000	. 00000E. . 00000E. . 0000E. . 0000E. . 0000E.	000000	. 0000E+0	
HFCG- HOLE; M HOLE; M HOLE; M HOLE; M HODUL	COMBINED OF STATE OF	375	 	2750		00000 00000 000000	99999999999999999999999999999999999999	375
		0.41 84	6848	ა ღ ც4- 14დტ	യ ഗ ഗ ഗ ര മ ഗ 4 ഗ	78893 78893 78893	100001	23
######################################	CYCLES	01-1	n - m c	0 W W 4 1	へののいり	-004V	2007 2007 2004 2004 2004 2004	10
	#	→ 000	4 NO OL	- 00 0 0	-2554 m	92286	33578	22

4
3
Flaw
E
=
1
FCG-4
4
S
Calculations
at
=
2
=
S
dc/dn
7
ŏ
Vs
K MAX
3
Y
Table 78.
9
P
19
-

TEST CASE ID AFCG-4 F4	
# OF CYCLE ENTRIES,M= 27	CRACK TYPE CODE,E= 2
# OF CRACKS IN HOLE, B= 1	GROSS AREA STRESS,S= 21.910
FASTENER LOAD, P= 0.000	HOLE DIAMETER, D= 0.3540
PANEL MIDTH, W= 4.0000	PANEL THICKNESS, T= 0.3750
FASTENER/PLATE MODULAS RATIO, R= 0.000	ଉ.ଉଉଡ

NOTES:
E=1,FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION~-(D2C/DN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE~-(DC/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE~-(D2C/DN)
A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)~-T DIRECTION
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)
FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

	DC/DN		3.0400E-04	3.4833E-04	4.8871E-04	5.4634E-04	6.1154E-04	7.2407E-04	6.9211E-04	7.5435E-04	8.3571E-04	8.8182E-04	9.4706E-04	1.1261E-03	1.0217E-03	1.1050E-03	1.2929E-03	1.2714E-03	1.3844E-03	1.3650E-03	1.4364E-03	1.5556E-03	1.6118E-03	1.5435E-03	1.6579E-03	1.6750E-03	1.7500E-03	1.7135E-03
AVG	KMAX		17.340	18.878	20.575	21.420	22,120	22.889	23.501	23.994	24.586	25.038	25.372	25.741	26.051	26.337	26.704	27.104	27.566	28.041	28.443	28.861	29.259	29.727	30.239	30 756	31.291	31.810
КМЯХ		16.971	17.708	20.047	21.102	21.739	22.501	23.276	23.727	24.261	24.911	25.166	25.578	25,984	26.198	26.475	26.933	27.275	27.857	28.225	28.662	29.068	29.459	29.994	30.485	31.027	21.555	32.064
	2								2.6300E-02																		3.1500E-02	
٥		0.0346	0.0422	0.0840	0.1143	0.1367	0.1685	0.2076	0.2339	0.2686	0.3154	0.3348	0.3670	6.3929	0.4164	0.4385	0.4747	9.5014	0.5457	0.5730	0.6046	0.6326	0.6600	0.6955	0.7270	0.7605	0.7920	0.8213
	当		9.9999E+99	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	9.9999E+99	0. ଉତ୍ତତ୍E+ଉତ	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+60	9.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	9.0000E+00	0.0000E+00	9.0000E+00	0.0000E+00	BOBBE	0.0000E+00
Œ		0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	9.3759	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	9.3750	0.3750	0.3750	0.3750	0.3750	0.3250
	K		25	120	62	41	52	00 44	38	46	99	22	34	23	23	20	28	21	32	20	22	13	17	23	19	20	18	17
CYCLES		io.	30	150	212	253	305	359	397	443	499	521	522	228	601	621	649	629	202	722	744	292	622	802	821	841	828	928

2 KMAX Vs d2c/dn Calculations - AFCG-4 Flaw Table 79.

		D2C/DN		.5682E-0	.9737E-	.7363E-0 .7561F-0	.3462E-	.2407E-0	.1413F-0	.2750E-0	1.6300E-03	.00000. .000001 .000001	.1435E-0	.1957E-0	.6050E-0	. 7888E-8	1857E-3
.918	CTION CRACK(S)	AVG KMAX	SB2	00	201	. 4	41.	V-1 © 0 0 0	-00	9. J	200 4. 000 000	· · ·	σ 	F- 1	4.00 00.4		6.10
E= 1 S,S= 21 0.0000 T= 0.375	STRESS -(D2C/DN (DC/DN) 2C/DN) 2C/DN) 1 DIRE CORNER	MAR C	12.884	.69	4 u	- 10	6.52		9.01	0.19	(0) (0)	· (1	3.3	4.12	4 C	0.00	7.18
TYPE CODE, AREA STRES DIAMETER, D=	CKNESS CRACK IRM GROSS AREA BND E-3 CONFIGURATION- STENER HOLE ISTENER HOLE TENER HOLE TENER HOLE TO CRACK(S) COR LENGTH OF COR LENGTH OF	D2C	.5000E-0	.5700E-0	. 57557. 57557. 57557.	.3600E-0	.3000E-0	. 45000E-0	.2500E-0	.5900E-0	3.2688E-82	.2200E-0	.9300E-0	. 8588E-8	.2100E-0	.5700E-0	.6900E-0
CRACK GROSS HOLE PANEL	CARCALLER CORRECTED TO THE CORRECTED	υ :	6.1168 6.1148	 S.C.		164	.180	2000 2000	246	.269	000 000 000	333	.358	. 383	4.4 200 000	451	484
4 4 6 6 6 6 6 6	CE CRACK CRACK CRACK CRACK CATHROUGH CATHITHI CRECK CRACK CR	ЪН	. BBBBE+B	. 0000E+	• 20 (7	.0000E	. BBBBE		.0000E	. BBBBE+B	B. BBBBE+SS	. BBBBE+B	.0000E+0	. 8888E+8	. NUNUNE+B	. 0000E+0	. 0000E+0
AFCG- NTRIES,M: IN HOLE: D,P= ,0.0	FOR SURPER SURPER SURPER CORRESPONDENCE CORRESPONDE	æ 6	6.3759	.375	0,00	.370	.375	.375	375	.375	070	375	.375	.375	0,00	375	.375
CASE ID CYCLE E CRACKS NER LOA	NON 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Z	00 00 00	41	90	41	ev : In t	υς • α	46	98	3 2	34	23	S 5	200	100	21
TEST # OF FASTE PANEL	garden en de ret en fre Director de de en de El mention media en management	CYCLES	36	- L	0 -	10	OI	OU	4	P- (4 NO 20 CO	W)	P-	(S) (VO	4	1-

RECE ENTRESTED CONTROL OF STREESS, S = 10.000 RROLD P = 0.000 MIDTH,W = 4.0000 RR LOAD.P = 0.000 RR LOAD.P = 0.000 RR LOAD.P = 0.000 RR PRICE THICKNESS, T = 0.3750 RE 1.FOR SURFACE OR THROUGH THICKNESS CRACK E = 3.FOR CORNER CRACK(S), HORFORM GROSS AREA STRESS E = 3.FOR CORNER CRACK(S), FRSTENER LOAD ONLY E = 4.COMBINED LOAD CASE OF E = 2 AND E = 3 R = 0.51 NGLE CRACK MITHIN THE FASTENER HOLE - (DC/DN) R = 1.SINGLE CRACK MITHIN THE FASTENER HOLE - (DC/DN) R = 2.TWO CRACKS MITHIN THE FASTENER HOLE - (DC/DN) R = 2.TWO CRACKS MITHIN THE FASTENER HOLE - (DC/DN) R = DEPTH OF SURFACE CRACK OR CORNER CRACK(S) - T DIRECTION C = HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF E = 2

DC/DN		-	_		J.		w		-		-		•												~	9.2500E-06	-	
RVG KMRX		4.551	4.652	4.776	4.891	4.949	4.993	5,044	5.097	5.142	5.187	5.247	5.389	5.364	5.425	5.492	5.598	5.699	5.770	5.881	6.012	6.160	6.337	6.467	6.551	6.656	6.773	6.861
КМЯХ	4.499	4.603	4.702	4.851	4.930	4.967	5.020	5,069	5.124	5,159	5.214	5.281	5.337	5.398	5,459	5.525	5.671	5.726	5.814	5.948	6.076	6.243	6.430	6.505	6.596	6.715	6.830	6.892
DC		8000E	9000E	30008	BBBBB	1.0000E-03	50006	5000E	SOBBE	2000E	GOOGE	GOODE	4000E	4000E	4000E	SBBBE	7000E	7000E	BOODE	BEBBE	1400E	7000E	2000E	BOODE	1.3000E-02	1.8500E-02	1.9500E-02	1.1000E-02
o e		0.0213				A 100																						
DA		1.8000E	1.9000E	3.3000E	2.0000E	1.0000E	1.5000E	1.5000E	1.8000E	1.2000E	2.0000E	2.6000E	2.4000E	2.4000E	3.4000E	3.5000E	8.7000E	3.7000E	6.3000E	1.0600E	1.1400E	1.7000E	2.2000E	1.0000E	1.3000E	1.8508E-02	1.9500E	1.1000E
Œ	0.0200	0.0218	0.0237	0.0270	0.0296	9.6366	0.0315	0.0336	0.0348	0.0366	0.0386	9.0406	0.0436	0.0454	0.0488	0.0523	0.0616	0.0647	0.9716	0.0816	0.0936	0.1100	0.1320	0.1420	0.1550	6.1735	0.1930	0.2040
A		1866	1899	4466	3200	866	1800	2000	1600	2200	1866	2400	2400	1400	3400	2600	3200	2000	2200	3000	3000	3200	2800	2888	1688	2000	2000	1669
CYCLES	2200	4868	5889	19266	13466	14200	16000	18000	19600	21800	23600	26000	28400	29860	33200	35866	39000	41666	43200	46200	49200	52400	55266	57200	58899	60800	62800	63899
#		cu.	0	4	m	Ó	r-	00	g,	10		N	0	4	5	10	2	8	61	(D)	Z.	C)	0	4	50	92	2	00

			DC/DN	.3333E	2727E	.25006	. 0000E	25006	. 6667E	.9167	.7143E	2.6923E-06	50006	.86676	.66678	.0000	. 00000	11506	1 1000
2	9	10N ACK(S)	A WG KMBX	1-1		ωσ.	0,0		ńω.	4 N	01			114	œα	90.	-0	:	7.78
9	୍≕ 10.0 .3200 ଚ.3750	STRESS +(D2C/DN) (DC/DN) 2C/DN) 2C/DN) CORNER CRR	E L	200.0	0.00	0.0	0-		. 4. 1	ņο	200		· CI C	ישיי	·0	.00	w.	4	7.694
ations - YPE CODE,	AREA STRESS IAMETER.D= THICKNESS.T	S CRRCK OSS AREA DO ONLY ORATION- R HOLE CRRCK(S) VIF E=2	ည	. 0000E-0	. ଚଉଚ୍ଚର - ଚ	. 8868E-8	.8000E-0	. 0000E-0	. GOOGE - G	. 0000E-0 . 6000E-0	. 8000E-0	.0000E-0	. 0000E-0	.3400E-0	3000E-0	.8000E-0	. 0000E-0	.2300E-0	2.3600E-02 1.1100E-02
dc/dn Calcu CRACK	GROSS HOLE D PANEL .000	UGH THICKNES UNIFORM GR OF E=2 NND GR CRACK CONFIG THE FASTENER K OR CORNER E CRACK OR L	ى 0 0	6.6229 6.0229	90	20	00	000	200	20	00	000	.00		-:-		de	iú	uu
KMX VS	3= 1 900 90 15 RATIO,R= 0	NOTES: E=1.FOR SURFACE OR THROUGH E=2.FOR CORNER CRACK(S), U E=3.FOR CORNER CRACK(S), FOR CORNER CRACK(S), FOR CORNER CRACK(S), FOR SURFACE OR THROUGH CRACK WITHIN THE B=2, TWO CRACKS WITHIN THE REPORTH OF SURFACE CCHACK OF TILLED HOLE CORRECTIONS APPLICATIONS APPL	В	-6.8888E-8	1.0000E-0	1.0000E-0	1.8000E-0	2.0000E-0	3.0000E-0	5.0000E-0	3.8000E-0	7.0000E-0	9.0000E-0	1.7600E-0	2.3000E-0	2.8000E-0	2.0000E-0	2.2300E-0	2.3600E-02 1.1100E-02
e e e e e e e e e e e e e e e e e e e	MODULAS MODULAS	SURFECTOR SURFE	E 0	0.0227	90	20	00	000	200	20.00	20	000	100		-:-	10	w	10	ww
ASE ID-	CRACKS IN ENER LOAD, P WIDTH, WE	00 E = 18 E = 18	ă	1800	4400	3266	1800	1600	1800	2468	1400 3400	2600	2000	3000	3000	2800	2000	2000	2000
TEST C			CYCLES	40000	10200	13466	16000	19600	23600	26666	33288	35888	41000	45200	49200	55200	57200	60800	62888
				- 00 0	041	o o	~ α	000	2 = = =	13	4 1	116	8	50	22	531	4 K	56	28

aw
E
AFCG-5 Flaw
1
Calculations
dc/dn
Vs
KWAY
×
82.
e
Fable

		CRACK TYPE CODE, E= 2	GROSS AREA STRESS,S= 10.000	HOLE DIAMETER, D= 0.3230	PANEL THICKNESS, T= 8.3750	ଓ ପ୍ରସେଶ
V	LEST CHSE ID HFCG-5 FG	# OF CYCLE ENTRIES,M= 21	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P = 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO, R= 0.000

OLE,8= 1 GROSS AREA STRESS,8
30 11
ODULAS RATIO,R= 0.000
E=1, FOR SURFACE OR THROUGH THICKNESS CRACK
E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS
E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY
E=4,COMBINED LOAD CASE OF E=2 AND E=3
B=0,SURFACE OR THROUGH CRACK CONFIGURATION(DJC/JN)
B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN)
B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/IN)
A-DEPTH OF SURFICE CRACK OR CORNER CRACK(S)T DIRECT
C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CR
FILLED HOLE CORRECTIONS APPLIED ONLY IF F=2

		0	.1111E-0	.8889E-B	.4615E-0	1.0276E-05	. 1000E-0	.2500E-B	.3750E-0	.4091E-0	.5556E-0	.6667E-8	.8333E-B	. 1154E-0	. SBBBE-B	.4167E-0	. 6900E-0	8929E-B	B-BOE-B	. 235BE-B	7500E 0	6899E 0
AVC	KMAX		00	10	.0	(O) (N) (N)	₹.	T.	0,	E.	(Z)	T)	(Z)		4		00	0	0	N-	3.0	3
KMHX		00	98.	00	1.		40.	·	8.82	B.28	6.48	6	1.01	1.33	1.62	1.39	2.00	2.5B	2.57	3.00	3.10	(C)
	. III.		. 28bbE-B	4200E-0	14600E-0	5.9600E-02	. 9800E-0	. SOBBE-B	. 2000E-0	, 1000E-0	. SOBBE-B	. ӨӨӨӨЕ-Ө	, 4000E-0	. SOBBE-B	. ОБООЕ-О	9-BBBBE-B	.6400E-0	. 1000E-0	. 2360E-0	.4700E-0	. SBBBE-B	- 6460E-
Ü		.001	.013	.828.	.052	0.1122	132	.157	£71.	.210	000 N	®~0.	01 04 09	.377	427	.456	(C) (T) (T)	470.	000.	.651	.666	01 00 1-
Ĥ	HI	5	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	3750 0.0000E+00	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	758 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0	750 0.0000E+0
	M		999	800	600	5869 8.	890	999	600	200	899	488	400	600	200	200	400	866	466	000	99	00
CYCLES		Q.	Ø	00	4	14288	0	88	9	8	98	Ø	か	2	8	4	ထို	90	9	Ξ	4	0
#		-	cu	က	4	ريا ديا	œ	~	00	σ		=										

Table 83. K_{MAX} Vs dc/dn Calculations - AFCG-5 Flaw 4

CRACK_IMPE CODE.E= 2	LOLD BIOMFIED BY COSE	PANEL THICKNESS,T= 0.3750	ଜ ଜଣ୍ଡଣ	
# OF CYCLE ENTRIES,M= 17	# UP CRHCKS IN HOLE,8= 1 FRATENSE - OBD.P= 0 000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO.R= 0.600	

NOI E O	E=1.FOR SURFFICE OR THROUGH THICKNESS CRACK	E=2.FOR CORNER CRACK(S). UNIFORM GROSS AREA STRESS	E=3.FOR CORNER CRACK(S), FASTENER LOAD ONLY	E=4, COMBINED LOAD CASE OF E=2 AND E=3	B=0.SURFACE OR THROUGH CRACK CONFIGURATION(0.5C/IN)	B=1.SINGLE CRACK WITHIN THE FASTENER HOLF(DC-10)	B=2,TWO CRRCKS WITHIN THE PRSTENER HOLE(1927,500)	A=DEPTH OF SURFFICE CRECK OR CORNER CRAFK(S): DIRECTION	C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CHARER CRACK	HOLE CORRECTIONS APPLIED ONLY IF FED	
---------	---	--	---	--	---	--	---	---	--	--------------------------------------	--

À	6.6667E-06 7.7778E-06	.8462E-0		.5366E-6 .8125E-8	.7273E-0	0778E-6	.166/E-6	(1) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.83465-6	.2773E-0	.7167E-0	. 928AF-G	52505-0
КМА КМАХС	₽ 4	(Tr - 1	ბ. 4.ბ. 1.00 1.00 1.00	(D) (E) (D) (E) (E) (E) (E) (E) (E) (E) (E) (E) (E	6. 6. 6.	00	1.15	1.4	00 10	(N	00 · 00	Œ,	و
жни 19.	000 000 000 000	 (2) (2)	ად. თდ. ეძ	0.00 0.00	(A)	1.00	1.30	1.63	2.07	i.0:	⊕8°.	. T	4.11
2	. 2000E-0	.3000E-0	6.5500E-02 2.3900E-02	. BEBBE-B	. SBABE-B	. 1866E-6	D-BODDS.	.8600E-0	.3700E-0	.2100E-0	.4600E-0	. SØØØE-Ø	.2670E-0
ი . მ 44	8.80061 8781	 	.100	0.44 0.44	288	.321	100 100 100 100 100 100 100 100 100 10	4.	. 500	.577	.622	.677	. 8B3
α ()-	. 8888E+8	.3750 0.0000E+0	.00	.3750 0.0000E+0 3750 0.0000F+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0	.3750 0.0000E+0
A	1898	2690	5000 10000 1000	2000 1600	(2000 (2000) (2000) (2000) (2000 (2000) (200	1866	2400	2400	2699	2200	1200	1400	2880
CYCLES 2200	4 6660 8600	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	14299 16999	$\infty \sigma$	21000	$^{\circ}$	w	ω	-	(1)	4	588	860
#	ou e) च	ഗവ	r- 0	000	10	11	12	0	14	15	16	17

Table 84. K_{MAX} Vs d2c/dn Calculations - AFCG-5 Flaw 5

CRACK TYPE CODE,E= 1 GROSS AREA STRESS, = 10.000 HOLE DIAMETER,D= 0.0000 PANEL THICKNESS,T= 0.3750	TES: E=1.FOR SURFACE OR THROUGH THICKNESS CRACK E=2.FOR CORNER CRACK(S), UNIFORM GROSS AREA SIJESS E=3.FOR CORNER CRACK(S), UNIFORM GROSS AREA SIJESS E=4.COMBINED LOAD CASE OF E=2 AND E=3 B=9.SURFACE OR THROUGH CRACK CONFIGURATION——(GLC/DN) B=1.SINGLE CRACK WITHIN THE FASTENER HOLE—(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)—(DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CURNER CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2
TEST CASE ID AFCG-5 F5 # OF CYCLE ENTRIES,M= 18 # OF CRACKS IN HOLE,B= 0 FASTENER LOAD,P= 0.000 PANEL WIDTH,W= 10.0000	NOTES: E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION—B=1,SINGLE CRACK WITHIN THE FASTENER HOLE—B=2,TWO CRACKS WITHIN THE FASTENER HOLE—CB B=2,TWO CRACKS WITHIN THE FASTENER HOLE—CB C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2

P20/014	17E 0		.2222E-0	. OBBBBE-6	625E-0	.1818E-0	.3889E-0	.6250E-0	417E-0	.5385E-0	. 6000E-0	.7500E-0	. 0000E -0	.5679E-0	.0250E-0	.1100E. E	8000E-0	
KMAKG	00	6.214	50	-71	7		(*)	, O	00.	0	·	6	16	00.	39	0	4	
MAX.	0. 0. 0. 0.	(D) 寸。	19.	00	. 01	00.	90.	90	. □	· BB	50	ज क	00	0	94.	01	େ ଅପ	
D2C	.5100E-0	3. SBBBBE-B2	. SOBBE-B	BOBE-B	. 7000E-0	. EBBBE-B	.5000E-0	B-BBBBE.	. 9000E-0	. GBBBE-B	. GBBBE-B	. 2000E-0	. GBBBE-B	.2790E-0	BIODE-0	B-BBSSS.	.1200E-0	
0 0	Ø.1135	.132	₩.139	. 148	921.	. 169	.182	. 201	922.	900 ·	000 000 000 000 000 000 000 000 000 00	.313	.341	.405	415	.476	4.01	
ω. Έν	, BBBBE+	. w	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	.3750 0.0000E+	
3	10	5880	00	(3)	U	O	00	寸	TT.	W	(3)	寸	4	00	400	2000	400	
00	8400	(니 다	99	130	O.	0	36	9	00	0	20	4	8	98	90	10	4	
#	cu	(0)	4	רנו	9	۲-	00	(T)					14					

-
aw
E
AFCG-6 Flaw
1
Calculations
5
Calc
dc/dn
٧s
KMAX
82.
able

	CRACK TYPE CODE, E= 2	GROSS AREA STRESS, S= 8.500	HOLE DIAMETER, D= 0.2824	PANEL THICKNESS, T= 0.3750	ଜ.ଜଜଜ
TEST CASE ID AFCG-6 FI	# OF CYCLE ENTRIES, M= 31	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P = 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO,R= 0.000

DC / DN	119 /09	.5267E-0	.5789E-0	1.1613E-05	.7004E-0	519E-0	.7196E-0	.1196E-0	.0710E-0	.6455E-0	.6296E-0	.3383E-0	.2673E-0	.6715E-0	.1647E-0	.9055E-0	.1344E-0	.5700E-0	.6353E-0	8E-0	.0492E-0
9 0 0 0 0 0 0	VIIIV	40.	· 67	4.163	.31	.43	.53	.67	-7	0	96.	. 02	110	5	0	σœ.	94.	.61	N.	88.	98.
KMAX	2	4.646	. 18	<u>N</u>	4.	4.0	.61	N.	8.	о. •	Ф Ф.	40.	.16	evi evi	46.	. 4 U	40.	.68	1-	.83	96.
Ç	- In	. BBBBE-B	. OBOBE-B	3.6000E-03	.4000E-0	. BBBBE-B	.2000E-0	.8000E-0	. BBBBE-B	. BBBBE-B	.1000E-0	. 7000E-0	.3200E-0	. 6000E-0	.7700E-0	.5700E-0	.6000E-0	.7100E-0	.9700E-0	.2200E-0	.5400E-0
J	. A26	0.0256	.027	.031	. 839	. 041	.050	.058	.065	.075	. 082	.087	. 100	.108	.125	.141	.157	.184	.204	.216	.232
ė,		-4.0000E-3	2.0000E-0	3.6000E-03	8.4000E-0	2.0000E-0	9.2000E-0	7.8000E-0	7.0000E-0	1.0000E-0	7.1000E-0	4.7000E-0	1.3200E-0	7.6000E-0	1.7700E-0	1.5780E-0	1.6000E-0	2.7100E-0	1.9700E-0	1.2200E-0	1.5480E-0
Œ	0.0	0.0260	. 02	. 03	40.	40.	. 65	. 65	.06	. 07	. 98	. 98	.10	. 10	.12	14	.15	. 18	.20	.21	.23
740	<u> </u>	10	(3)	319	O	(2)	(0)	D	00	P-	P-	(2)	(2)	(2)	O	(3)	00	O	O	4	(2)
CYCLES	600	601	905	2	70	8	50	2	89	5	20	96	8	5	46	40	0	80	25	2669	36
#	-	(N	0	4	S	ø	~	00	σ											50	

	Z Z				-0.5	E-05	196	2 4	100	N	45	
	DC/D	0871E	5072E	3846E	1381	1941	1419	0 44215	S ASSOR.	9 4049E.		
ntinued)	AVG KMRX		6.108		3.4	6.82	1.380	100 S	のから、四十	10	21.119	
Flaw 1 (Co	КМЯХ	99	7	00	4	16	D.	of T	7	00	:2.665	
Vs dc/dn Calculations - AFCG-6 Flaw 1 (Continued)	Ö.	.9200E-	.1400E-	- BBBBE-	4000E-	.2000E-	- 2000E-	. 1000E-	- BOBBB-	- SBBBE-		
Calculat	U	.261	.272	.279	0.3036	335	92.	90	98	99.	<u>4</u>	
KMAX	E H	.9200E-	.1400E-	-BOOOG.	.4000E	-2000E-	.2000	. 1666	2.0000E-1	.8999	. 1666	
Table 85.	σ	.26	2	28	38	33	46.	37	0.3990	43	च च	
	Z	574	207	130	391	471	168	365	231	404	33	
	CYCLES	7876	8083	8213	8604	9075	9243	9608	9839	10243	10316	
	#	22	23	24	25	56	22	28	53	30	E	

Table 86. K_{MAX} Vs dc/dn Calculations - AFCG-6 Flaw 2

		GROSS AREA STRESS,S≃ 8.500	HOLE DIAMETER, D= 0.2824	PANEL THICKNESS, T= 0.3750	ଓ. ଉପ୍ତ
TEST CASE ID AFCG-6 F2	# OF CYCLE ENTRIES,M= 31	# OF CRACKS IN HOLE, B= 1	FASTENER LOAD, P = 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO,R= 0.000

NOTES:	E=1,FOR SURFACE OR THROUGH THICKNESS CRACK	E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS	E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY	E=4,COMBINED LOAD CASE OF E=2 AND E=3	B=0.SURFACE OR THROUGH CRACK CONFIGURATION(SC/DN)	B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN)	B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/JN)	A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION
E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(CSC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) A=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION	E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(USC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION	E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(CSC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION	E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(C3C/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION	B=0.SURFACE OR THROUGH CRACK CONFIGURATION(38/2DN) B=1.SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2.TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)7 DIRECTION	B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)) DIRECTION	B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/JN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)7 DIRECTION	A=DEPTH OF SURFRCE CRACK OR CORNER CRACK(S)1 DIRECTION	
E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(CSC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)	E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(CSC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)	E=3,FOR CORNER CRACK(S),FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(CSC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)7 DIRECTION C=HALF LENGTH OF SURFACE CRACK.OR LENGTH OF CORNER CRACK(S)	E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(CSC/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)7 DIRECTION C=HALF LENGTH OF SURFACE CRACK.OR LENGTH OF CORNER CRACK(S)	B=0.SURFACE OR THROUGH CRACK CONFIGURATION(38/2DN) B=1.SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2.TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION C=HALF LENGTH OF SURFACE CRACK.OR LENGTH OF CORNER CRACK(S)	B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)7 DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)	B=2,TWO CRACKS WITHIN THE FASTENER HOLE(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)1 DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S)	A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)7 DIRECTION C=HALF LENGTH OF CORNER CRACK(S)	CHALF LENGTH OF SURFFICE CRACK OR LENGTH OF CORNER CRACK(S)

DC/DN	.2901E-0	.9355E-0	19E-6	4348E-6	9365E-6	.1111E-6	.9010E-0	1529E-6	
ANG									4. 425
MAX.	32	9.49 4.49	93	1.00 A	000	68	9.4 20.4	888	44 40. 600
DC	. ଉପରସ୍ଟ-ପ . ଉପସ୍ତି-ପ	. 8888E-	. ଅଷ୍ଟର୍ଗ-ଜ . ଅଷ୍ଟର୍ଗ-ଜ	. 8898E-8	. 6666E-6	. 8888E-8 . 8888E-8	. 0000E-0 . 3000E-0	.9888E-8 .5888E-8	3.3000E-03 7.0000E-03
ი ი	. 995 . 996	. 005 005	. 885 788	989	410	.010	. 023 . 026	. 831 836	0.0396 0.0466
А .8875	.0069-6.0000E-0 .0075 6.0000E-0	.0069-6.0000E-0 .0070 1.0000E-0	.0072 2.0000E-0 .0090 1.8000E-0	.0110 2.0000E-0 .0130 2.0000E-3	0160 3.0000E-0	.0210 2.0000E-0	.0250 4.0000E-0 .0280 3.0000E-0	.0332 5.2000E-0 .0377 4.5000E-0	0.0410 3.3000E-03 0.0480 7.0000E-03
Ä	262 262 242	8 4 9 4 8 4	188 535	თ თ დ ო ო ო	9.00	201	484 484	4 204 202 202	387 593
CYCLES 339	601 905	1215 1709	1817 23 5 2	2729 3 9 58	3436	3907 3907	4311 4518	4949 5349	5732 6325
# +-	ol o	4 W	or	00 0	9	10	₩ 4	50	200

			.05	LO.	ம	Į,	v'	v	2	M	un.	LO.	n	in'	S
10 KB 000		DC/14	118E-		016E-	77.DE.	9324E-		4696E-	8875E-	9762E-	7671E-	5498E-	-3601b	6627E-
inued)	AN'G	KMAX	4.631	4.697	4.156	4 852	4.931	4. 9.7	5.026	5.122	5.200	5.258	5.324	5.403	5.459
aw 2 (Cont	KMAX		929.	718	.793	4.910	.953	966	.063	180	220	1000	385	454	465
MAX Vs dc/dn Calculations - AFCG-6 Flaw 2 (Continued)		DC	. BBBBE-B	. OBBBE-B	. SOBOE-0	1.0200E-02	. BBBBE-B	.7000E-0	. 7000E-0	.3600E-0	.OBOOE-0	.0100E-0	. 2000E-0	.5800E-0	9999E-8
Calculatio	٥		.052	.055	.061	0.0716	.075	.079	. 087	. 100	.105	.115	.123	.139	141
86. KMAX Vs dc/dn	T.	HG	.0540 6.0000E-0	.0570 3.0000E-0	.0628 5.8000E-0	.0730 1.0200E-02	.0770 4.0000E-0	.0807 3.7000E-0	.0884 7.7000E-0	.1020 1.3600E-0	.1070 5.0000E-0	.1171 1.0100E-0	.1253 8.2000E-0	.1411 1.5800E-0	.1438 1.9888-8
Table		呂	50	1-1	50	574 8	20	90	91	+	00	5	31	40	00
	CYCLES		6759	2669	7302	7876	8083	8213	8684	9075	9243	9688	9839	10243	10316
	#		19	20	21	S	23	24	25	26	27	28	53	30	50

3
Flaw 3
AFCG-6
Calculations
5
Cal
dc/dn (
٧s
K MAX
87.
Je

CRACK TYPE CODE, E= 2	GROSS AREA STRESS, 3 8.500	88	PANEL THICKNESS, T= 0.3750	3.688
# UP CYCLE ENTRIES, M= 25	# OF CRACKS IN HOLE, B= 1	*ASTENER LOAD, P = 0.000	PANEL WIDTH, W= 4.0000	FASTENER/PLATE MODULAS RATIO,R= 0.000

CRACKS IN HOLE, B= 1 GROSS AREA STRESS, S= 8.500 NER LOAD, P= 0.000 HOLE DIAMETER, D= 0.3130 MIDTH, W= 4.0000 PANEL THICKNESS, T= 0.3750 NOTES: NOTES: E=1, FOR SURFACE OR THROUGH THICKNESS CRACK E=2, FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3, FOR CORNER CRACK(S), FASTENER LOAD ONLY E=4, COMBINED LOAD CASE OF E=2 AND E=3 B=0, SURFACE OR THROUGH CRACK CONFIGURATION—(D2C/DN) B=1, SINGLE CRACK WITHIN THE FASTENER HOLE—(D2C/DN) B=2, TWO CRACKS WITHIN THE FASTENER HOLE—(D2C/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)—1 DIRECTION	C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF F=2
---	--

	DK/DN		115E-05	539E-05	323E-05	486E-05	037E-05	673E-05	922E-05	917E-05	640E-05	963E-05	677E-85	208E-05	126E-05	706E-05	040E-05	607E-05	494E-05	353E-04	729E-04	885E-04	540E-04	874E-04	1.69136 04	Stor of	
	-																										
ANG	KWWX		6.714	6.951	7.177	7,436	7.689	7.775	2.996	8.163	8.339	8.501	8.613	8.752	8.896	9.038	9.225	9.408	9.645	9.892	10.071	10.240	10.586	10.936	11.108	11.41	
KMAX		6.091	6.838	7.065	7.288	7.583	7.635	7.915	8.078	8.247	8.432	8.571	8.656	8.848	8.943	9.133	9.318	9.498	9.786	10.004	10.138	10.342	10.829	11.043	11.173	11.649	
	26		9.2000E-03	1.0500E-02	1.2500E-02	2.0000E-02	4.0000E-03	2.3900E-02	1.6200E-02	1.8900E-02	2.3300E-02	1.9700E-02	1.3000E-02	3.2000E-02	1.7000E-02	3,6000E-02	3.7000E-02	3.7000E-02	5.9000E-02	4.4000E-02	2.6500E-02	3.9300E-02	8.9200E-02	3.7000E-02	2.2000E-02	7.6400E-02	
o	0	0.2410	0.0210	0.0615	0.0740	0.0940	0.0980	0.1219	0.1381	0.1570	0.1803	0.2000	0.2130	0.2450	0.2620	0.2980	6.3358	0.3720	0.4310	0.4750	0.5015	0.5408	0.6300	0.6670	0.6890	0.7654	
	DA		ଡ. ଉଉଉଉE+ଉଉ	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	9.0000E+00	0.0000E+00									
Œ	0	M.3/28	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	0.3750	IO.	0.3220	
	Z		262	304	310	464	108	535	368	338	378	270	201	404	202	425	402	387	593	425	242	305	574	202	130	391	
CYCLES	(933	601	905	1215	1709	1817	2352	2720	3658	3436	3706	3967	4311	4518	4943	5345	5732	6325	6750	2669	7302	2876	8083	8213	8604	

Table 88. K _{MAX} Vs dc/dn Calculations - AFCG-6 Flaw 4	CRACK TYPE CODE,E= 2 GROSS AREA STRESS.= 8.500 HOLE DIAMETER,D= 0.3150 PANEL THICKNESS,T= 0.3750 00	
KMAX Vs dc/dn	AFCG-6 F4 RIES,M= 27 ROLE,B= 1 HOLE,B= 1 GRI 4.0000 MODULAS RATIO,R= 0.000	
Table 88.	TEST CASE ID AFCG-6 F4 # OF CYCLE ENTRIES,M= 2 # OF CRACKS IN HOLE,B= 1 FASTENER LOAD,P= 0.000 PANEL MIDTH,W= 4.0000 FASTENER/PLATE MODULAS R	NOTES:

	E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION—(D2C/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE—(D2C/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE—(D2C/DN) C=4,TWO CRACKS WITHIN THE FASTENER HOLE—(D2C/DN) C=4,TWO CRACKS WITHIN THE FASTENER HOLE—(D2C/DN) C=4,TWO CRACK OR CORNER CRACK(S)—T DIRECTION FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2	
01170	URFACE OR ORNER CRAI ORNER CRAI OR LOAD CRE OR THRI FECKS WITHER OR SECTION	-
all all all all all all all all all all	MOTES: E=1,FOR S E=3,FOR C E=4,COMBI B=0,SURFA B=1,SINGL B=1,SINGL B=1,SINGL B=1,SINGL B=1,SINGL B=1,FINGL	
L	5 	-

CYCLES		Œ		ပ		KMAX	Pro	
	K		H		2		X BBA	
339		.37					- FR - 18 - 1	Na/Sa
601	262	.37	0		.3000E		6.433	2.0229E-05
905	364	.37	ø		.2000E		6.648	2.6974E-05
1215	310	37	Ø		. BBBBE		6.884	3.2258E-05
1709	464	.37	ø		.1500E		7.194	4.3522E-05
1817	108	.37	ø		. SøøbE		7.420	1667E
2325	535	.37	ø		.6500E		7.628	9533E
2720	368	.37	0		.8500E		7.902	8272E
3058	338	.37	ø		.8500E		8.691	4734E
3436	378	.37	ø.		. 0500E		8.267	4233E
3786	278	.37	ø.		. 7000E		8.418	2963E
3987	201	.37	Ø		. 0300E		8.520	1244E
4311	404	.37	ø		.5700E		8,640	3614E
4518	202	.37	œ.		. 4000E		8.767	6.7633E-05
4943	425	.37	ø		. 8000E		8.889	5882E
5345	402	.37	Ö		.900E		9.645	2139E
5732	387	.37	ø		. 1999E		9.200	0103E
6325	593	.37	ø		. 4000E		9.411	1062E
6229	425	.37	ø.		. 5000E		9.652	9588E
2669	242	37	ø.		.900BE		9.833	1741E
7302	385	37	ø.		.9000E		19,662	2787E
2876	574	37	ø,		.5600E		10.323	4913E
8083	202	.37	ø.		.1400E		10,633	1.5169E-04
8213	130	37	0		30060;		10.777	1.6077E-04
8694	391	37	Ö		.1200E		11 044	1.82186 04
9075	471	0.3750	0.0000E+00	9.7766	7.7900E-02		-	
9243	168	37	œ.	0.8206	4.4000E-02	12.037	11.884	2.6198E-04

-6 Flaw 5		1.45	≈ 8,500	6000	0.3750
tions - AFCG		PE CODE, E=	GROSS AREA STRESS, S=	METER, D= 0.	PANEL THICKNESS, T= 0.3750
Table 89. K _{MAX} Vs d2c/dn Calculations - AFCG-6 Flaw 5		CRACK TY	GROSS AR	HOLE DIA	PANEL TH
MAX VS d		4.			
Table 89. K	TEST CASE ID AFCG-6 FS	# OF CYCLE ENTRIES,M= 24	# OF CRACKS IN HOLE, B= 0	RSTENER LOAD, P= 0.000	PANEL WIDTH, W= 10.0000

PANEL THICKNESS, T= 0.3750	E=1,FOR SURFACE OR THROUGH THICKNESS CRACK E=2,FOR CORNER CRACK(S), UNIFORM GROSS AREA STRESS E=3,FOR CORNER CRACK(S), FASTENER LOAD ONLY E=4,COMBINED LOAD CASE OF E=2 AND E=3 B=0,SURFACE OR THROUGH CRACK CONFIGURATION(D2C/DN) B=1,SINGLE CRACK WITHIN THE FASTENER HOLE(DC/DN) B=2,TWO CRACKS WITHIN THE FASTENER HOLE(DC/DN) A=DEPTH OF SURFACE CRACK OR CORNER CRACK(S)T DIRECTION C=HALF LENGTH OF SURFACE CRACK OR LENGTH OF CORNER CRACK(S) FILLED HOLE CORRECTIONS APPLIED ONLY IF E=2
10.0000	SURFACE CORNER C CORNER C SINED LOG SINED LOG CRACKS T CRACKS T CORNER C CRACKS T CORNER C CORNER C C C C C C C C C C C C C C C C C C C
MIDTH, W= 10.0000	MOTES: E=1,FOR E=3,FOR B=6,SUR B=1,SIN C=BE7TH C=HRLF FILED

	Ma ora	.1298E-0	.3882E-0	.4516E-0	.7845E-8	. 0000E-0	.1682E-0	.3207E-0	.7633E-0	.7143E-0	.7037E-0	5.9701E-05	.6832E-0	.7295E-0	.9294E-0	.1045E-0	. BBBBE-B	.2816E-0	294E-0	.7409E-0	.9672E-0	.3171E-0	. 7488E 6	-8418E-0
KANAX X												6.441												
КМЯХ	4.939											6.494										-		-
D2C		.2000E-	. 0300E-	.0700E-	-300E8.	.4000E-	.2300E-	.5900E-	.6100E-	.1600E-	.5400E-	1.2000E-02	-7000F-	- 6000E-	-3007E-	-6600E-	-8700E-	- 6000E-	.5000E-	-3000E-	- 9000G -	-3300E-	-30069.	.7600E-
	0.1074	.111	.116	.122	.131	.133	.145	.153	.161	.171	.179		.199	.207	.223	.242	.261	.299	.332	.353	.383	.450	.478	.497
ДA		. 0000E+	. 0000E+	. 0000E+	. 0000E+	. 0000E+	. 0000E+	. 0000E+	. 0000E+	· BBBBE+	. BBBBE+	9.0000E+00	. 0000E+	· BBBBE+	· BBBBE+	. 0000E+	· BBBBE+	. 0000E+	. 0000E+	. 0000E+	· BBBBE+	. 0000E+	. 0000E+	.0000E+
•	0.3750	8	.37	.37	.37	.37	.37	.37	.37	.37	.37	.37	.37	.37	.37	37	.37	.37	.37	37	.37	.37	.37	32
Z		262	364	310	464	108	535	368	338	378	270	201	404	207	425	402	387	593	425	247	305	574	202	130
CYCLES	339	601	905	1215	1709	1817	2352	2720	3058	3436	3786	3907	4311	4518	4943	5345	5732	6325	6229	2669	7382	2876	8683	8213
	-	N	ო	4	n	9	~	œ	0	10	=	12	13	14	15	16	17	13	19	20	21	22	53	24

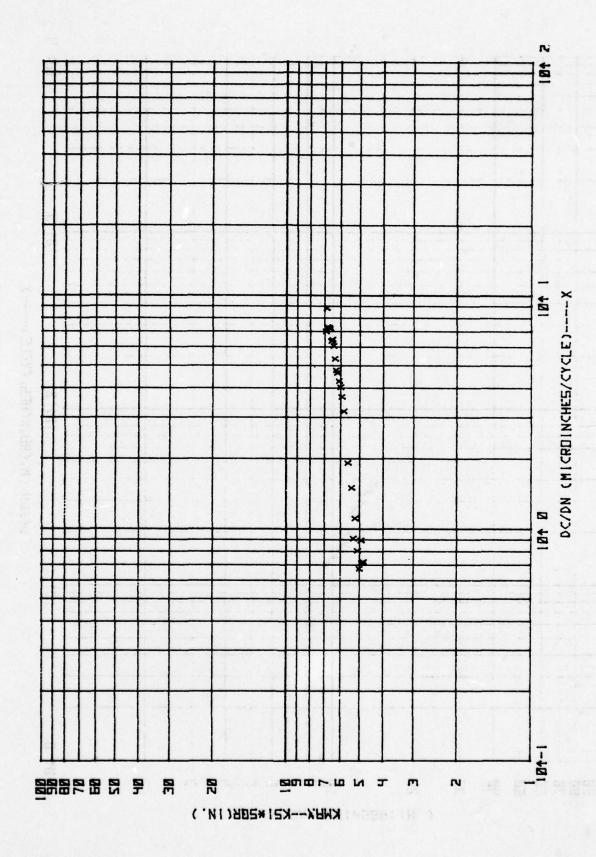


Figure 45. K_{MAX} Vs dc/dn Plot - AFCG-1 Flaw 2

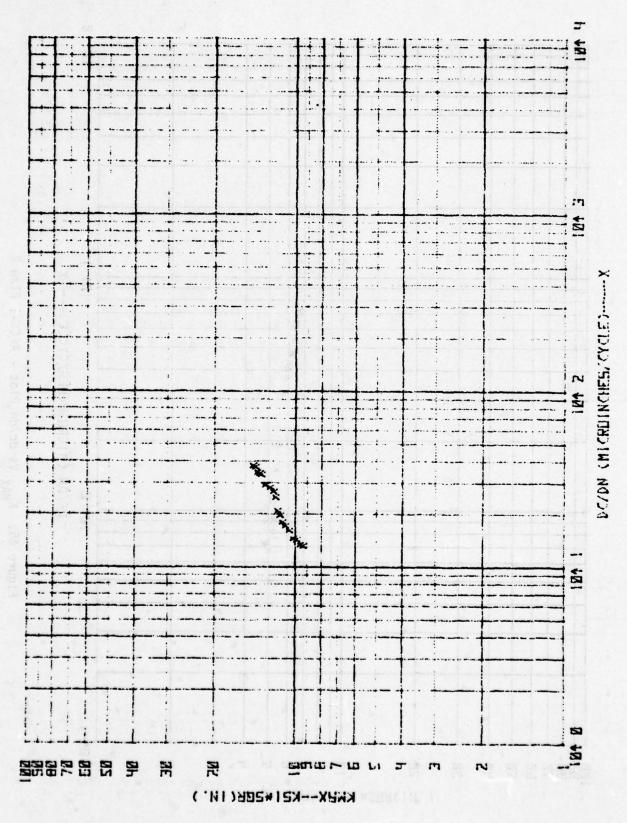


Figure 46. KMAX Vs dc/dn Plot - AFCG-1 Flaw 3

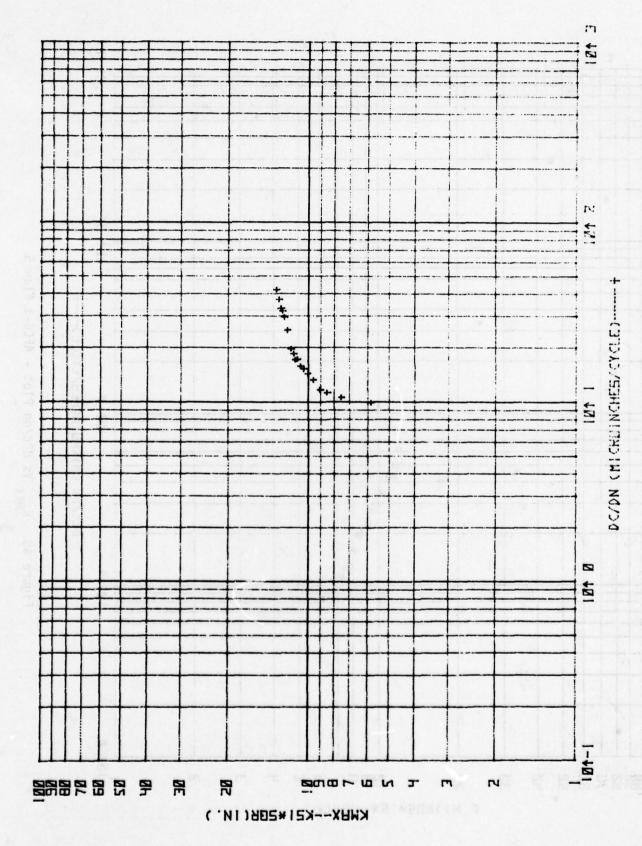


Figure 47. KMAX Vs dc/dn Plot - AFCG-1 Flaw 4

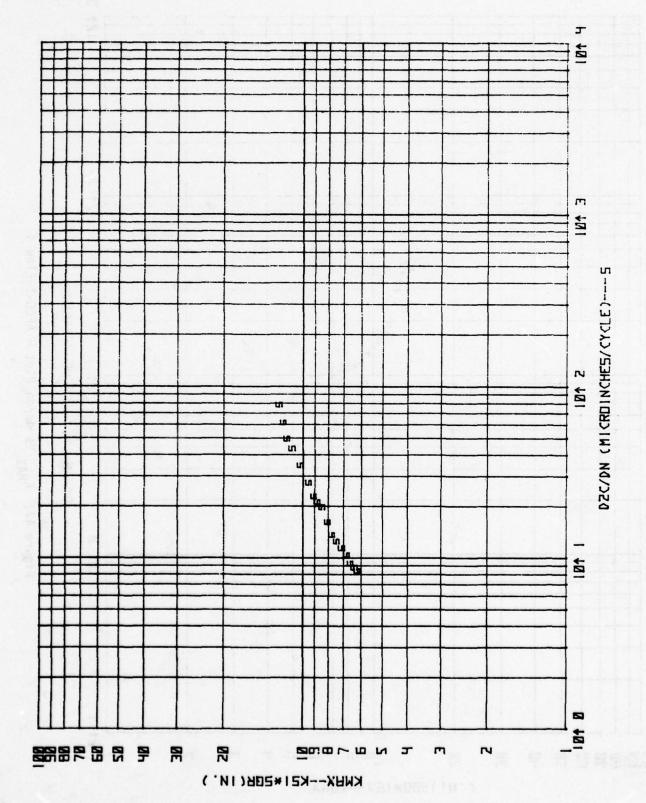


Figure 48. K_{MAX} Vs d2c/dn Plot - AFCG-1 Flaw 5

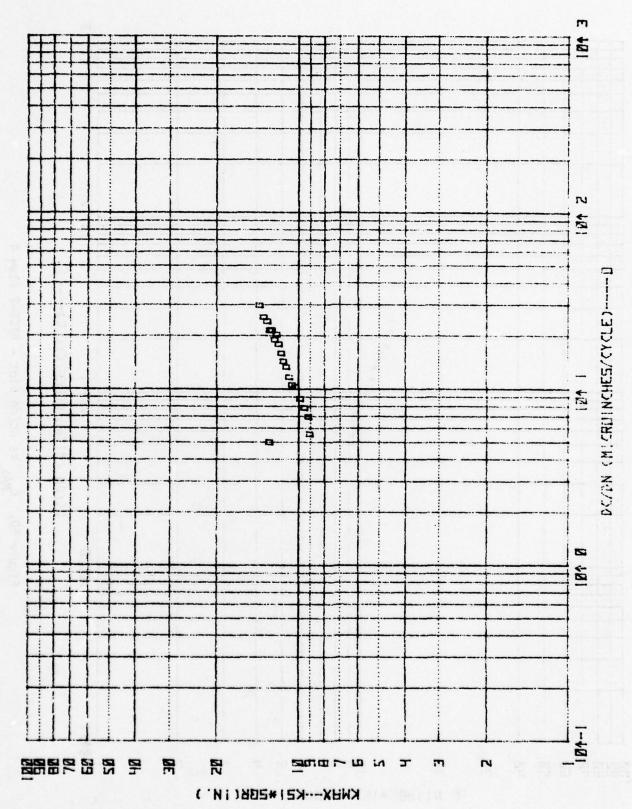


Figure 49. K_{MAX} Vs dc/dn Plot - AFCG-2 Flaw 3

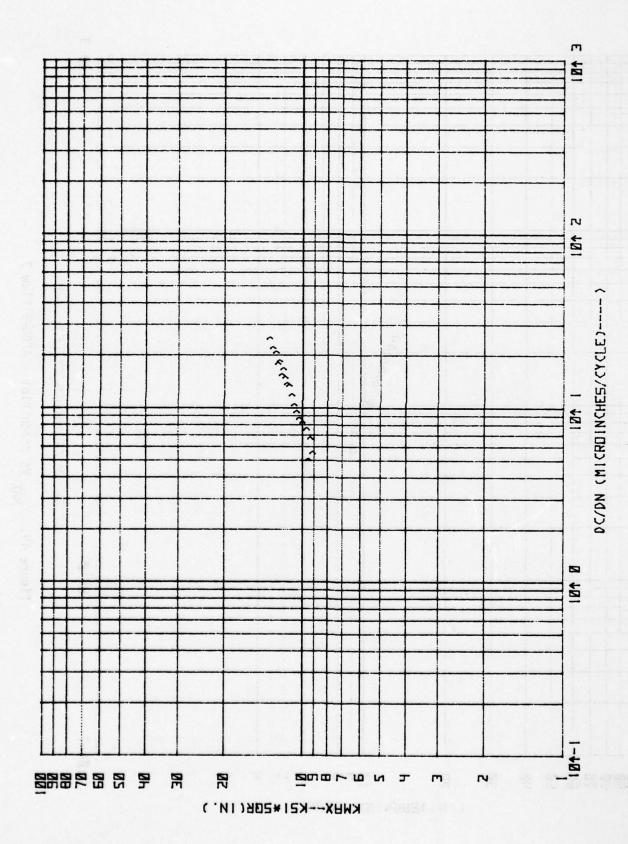


Figure 50. K_{MAX} Vs dc/dn Plot - AFCG-2 Flaw 4

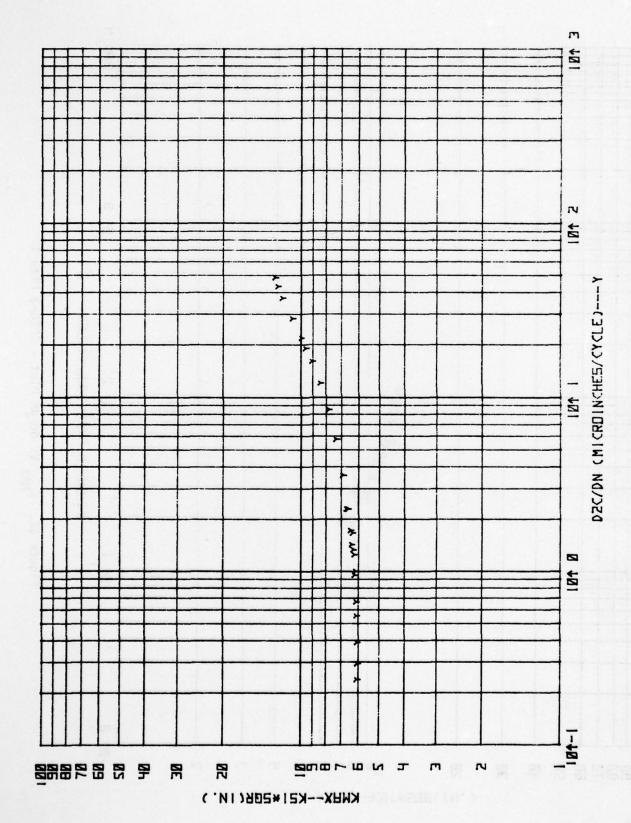


Figure 51. K_{MAX} Vs d2c/dn Plot - AFCG-2 Flaw 5

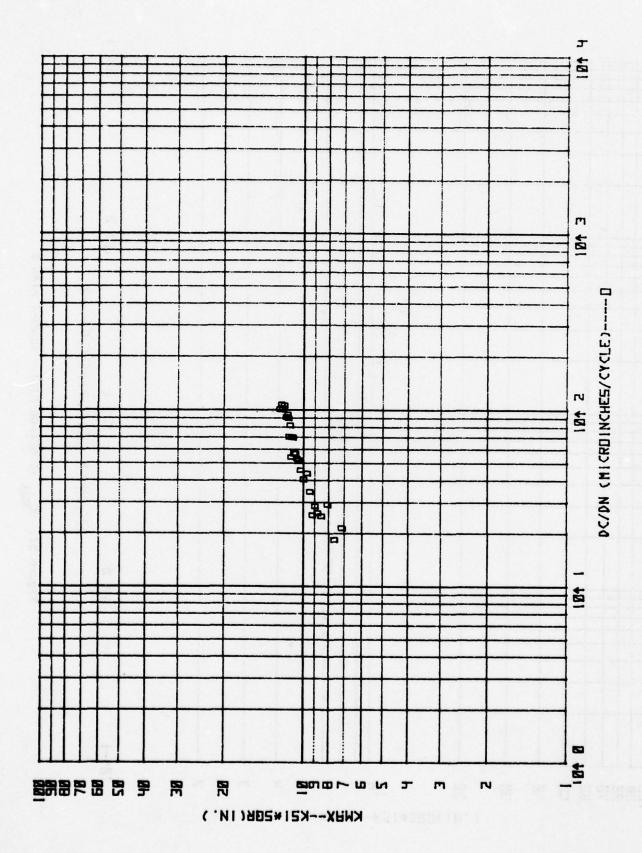


Figure 52. K_{MAX} Vs dc/dn Plot - AFCG-3 Flaw 1

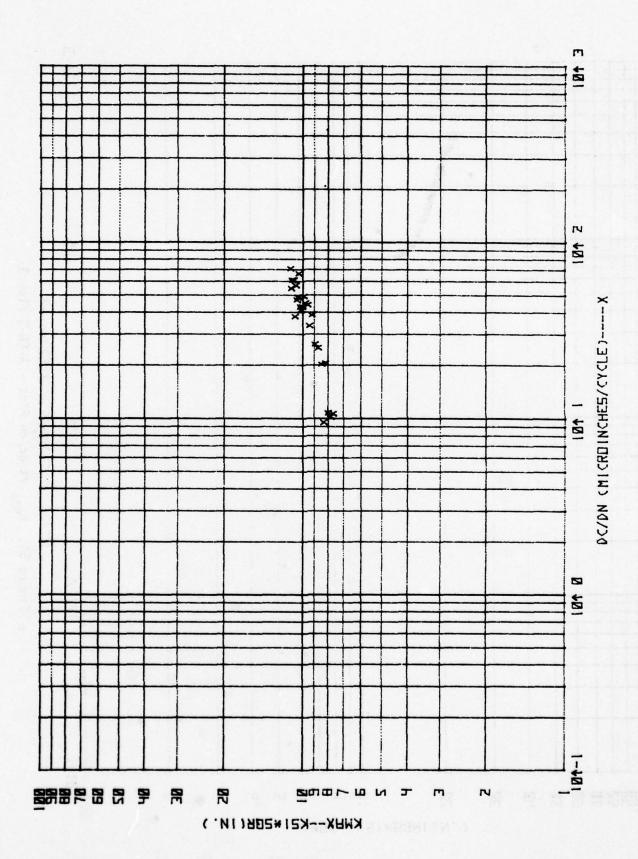
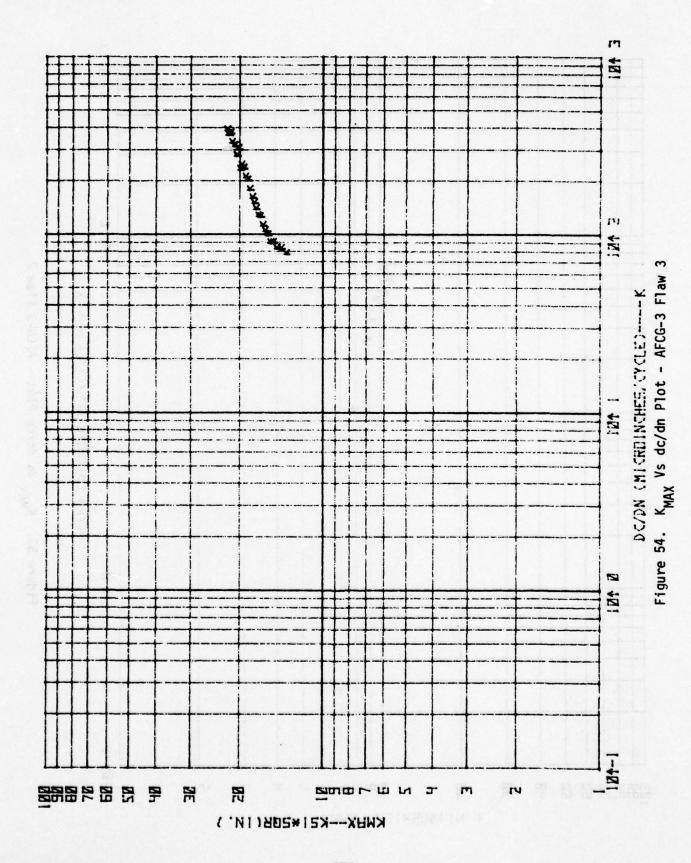
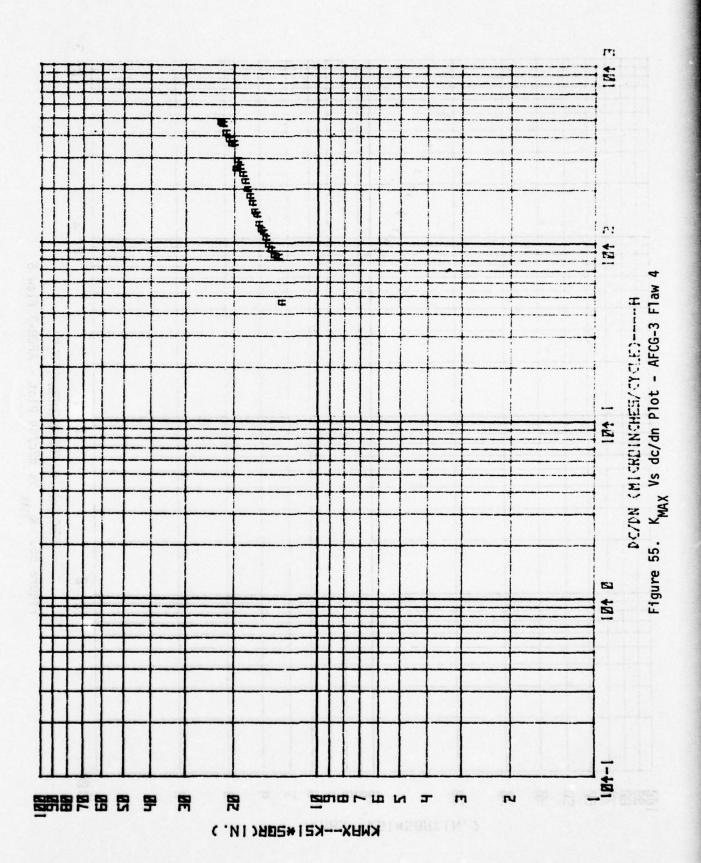
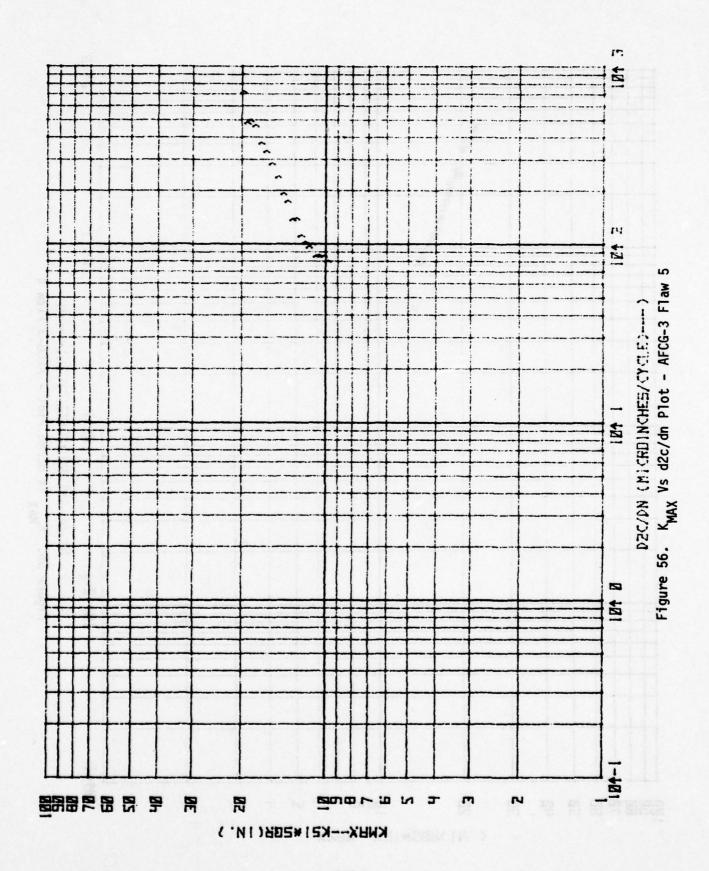
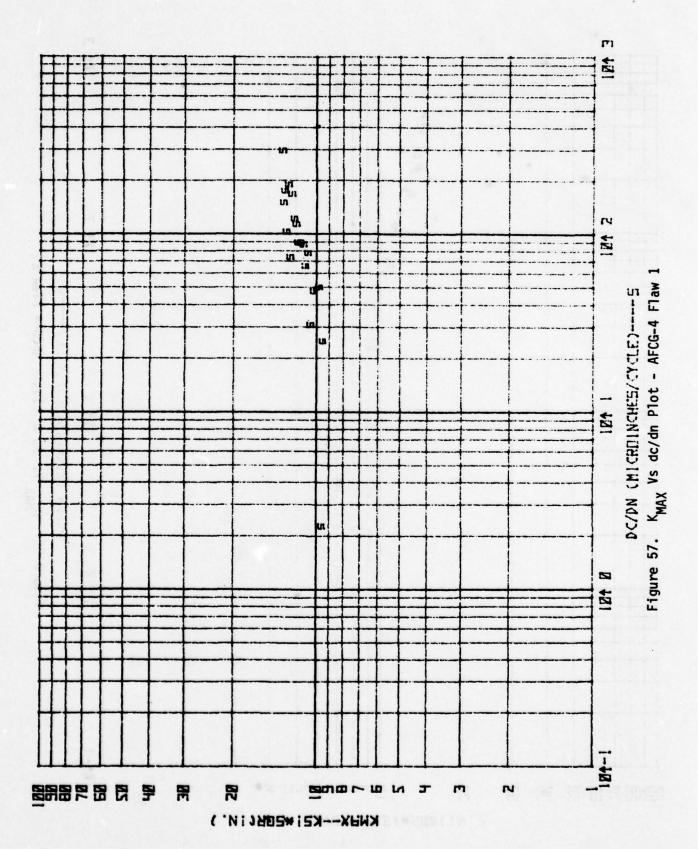


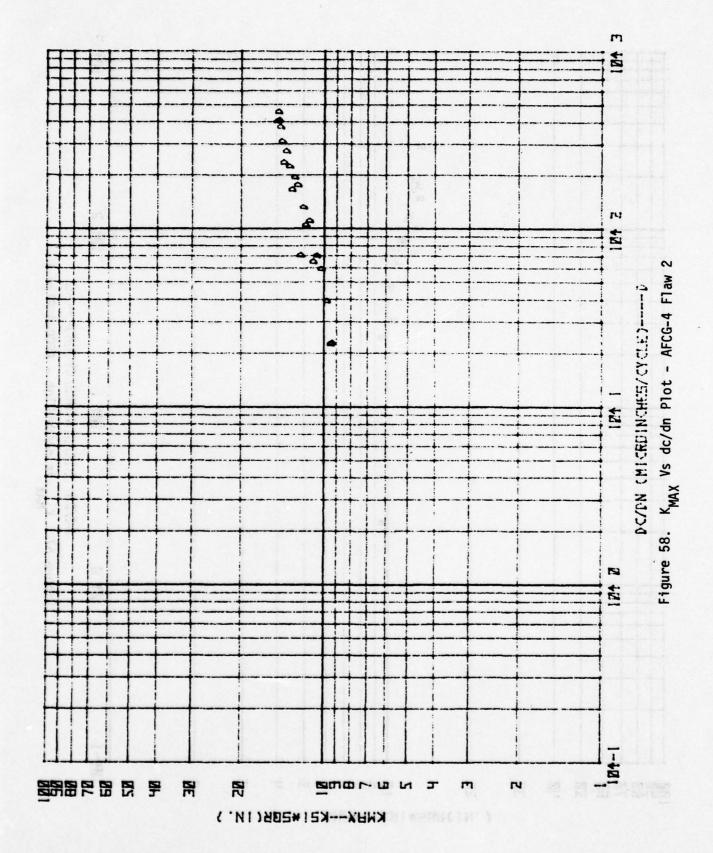
Figure 53. K_{MAX} Vs dc/dn Plot - AFCG-3 Flaw 2

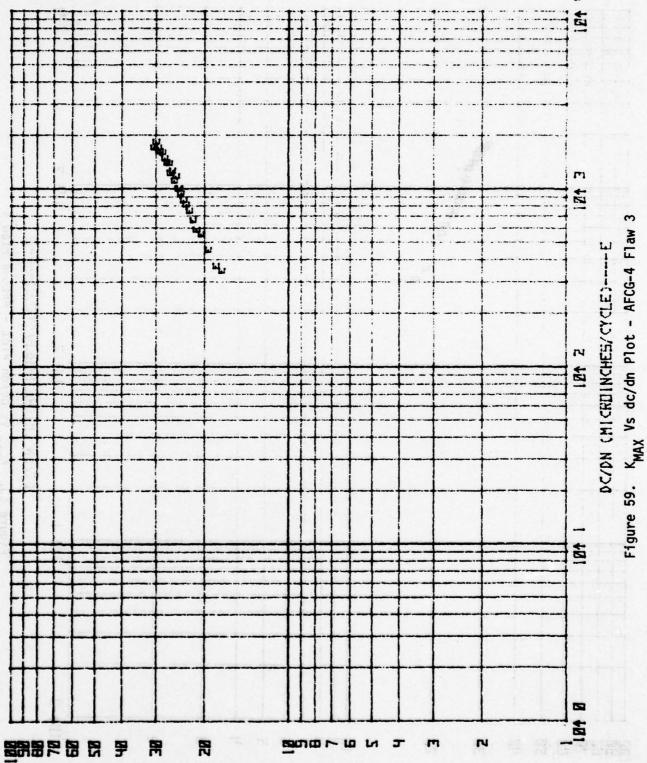


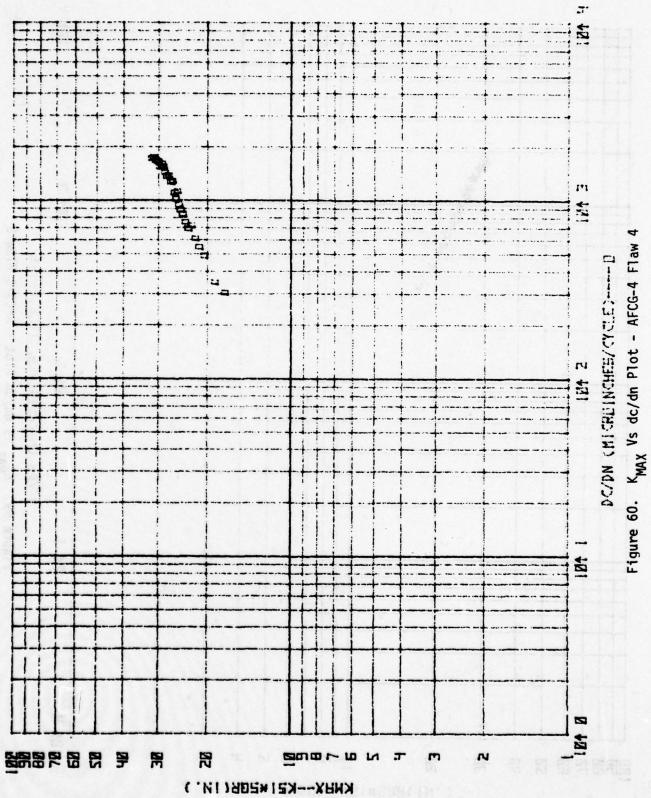












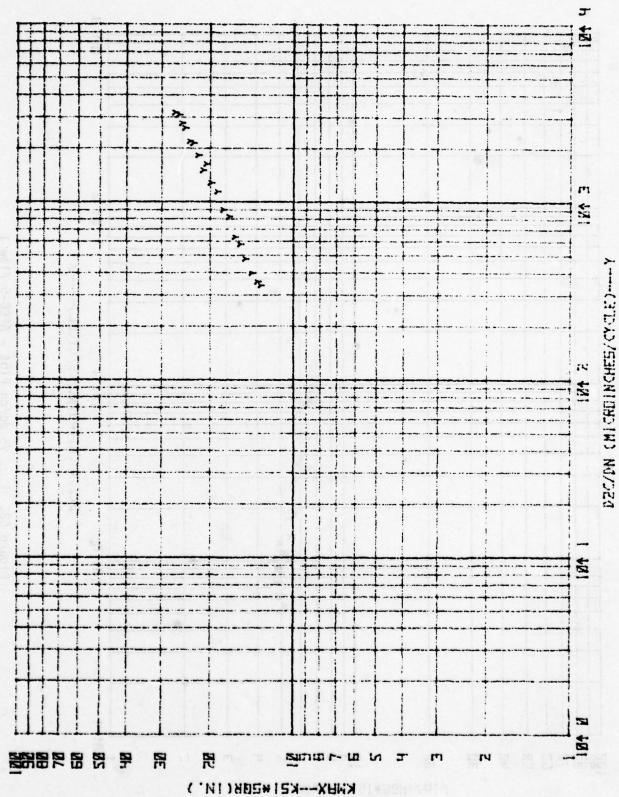


Figure 61. K_{MAX} Vs d2c/dn Plot - AFCG-4 Flaw 5

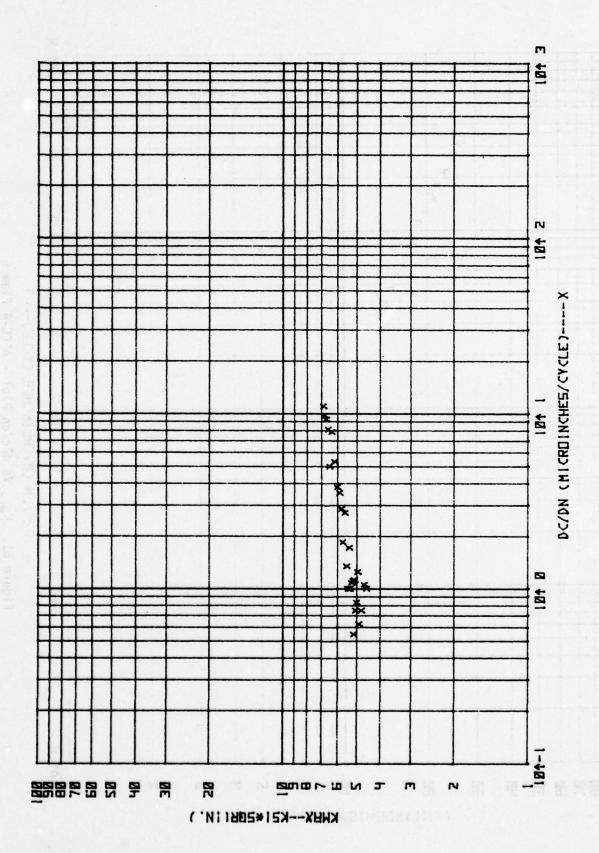


Figure 62. K_{MAX} Vs dc/dn Plot - AFCG-5 Flaw 1

Figure 63. K_{MAX} Vs dc/dn Plot - AFCG-5 Flaw 2

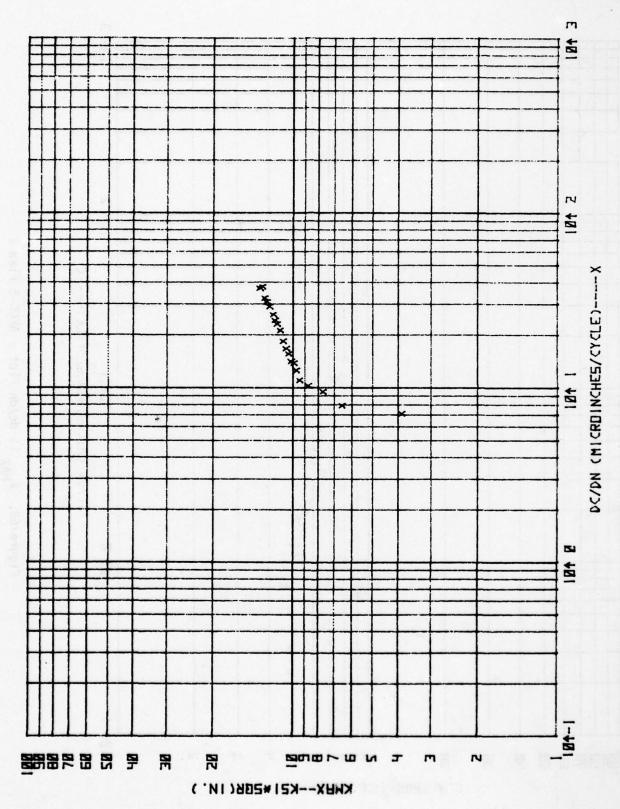


Figure 64. KMAX Vs dc/dn Plot - AFCG-5 Flaw 3

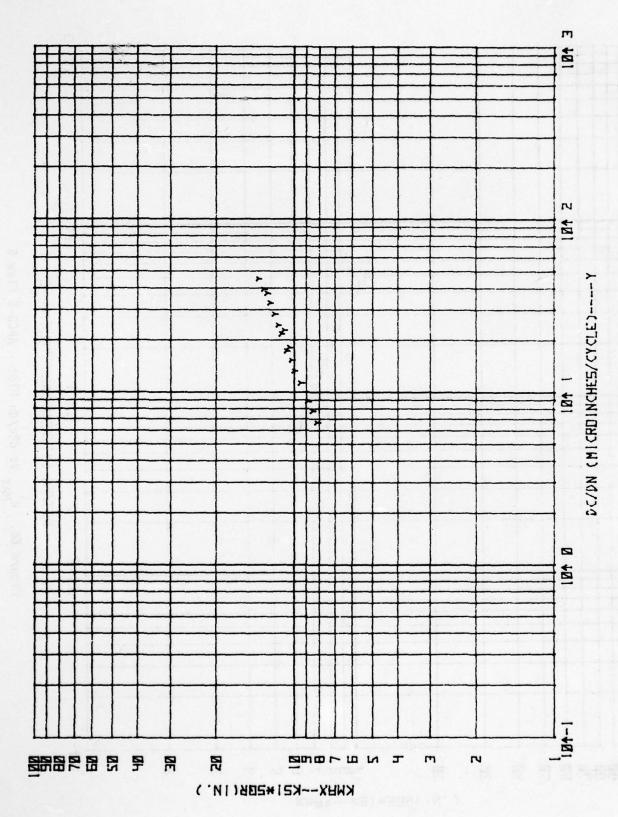
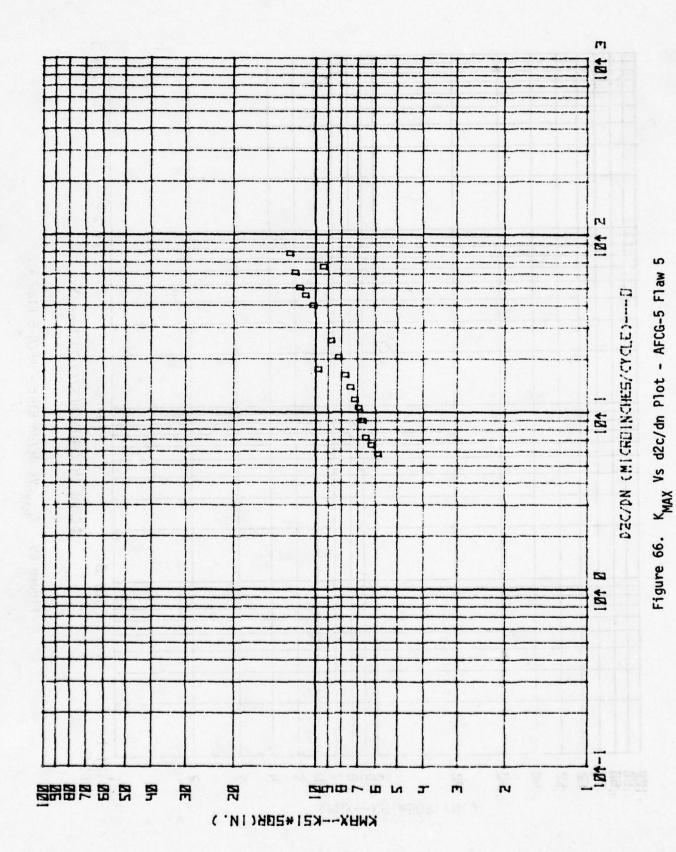


Figure 65. K_{MAX} Vs dc/dn Plot - AFCG-5 Flaw 4



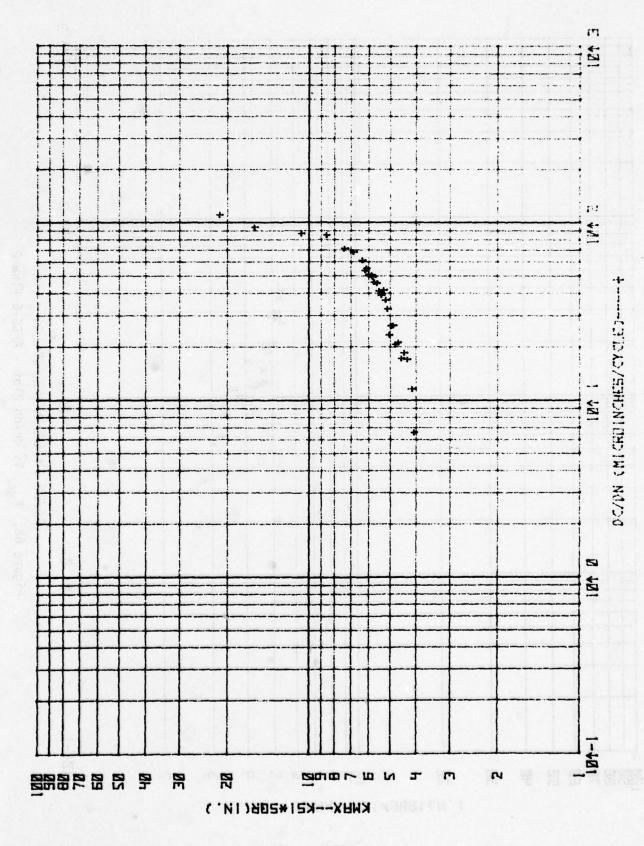
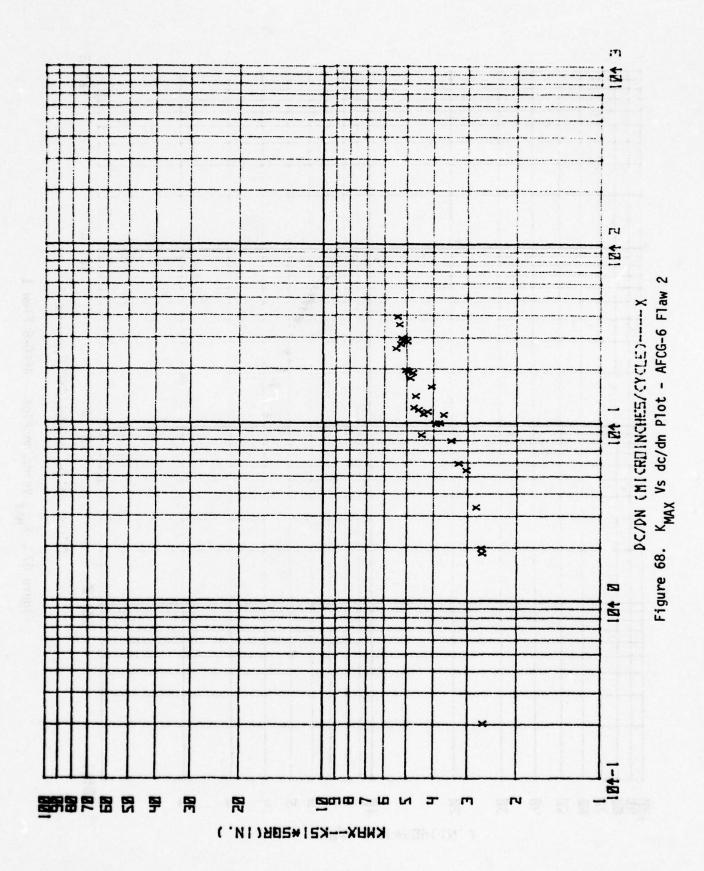
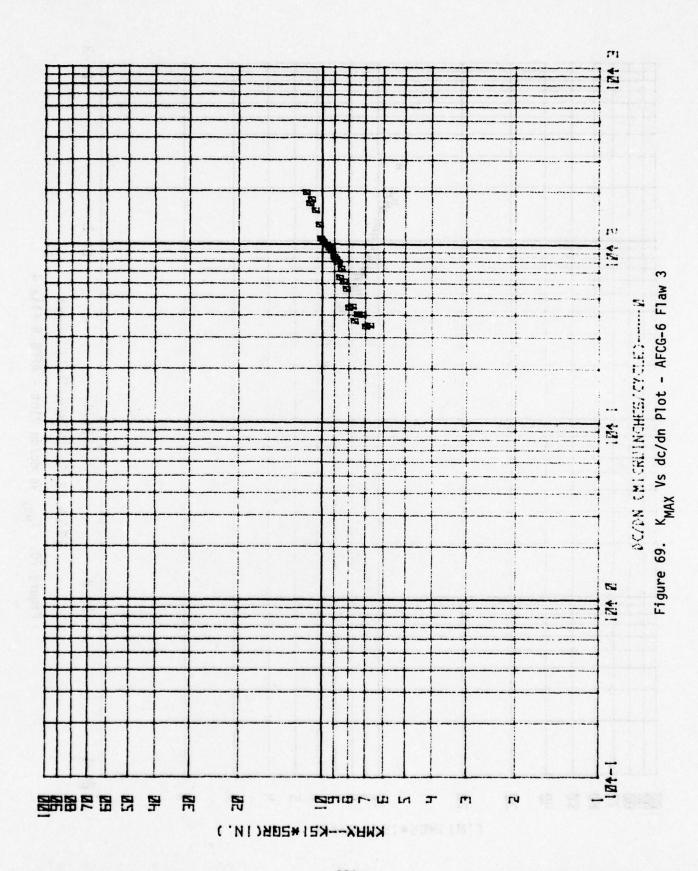
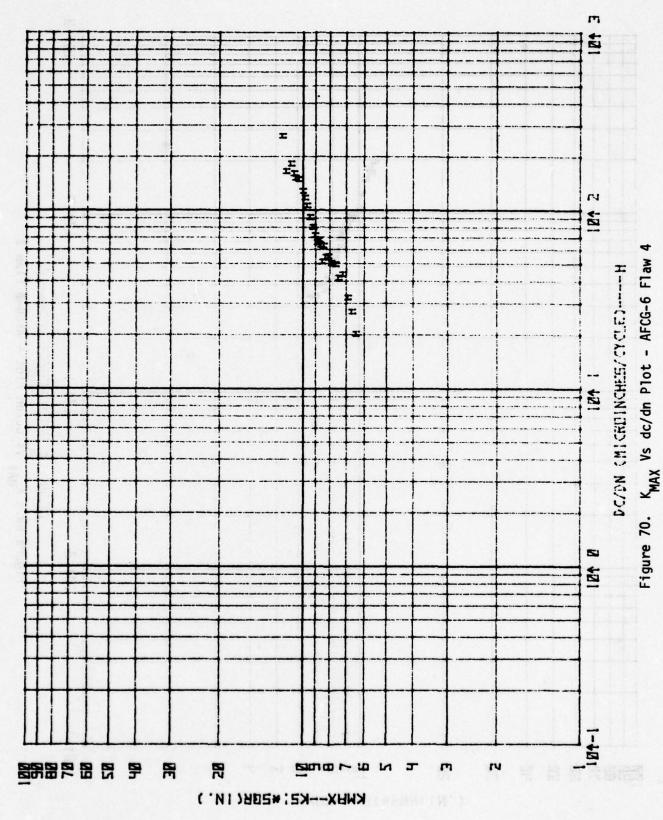
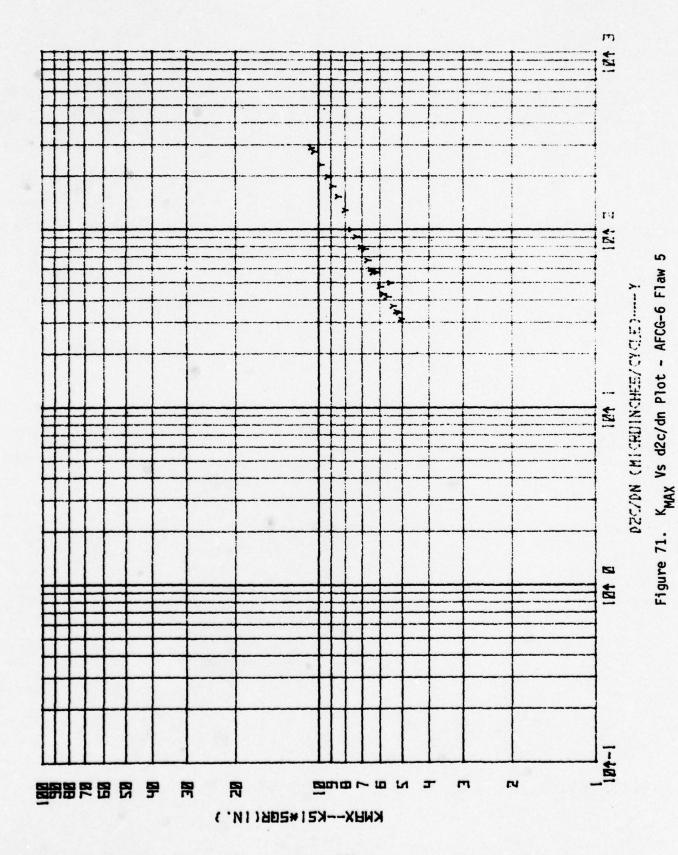


Figure 67. K_{MAX} Vs dc/dn Plot - AFCG-6 Flaw 1









SECTION VI CRACK GAGE MATERIAL da/dn TESTS

Six small coupon crack propagation tests were conducted to determine basic K_{MAX} vs da/dn properties of the crack gage material in the (.02 inch) thickness. These tests were conducted in load control. Figure 72 describes the small coupon details. Recorded test data of crack length and cycles is presented in Tables 90 through 95. A plot of crack length vs cycles is presented in Figure 72.

Calculation of K_{MAX} vs da/dn is presented in Tables 96 through 101. Log-log plots of K_{MAX} vs da/dn are presented in Figures 73 through 79.

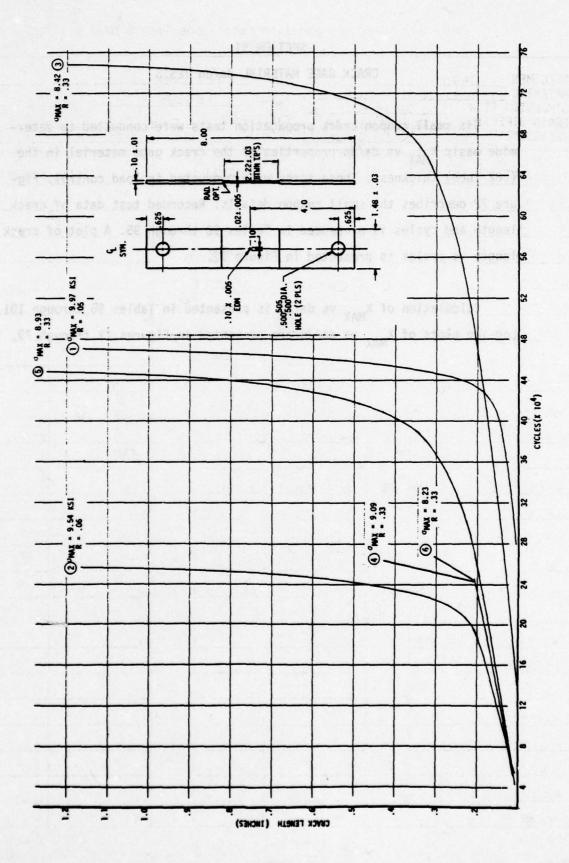


Figure 72. Thin Section Specimen Detail & da/dn Plot

Table 90. Crack Propagation Data - Specimen DADN-1

SPECIMEN	DADN-I	P _{MA})	292	LBS. A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A.A
MATERIAL DIMENSION (T	.W.) .0198 .	P	15	LBS.
GRAIN DIRECT	ION Longi		E RATE	5 Hz
				200 KIL- MTS, 4 KIP RANGE
(CYCLES/FLTS)	(INCHES)	(CYCLES/FLTS)	(INCHES)	(CYCLES/FLTS) (INCHE
EDM	.0959	464400	.7370	
391000	.1382	464900	.7620	9503 . 5043
400000	.1494	465500	.7910	1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
410000	1510	466000	.8230	1 133.41 1002.5
41.2000	.1860	466500	3533	Line / Ni sale
440000	.2460	466 900	.55.0	<u> </u>
441700	.25	467800	.9350	
443900	2755	468 300	.9650	
445800	4.55	468500	.9913	19.3. 1. 15.00
449000	.3212	465 800	1.0050	12.22. 12.82.
449400	.3240	469100	1.0525	1 1221 2530
450800	.3610	463700	1.0700	op Jakin I Saci
452600	.3940	470300	1.1028	
454200	.4240	470700	1.1470	4
455700	.4560	470 800	1.1590	I Jara Literati
456700	.4770	1816	0014	J - 1598 1595 8
457700	.4396		2503-	Lorga Ligata
458600	5250	1545.1	101921	190001 100001
459600	5500	LIZACLE	192124	P LOBUL LOCKER
460600	.5830	10	152 157	1 <u>1868</u> 1 1864
461300	.6070	15121	538.5	12021 12021
461900	.6297	19249 10	90534	1 10268 1 35069
462800	.6670	10018 LX	2111	There in good
463400	.2915	Larela	QUELK	1565 1 40815
463900	.7173	Literal Li	101321	1. 1995 1 100 80

Table 91. Crack Propagation Data - Specimen DADN-2

SPECIMEN MATERIAL DIMENSION (T GRAIN DIRECT ENVIRONMENT	ION Long	, 1.479 MIN	E RATE 5 H	BS.	RANGE
N (CYCLES/FLTS)	2A (INCHES)	(CYCLES/FLTS)	2A (INCHES)	(CYCLES/FLTS)	2A (INCHES)
EDM .	.0967	233800	.3842	254500	.9457
55600	.1070	235000	.3983	455000	.9745
75600	.1209	236200	.4142	255400	1.0075
82500	.1258	237400	4260	255 700	1.02%
104400	.1417	232600	.4439	255000	545
121000	.1528	239900	.4603	250:00	1.00
134000	.1641	241000	.46.0	25.400	1. 0 3
143200	.171.	142000	4.1.6	256500	1.1209
159000	. 1810	243590	. 5190	256700	1.1459
169900	.1890	244000	.5450	250800	1.1641
181800	.1992	245000	5640		
196200	:146	245900	.5929		
205100	:40	246800	.6110		
211000	.2352	247700	64.54		
217600	.2575	248.00	.6665		
222700	.2893	249500	.6976	1	
123900	.2970	250200	.7239		
225000	.3050	350800	.7450		
226000	.3130	251300	.7681		
227000	.3224	251800	.7903		
228000	.3302	252500	.3213		4,50
229000	3370	253000	.8434		
230200	.3465	253500	.8700		
231400	.3607	253700	.8860		
232600	.3691	254100	.9110		

Table 92. Crack Propagation Data - Specimen DADN-3

SPECIMEN	DADN-3	PMA)			V Bright
DIMENSION (T GRAIN DIRECT ENVIRONMENT	.W.) <u>.0201</u> ION Longi	, 1.480 MIN	E RATE 3	HE. HIP - MTS, 4 KI	O RANGE
N (CYCLES/FLTS)	2A (INCHES)	(CYCLES/FLTS)	2A (INCHES)	(CYCLES/FLTS)	2A (INCHES)
EDM	.0976	629100	.20%0	727 800	.032
137000	.1010	639700	.3000	729300	.652
171500	.1100	659300	.3264	732400	.6895
184700	.1089	667100	3338	733500	.7029
199600	.1170	671800	.3450	734700	7312
230500	.1247	677500	5549	735×20	.7502
264700	.1343	6V 2 200	.3695	737400	7814
274300	.1345	655800	.3775	738500	7397
284700	.1514	690100	.3930	139600	.828
297700	.1442	693600	.4010	740300	.850
334000	.1542	626 200	.4145	741200	.8760
348700	.1572	639000	.4235	742000	379
362900	.1635	701900	.4400	743000	.9299
390000	.1740	703300	1114	743500	.950
411700	.1831	705000	.4545	744200	.972
420900	.1840	706800	.4631	744600	.9894
439300	.1900	708700	.4734	745500	1.000
460800	.1980	710500	.4850	745900	1.0172
473000	.2118	711900	.4949	746400	1.047
498500	.2130	713400	.5023	746900	1.0915
537800	.2320	715700	.5200	747300	1.1153
564800	.2460	718500	.5461	747700	1.1375
587600	.2608	720800	.5644	748000	1.1621
609500	.2760	723500	.5859	748400	1.1973
617400	.2825	725400	.6068		

Table 93. Crack Propagation Data - Specimen DADN-4

SPECIMEN MATERIAL DIMENSION (T GRAIN DIRECT ENVIRONMENT	DAON- 4 7075-TG51 (W.) 0186 ION Longi 95% + Rela	P.478 P. tudinal C.tive Humidity	MAX 250 LB MIN 82.5 CYCLE RATE 5 NACHINE 200	BS. HZ. D KIP-MTS, 4KIP	RANGE
N (CYCLES/FLTS)	2A (INCHES)	N	S) (INCHES)	(CYCLES/FLTS)	the same of the sa
EDM	.0994		50.00	Hara I	Mda
91500	.1048		0.000	low.	SPORE
103600	.1356			GAIL	098/6
120800	.1439			lesc.	0.0749
176700	.1708			Heat.	
195200	.1800				
120500	.1934				
145600	-2076				06404 950494 900794
				55521	narus Speno
			103/200	000	504064 304064
				Internal	000/E4 20/2/2010
			30390	6.85	
		Lazon			001673

Table 94. Crack Propagation Data - Specimen DADN-5

MATERIAL	DADN-5	P _{MAX}	250	.5 LBS.	ngelt blanz De De De De
DIMENSION (T GRAIN DIRECT ENVIRONMENT		tudinal CYCL	E RATE	B HE.	PANGE
(CYCLES/FLTS)	2A (INCHES)	(CYCLES/FLTS)	2A (INCHES)	(CYCLES/FLTS)	2A (INCHES)
EDM	.0965	401200	.3900	443600	.9353
24000	.1066	403900	.4029	444200	. 355
43600	.1070	405700	.4111	445000	.930
76500	.1210	408800	.4310	445400	1.023
103600	.132%	410700	.4400	445900	1.0250
129800	.1431	412600	.4550	446700	1.075
141800	.1496	414200	. 4645	447100	(*)
167900	.1580	115000	.4763	447500	1.142
201300	.1740	416500	45:0	447800	1.1579
230000	.1884	417600	.4372	448300	1.203
250700	.1390	418300	.5058	448600	1.2471
268500	.2074	421500	5292		
303300	.2310	423600	.5500		
319000	.2434	425600	.5750		
329300	.2530	4:2300	.6006		
343000	.2675	430600	.6400		
352700	.2780	433300	.6660		
358500	.2860	434800	.7115		
367800	.3010	436000	7339		
373300	.3100	437700	.7660		
378500	.3200	439500	.7931		
384200	.3340	439700	.8144		
390000	.3494	441100	.8579		
394600	.3638	442000	.8780		
398100	.3778	442800	.9000		

Table 95. Crack Propagation Data - Specimen DADN-6

MATERIAL TO THE PROPERTY OF TH	DADN-6 7075-T651 .W.)0206 .IONLongi 95% + Rela	1490	PMIN	250 15 RATE NE20	LBS.		PANFE
N (CYCLES/FLTS)	(INCHES)	(CYCLES/F	LTS)	2A (INCHES)		(CYCLES/FLTS)	2A (INCHES)
EDM	. 0978	Lanes		x 10 x		1.6353	MC?
52000	.1106			25.01			
63400	.1154						d Beering
89800	.1271	1000					
116000	.1392			18.74			each.
136300	.:490						322
161602	.1618						
166200	.1645			2			
		i cal.		0.004 0.004 0.004		10810 1082 10108	
				31.821.			
				0 : = 4 32 : 34 A			9634E3

Table 96. K_{MAX} Vs d2c/dn - Specimen DADN-1

Table 97. K_{MAX} Vs d2c/dn - Specimen DADN-2

				VAL					
		TEST CR # OF CY FASTENE PANEL W	CASE ID CYCLE ENTR CRACKS IN ENER LOAD,P	DADN-2 RIES.M= 38 HOLE.B= 6 P= 0.000		CRACK TYPE CODE, GROSS AREA STRES HOLE DIAMETER, D PANEL THICKNESS,	# \$ \$ # • \$ #	1 = 4.548 8888 6.8177	
	CYCLES	ä	Œ	Ä	O	120	КМЯХ	50 00 00 00 00 00 00 00 00 00 00 00 00 0	
	55600		9.91		000		0.0 0.0 0.0		D2C/D
	22500	99997	2)(Z		5. Bess	1.3900E-02	271.4	4 4 20 0 4 - 20 10	6.9588E-8
	164466		0.01	. GOOGE +	0	5966E-8	4.526	4.00.00.00.00.00.00.00.00.00.00.00.00.00	2603E
10	121000		0.01	. 0000E+	Θ.	1100E-0	4.705	4.616	.6867E
	134666		9.0	. 0000E+		1300E-0	4.881	4. V-0 W(0)	
	159000		90	. GOODE +	202		, m	ታ [ማ ር . ማ ር .	. 5655F
	169900		0.01	. 0000E+	(2)	BBBBE-B	5.201	0.100	.3394E
0	181800		0.01	. 0000E+	(2)	B3BBE-B	0.000 0.000	സ രം വ	.655E
_	196200		9.91	. 0000E+	-:	5386E-8	5.612	5.505	.0625E
	205100		0.0	. 0000E+	-:	4000E-0	5,740	10. 10. 10.	.0562E
· ·	211000		200	. NONUE +	-: -	4200E-0		വ. നെ വ	. 4068E
+ 10	222788		90	. 8888E+		1000010	7000 1000 1000	0. 000 000 000	. 4747t.
	223900		0.01	. 0000E+		7000E-0		000 000 000	4167E
	225000		0.01	. GOODE+	-	ด-30000 ด	6.782	6.732	.2727E
00	226000		0.01	. 0000E+	7.	9900B	6.880	6.831	. BBBBE
•	228000		0.01	.0000E+	-:	7200E-0	7.090	6.985	.6000E
Θ.	231400		9.91	. 0000E+	-:	0500E-0	7.456	7.273	.9706E
_,	233888		80.0	. 0000E+	-:	3599E-8	7.736	7.596	.7917E
	220000		200	GOOGE +	a c	DENDER - D	000 200 200 200	ი 1 ი. აქი	. 2000E
	241000		0.0	. 9999E+	1 60	3188F-2	0 C		. 5875F
10	243000		0.01	. 9999E+	ed	7000E-0	000	9.111	.8500E
10	245000		9.01	. 8888E+	ea.	5000E-0	9.881	9.607	.2500E
	2468999		800	. 8888E+	69.0	7000E-0	10.471	10.176	.6111E
n	248688		9.0	. NUNNE +		STANKE - B	11.199	18.835	. 0833E
	251299		20	. BUBBET		/3888-12 43668-10	00 J	11.0000	.5813E
	0000000		200	GAGAE+	. 7	012000100000000000000000000000000000000	0.00 0.00 0.00 0.00	10.00 00.00 00.00	40000
	253500		0.0	. 0000E+	. 7	8700E-0	14.366	000 000 000	. 8700E
~	254100		0.01	. 0000E+	4	1000E-0	15,151	14,759	.8333E
+	255466		0.01	.000E+		6500E-0	17.321	16.236	.4231E
10.	256188		0.0	. 0000E+		8400E-0	18,940	18.130	.3429E
	256588		9.01	. OOOOE+		4900E-0	58.773	19.856	.3725E
	2007000		200	. UUUUUE+		OLDME-B	1.745	21.259	.2550E
2	200000		0.01	. BBBBE+		SZEDE - E	710.25	22.131	.8200E

Table 98. K_{MAX} Vs d2c/dn - Specimen DADN-3

	4	ø		
-NOH	ES, M	CRACKS IN HOLE, B=	NER LOAD, P= 0.	MIDTH, W= 1.4880
EST	P	40 #	ASTE	ANEL

	±0.54		
			00
	11	9999	0.019
11	00	3	11
ü	0		-
111	00	-	(0)
百	Ē		00
3	STRESS,	H	7
		DIAMETER, D=	X
T T	E	풀	H
7	AREA	王	I
		Ē	•
X	00	HOLE 1	П
T	ė	三	至
8	5	¥	4

994488448886844888888888888888888888888	0-35E-6
A	
X 0.00004444444 $0.00000000000000000000000000000000000$	0.00 0.00
$2 \times 7 \times 2 \times 1 \times 1 \times 1 \times 1 \times 2 \times 1 \times 1 \times 1 \times 1$.7100E-0
$\begin{array}{c} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} \mathbf{a} a$	••• ••0 ••0
	. 00000E+0 .0000E+0
WARRERONNELLARENNANTH	20
↑ 11112222233333333333333333333333333333	6966 4126
#	

Table 98. K_{MAX} Vs d2c/dn - Specimen DADN-3 (Continued)

######################################	CAC CAC ENER BOOM	E ID- CKS I CORI LOAL DIH:5	DADN-3 4TRIES,N= 41 1N HOLE,B= 4 1,P= 0.808 1= 1.4888 01 0.8888E+88	•		3. Test	3.420 5608 8.8198 13.619	1
	999	0.0201	0 0	6. UBBBB	4. ASSBE-62		14.041	10001E-00
	996	0.0201	Ø		.7200E	· O		24445
	500	0.0201	D		4380E	18.01G		SEPUF
-	100	0.9201	Ð		. BEUBE	(2)	1	4197
	400	0.6261	Ø		BOOKS.	0.	()	0.000000000000000000000000000000000000

Table 99. KMAX Vs d2c/dn - Specimen DADN-4

CRACK TYPE CODE,E= 1 GROSS AREA STRESS,S= 9.090 HOLE DIAMETER,D= 0.0000 PANEL THICKNESS,T= 0.0186	DEC	4.01.7	8.2000E-03 4.346 4.281 4	2.7000E-02 4.748 4.547 4	9.2000E-03 4.878 4.813	1.3400E-02 5.064 4.971 5.	TO CONT. TO COUNTY OF THE CONT. THE
ES,M= 6 OLE.B= 0 0.000 1.4780	Ð		. BBBBE+B	0.0000E+00	. BBBBE+B	. OBOORE+O	BEBBBE+8
YCLE ENIKIES,M= RACKS IN HOLE.B ER LOAD,P= 0.0 WIDTH,W= 1.478	Œ	Ø.9186		9810	0186	9186	9186
OF COF COF COF COF COF COF COF COF COF C	E		17200	55900	18500	25300	25100
	CYCLES	163690	120800	176700	195200	220500	245600

2
¥
DADN-5
-
E
Ċ.
Specimer
=
2
d2c/dn
/s
₹ X
100
a

		DOC-DN PSSSE	28E	.3254E-8 .0000E-8	.2184E-0	.7198E-0	6377E-0	.2809E-0	.7816E-0	. 00001 00001 00000000000000000000000000	2004FT-5	.0825E-0	.3793E-0	.6129E-0	.6364E18	. 4561E-6	.6552E-0	.1304E-0	.0000E-0	6889F-B	4194E-0	.3158E-0	.8750E-0	.5641E-0	. 0000E-0	. 9848E-8	. 2000E-6	. M@10F16	.5294E-0
8.936 666 6189	Ж В В С В В С В В С В В С В В С В В В В В	ų,		- Z	4	J. Z	00.	(D)	٠. ا	უ. ის	- 0. 0 60	100	F6.	. i		0 O	7.0	ლ	ණ.ර ලා ර) (\ 	4	.88	.13	्। च	~	D (10	. U	00
ADN-5 ODE, E= 1 TRE55, = R, D= 0.00 ESS, T= 2.	KMAX		000	57 15	· ·		(O)	5	4.	0	0 C	000	.1.	D:	4. P		100 100	ē.	(4) () (-1) ()) (O	5	(S)	(U)	00	す (00 (000	0.0	् च 	
Specimen D	n 2 C.	0 1 0 0	1.1200E-02		BOBE-6	8 2 2 2 2 2 3 4 5 5 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5 7 5	.6988E-0	.4000E-0	· SESSE-S	NASCETTE ABSSETTS	. 4555AF-5	. NSONE-A	. 6686E-6	. 5666E-6	. 222227-0	· ABBOTHE.	.5480E-0	.4400E-0			.9900E-0	. 4000E-6	.1300E-0	.9500E-6	0.000E		. USBERT 6	0 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	. 696666-0
KAX Vs d2c/dn -	O	6.6500 9600	960	202	679.	20 (2 (2) (4) (3) (4)	0.00	160	· · ·	NO.	100	139	.143	001.	001		174	. 1 0	00 U	100	215	225	(N)	D'N	11 C	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00	1000) ()) ()) ()
ADN-5 ES.M= 50 OLE.B= 8 0.888	H	គុធភាពក្នុង	BRABE	. 8888E+8 . 8888E+8	. 0000E+0	. BBBBBH+B . BBBBF+B	. BBSBE+6	. BBBBE+0	9490000.	2442222. 22222142	. 0000E+0	. BBBBE+B	. OBOOE+O	. 9999E+6	. 86686E+5	. 0000E+0	. BBBBE+B	. GGSGE+G	9+38888 88888 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	. BBBBE+B	. BBBBE+B	. 8888E+8	. 0000E+0	D+HMMAN.	. 22000H+2	24422224. 20022442	04400000.	SANDON -	. 0000E+0
E ID- LE ENTR CKS IN LORD, P	Œ	6.6109 6.0109	0.0189	55	9	55	. 01	. 91	50	200	5	.01	<u>.</u>	<u>a</u>	5.5	90	. 81	9	2.0 2.0 0.0 0.0	.0	9.	. 91	9	5	50	56	5 6	5 5	0.0100
EST CAS OF CYC OF CRA ASTENER ANEL WI	Z	000	27100	2000 000 000	619	7. O 7. O 7. O	070	180	4 (0) (0)	0 0 0 0 0 0	900	978	80		200	30	80	9	10 m	000	9	89	4	500	000	0 0	200	2.0	20
⊢##Lû.	CYCLES	43688 76588	936	00 cc	679	0000	587	685			14	527	S S S S	0/0 0/0 19/0	900 900	- 00 0 4 0 4	906	940	2 0 0 0 0 0 0	057	689	126	961	D (0)	000	0 V 0 V 0 V	000	0 0 0 0 0 0 0 0 0	323

Table 100. K_{MAX} Vs d2c/dn - Specimen DADN-5 (Continued) TEST CASE ID-- DADN-5

	PASTENCE PROFESTER	CKS IN CCKS IN CLORD, P	.nun-c LES,M= 58 HOLE.8= 6 - 0.688 1.4838		CRRCK TYPE GROSS AREA SHOLE DIAMETE	C005.E= STRECS.S ER.D= 0. MESS.T=	1 = 8.938 6688 6. 81 89	S
CYCLES	Z	Œ	Æ	ပ	D 2C	КМЯХ	; ; ;	D2C/DN
434800	2588 1288	6.6189 6.6189	0.0000E+00	0.3558 2.3578	.5500E-	⊕ 0.	10.762	200
437700	-	.018	. BBBBE+B	.383	.2100E-0	1.88	1.58	2000 2000 2000 2000 2000 2000 2000 200
439700	- 0		. 0000E+0	244 504	. 8466E-6	0.0 0.0		.4200E-8
442000		.018	. 0000E+0	10.4	.0100E-0			.2333E-0
442800		.018	. BBBBE+B	450	.2000E-0	10 m	0.15	.7500E-0
443600 444200		018	. ଅପସସମ + ପ . ଅପସସମ + ପ	. 465 677	000E-0	4.0 0.0	44.00.00.00.00.00.00.00.00.00.00.00.00.0	80E-9 67E-9
445000		.018	. GBBBE+B	.490	.SØBBE-8	5.76	(T)	.3750E-0
445988	•	ω. ω.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ.σ	. 8888E+8	.510 010	. 5868E-6	0.00 0.00	6.18	. 8889E-0
447800		010	. 00000E+0	7.0 0.0 0.0	0-10010. 00000H-0	N IV	70 G	.7583E-8
448200		.018	. BBBBE+B	.601	.5500E-0	10. 10.	-1 (.1375E-0
448600		.018	.0000E+0	.623	.3700E-0	5.13	00.00 00.00	.0925E-0

Table 101. KMAX Vs d2c/dn - Specimen DADN-6

	TEST CP # OF CP FHSTENE PANEL U	CASE ID CYCLE ENTR CRACKS IN NER LOAD,P	- DADN-6 TRIES,M= 7 N HOLE,B= 0 ,P= 0.000 = 1.4800		CRACK TYPE GROSS AREA HOLE DIAMET	YPE CODE,E= 1 REA STRESS,S= AMETER,D= 0.6	1 ≠ 8.200 8000 8.0206	B
CYCLES 52000 63400 116000 136300 161600	11 00 00 00 00 00 00 00 00 00 00 00 00 0	©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©©	0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00	മമയമയയയ മമയയയ മമയയ നെ സസർവംഗ വെഗയർ4യ വെഗർവർ	1.17000E-03 1.17000E-03 1.2100E-03 9.8800E-02	X 0000004. M 400000. X 0000000 244000000	X 00004. XX VAC 400-00 V-000-00 V-000-00	## D2C/DN 4.2105E-07 4.4318E-07 4.6153E-07 4.8276E-07 5.9593E-07 5.9595E-07 5.9505E-07 5
100000	4000		e. Bebert		- TOBBOY -		NO. 4	

⊣004000r

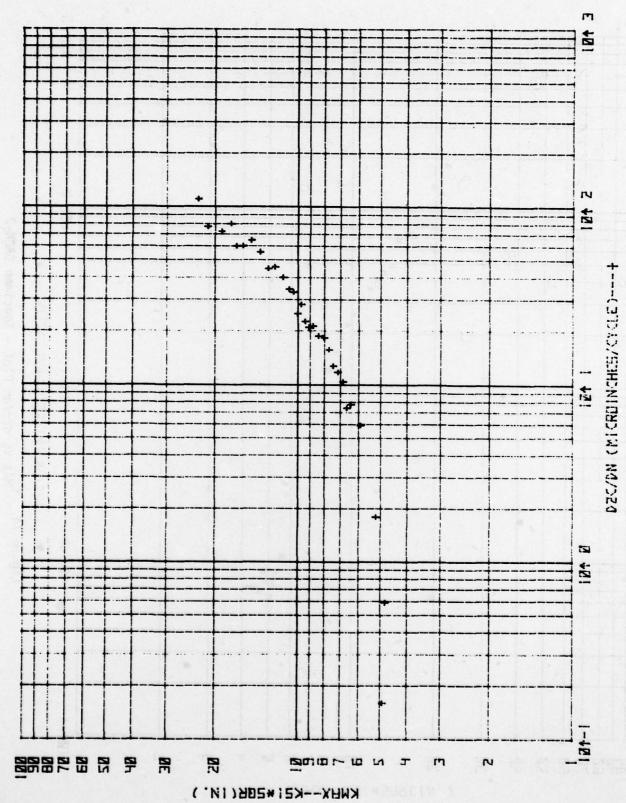
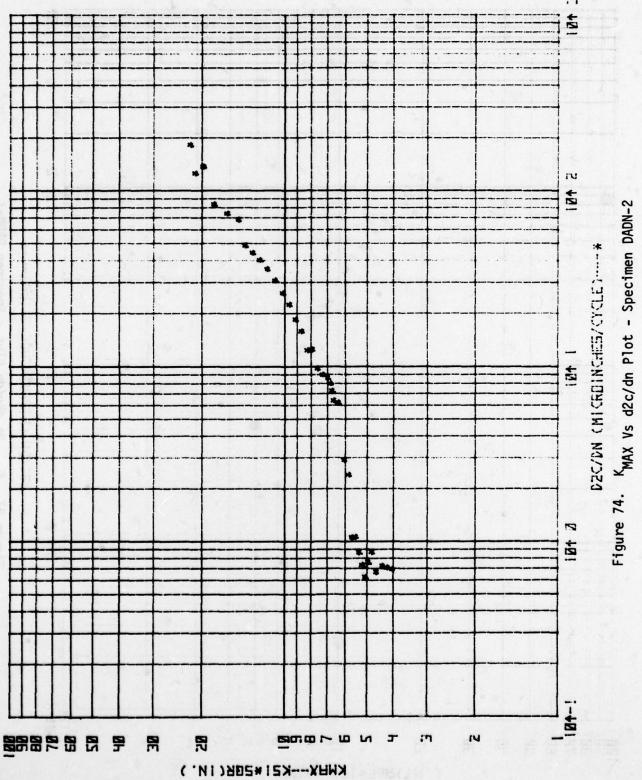


Figure 73. K_{MAX} Vs d2c/dn Plot - Specimen DADN-1



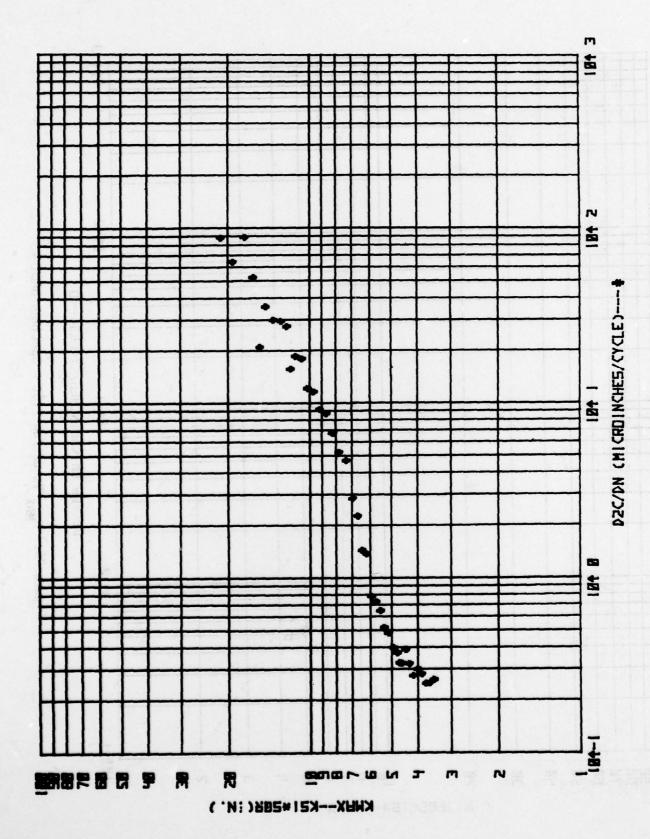


Figure 75. K_{MAX} Vs d2c/dn Plot - Specimen DADN-3

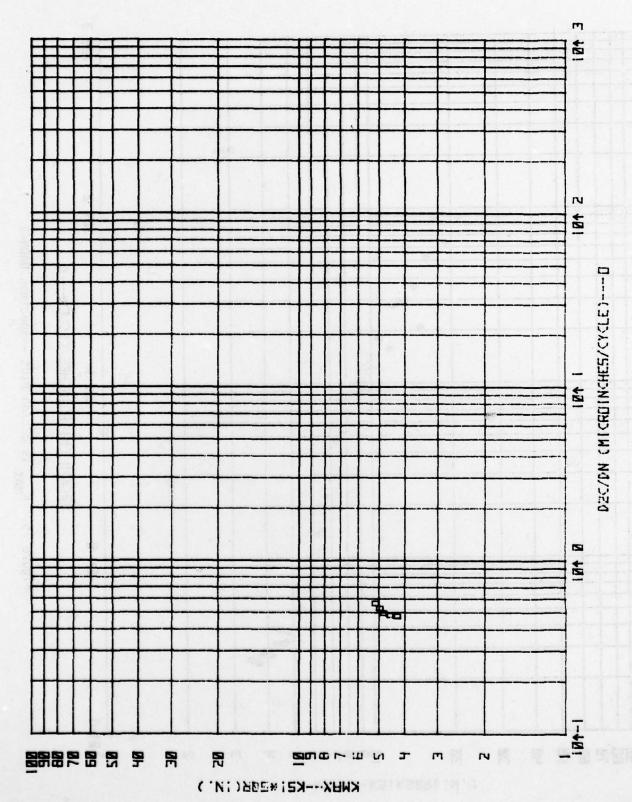


Figure 76. K_{MAX} Vs d2c/dn Plot - Specimen DADN-4

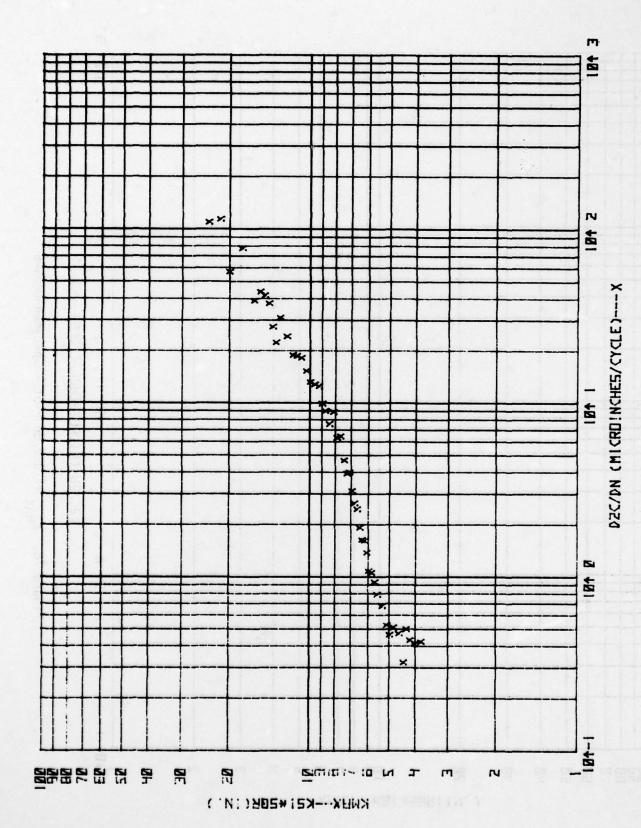


Figure 77. K_{MAX} Vs d2c/dn Plot - Specimen DADN-5

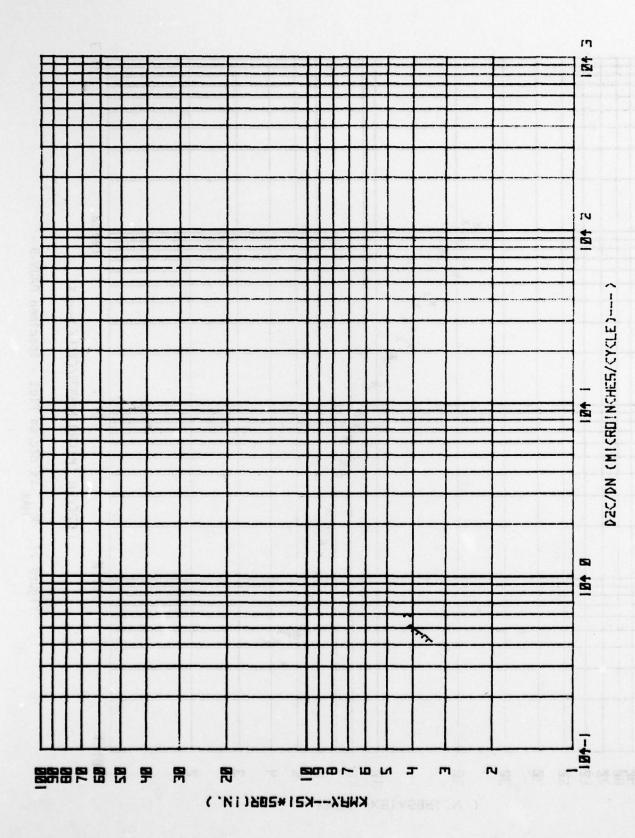
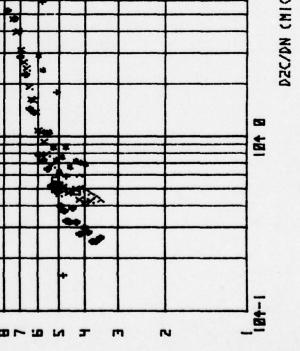


Figure 78. K_{MAX} Vs d2c/dn Plot - Specimen DADN-6



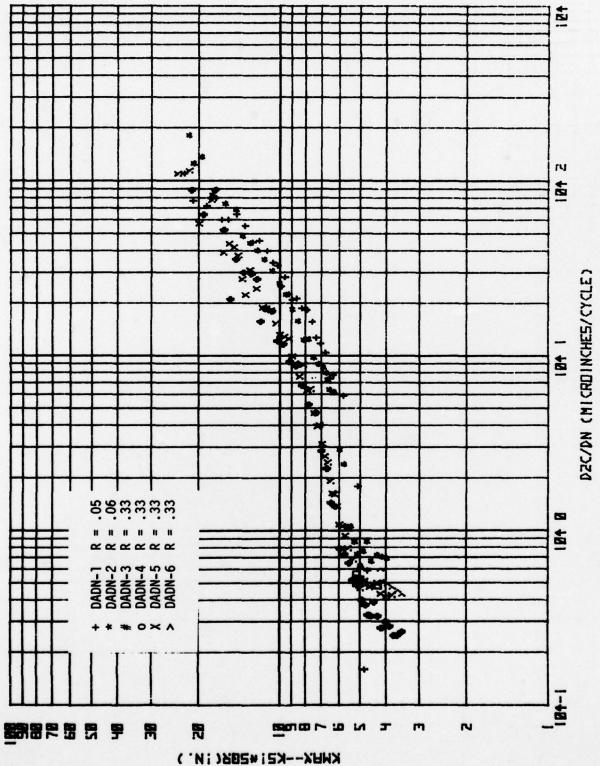


Figure 79. K_{MAX} Vs d2c/dn Composite Plot DADN-1 Thru DADN-6

ſ*!